Materials & Methods

Selection & use of

metals, nonmetallics, parts, finishes,

in product design & manufacture

April, 1957

Electrical Insulation Materials—M & M Manual

Combination Laminates

Creep Properties from Short Time Tests

Carburized Iron Power Parts

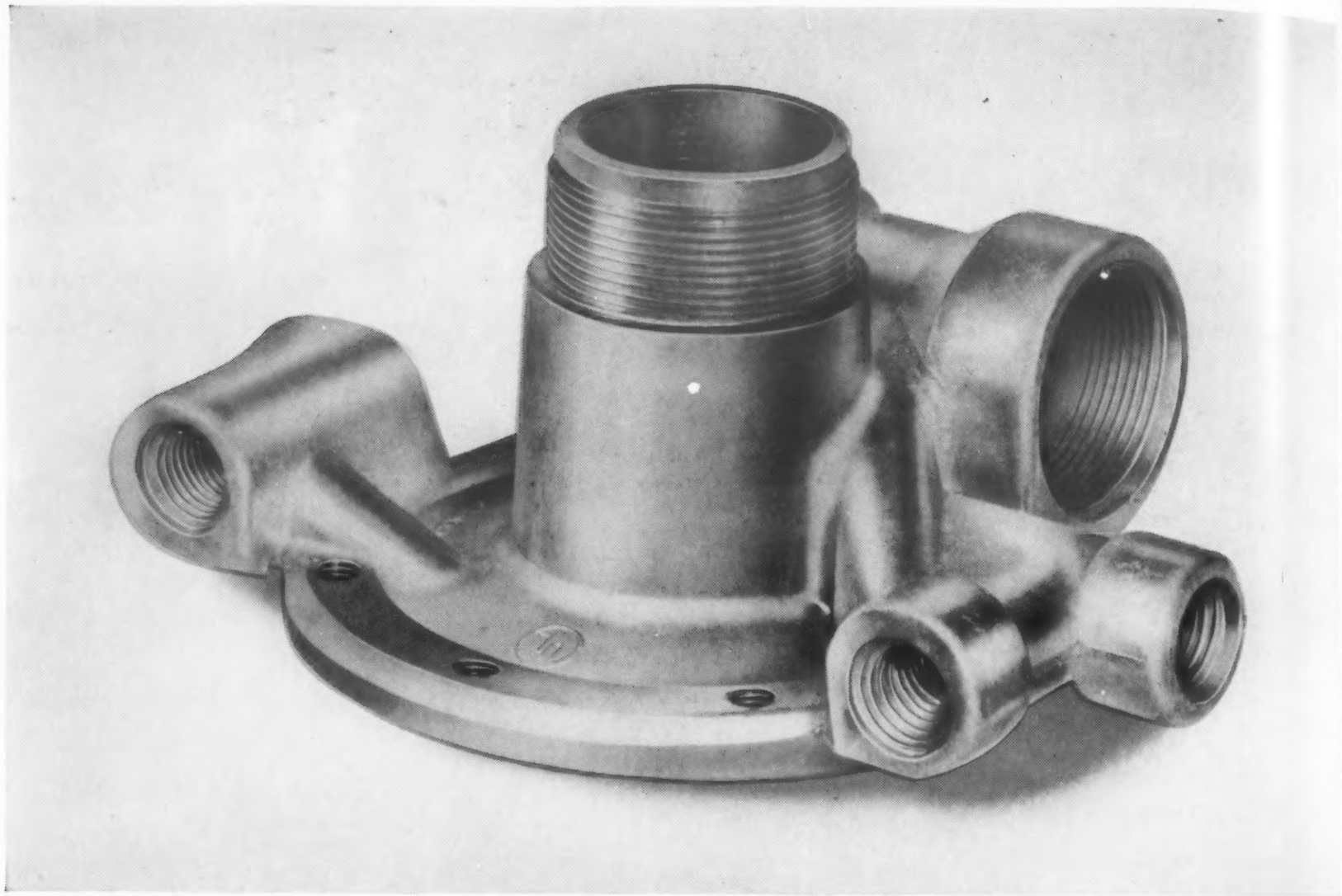
Epoxy Coatings for Metal Products

Dry Bearing Materials

Self-Expanding Thermoplastic Foam

Complete Contents—page 1

PRICE FIFTY CENTS

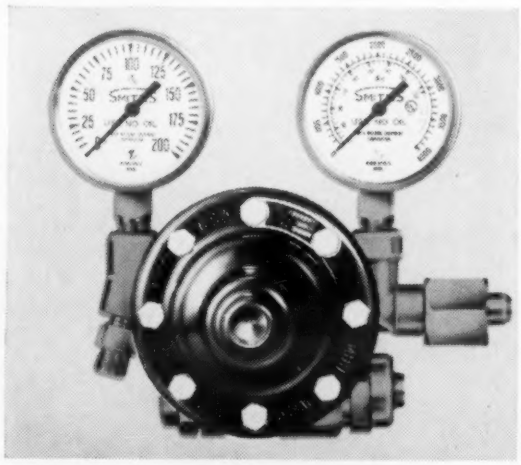


Anaconda Die Pressed Brass Forging after machining, ready for assembly in the gas-pressure regulator shown below.

Better regulators at less cost—with die pressed forgings

Save 25% in first cost—cut machining time, tool cost

Smith Welding Equipment Corp. of Minneapolis uses Anaconda Die Pressed Brass Forgings for gas-pressure regulator bodies as a result of the following analysis of the job.



Smith's two-stage oxygen regulator, Model H313. One of the Smith Welding Equipment Corp. products using Anaconda Die Pressed Brass Forgings.

First, die pressed forgings make a superior product because the twice-wrought metal has the uniformity, denseness, toughness, and strength to prevent gas leaks and to withstand pressures that run in excess of 2500 psi. And second, the forgings do the job economically. The initial cost of the die pressed forging is 25 percent less than the cost of sand castings. In addition, savings are realized in substantially reduced tool costs and machining time. And finally, the forgings are finished in a simple bright-dipping operation, with savings over sand castings estimated at 5 cents a unit.

SHORT CUTS: Anaconda Die Pressed Forgings are short cuts to superior products. Because of their high strength, hardness and resistance to impact, abrasion, and corrosion, they serve better functionally, often replacing more costly built-up assemblies of cast, stamped, drawn, or other machined parts. Their consistent accuracy of dimension eliminates most surface machining to size, permits trouble-free use of drilling jigs, threading or milling fixtures, broaching vises in secondary operations. They are ideally suited to high-speed automatic chucking machines.

The die pressed forging technique is practically unlimited in diversity of shape and field of application. Specialists at The American Brass Company will be glad to submit estimates on the cost of forgings for your critical components. Just submit a sketch or sample of the part involved—or write for Publication B-9. Address: The American Brass Company, Waterbury 20, Connecticut. In Canada: Anaconda American Brass Limited, New Toronto, Ontario. 5706

ANACONDA® **COPPER ALLOY DIE PRESSED FORGINGS**

Short cuts to superior products

For more information, turn to Reader Service Card, Circle No. 500

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Materials & Methods®

Selection & use of metals, nonmetallics, parts, finishes in product design & manufacture

APRIL 1957 **VOL. 45, NO. 4**

PRICE 50 CENTS A COPY. PAYABLE IN ADVANCE, ONE YEAR, $3.00; TWO YEARS, $5.00 IN U. S., POSSESSIONS AND CANADA. IN ALL LATIN AMERICAN COUNTRIES: ONE YEAR, $10.00; TWO YEARS, $16.00. ALL OTHER COUNTRIES: ONE YEAR, $15.00; TWO YEARS, $25.00 (REMIT BY NEW YORK DRAFT). PRINTED BY PUBLISHERS PRINTING CO. SECOND CLASS MAIL PRIVILEGE AUTHORIZED AT NEW YORK, N. Y. ADDITIONAL ENTRY AT BROOKLYN, N. Y. ESTABLISHED IN 1929 AS METALS AND ALLOYS.

Better flavor, better health in every bite . . . thanks, in part, to Monel.

What does this new sea salt have that you need?

Here is a new type of salt . . .

Three-quarters of it is sodium chloride — common salt. The other quarter consists of a natural mixture containing so-called "trace elements" — tiny amounts of copper and cobalt and magnesium . . . zinc . . . molybdenum . . . manganese . . . calcium . . . and other elements and minerals.

Experts believe that these trace elements may hold the key to many health problems. And with reason. Hasn't iodine been used to prevent goiter? Fluorine to stop tooth decay? Iron to overcome anemia?

Hence a spanking new plant—35 miles south of Corpus Christi, Texas — to produce *Admiral* Sea Salt from Baffin Bay, where the water is almost twice as salty as average sea water. Of course, the high salt content is an advantage from a manufacturing standpoint. But from the angle of plant designing — !

Engineers faced two potentially serious corrosion problems. Attack on *inside* surfaces of equipment by this extra-salty water . . . and attack on *outside* surfaces by salt-laden breezes.

Use of Monel* nickel-copper alloy in the more critical pieces of plant equipment avoids both hazards. Monel alloy is one of a family of Inco Nickel Alloys noted for corrosion resistance. Widely used in chemical, petroleum, marine and other industries where acids or alkalies are frequent troublemakers, Monel provides a ready solution to many common problems.

If you have a problem in which corrosion, high or low temperatures, stresses, fatigue, or the maintenance of product purity are troublesome factors, let's talk it over. We may be able to help you find out how Monel — or one of the more than fifty Inco Nickel Alloys now available — can overcome *your* difficulties. *Registered trademark

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Nickel Alloys Perform Better, Longer

For more information, turn to Reader Service Card, Circle No. 530

What's new IN MATERIAL

...AT A GLANCE

A NEW CORROSION PREVENTIVE LINING MATERIAL, an elastomeric copolymer based on vinylidene chloride, is now available. The flexible thermoplastic material resists a broad range of acids, alkalies, salt solutions and solvents. It can be readily installed with an adhesive.

COLUMBIUM offers promise as a high temperature material. Compared with molybdenum, the material has better oxidation resistance and retains its ductility after heating to elevated temperatures. Although columbium readily reacts with oxygen, nitrogen and hydrogen, it is easier to fabricate than other high melting metals. (See article in next month's issue for further details.)

SYNTHETIC FIBERS are being evaluated as reinforcing agents for acrylic resins and polyethylene. Impact strength of an acrylic resin is said to be improved eight times by reinforcing it with Orlon fibers. Although synthetic fiber reinforcement of polyethylene is still in the initial stage, it has been found that important gains in physical properties can be achieved with relatively minor fiber additions.

A NEW HIGH STRENGTH, HIGH TEMPERATURE ALLOY is finding use as turbine disks in jet engines. The material is essentially an alloy of iron, nickel, chromium, molybdenum, titanium and boron. It withstands 75,000 psi stress at 1200 F for 300 hr; under the same conditions a conventional turbine disk lasts only 10 hr. (More details next month.)

ISOTACTIC POLYPROPYLENE, twice as strong as ordinary polyethylene, is being made on a pilot plant scale in Italy. Like polyethylene, the material is expected to be useful in the form of film, moldings, pipe, bottles, and wire and cable insulation. Another potential use: a synthetic fiber for filter cloths and upholstery.

NEW GLASS DISPERSIONS provide a protective and lubricating coating during the forging of special alloy steels, titanium and other metals. Applied to metals at room temperature, the glass fuses to the surface of the metal during the heating cycle and inhibits oxidation and surface contamination.

STRONGER SHEET MATERIALS are possible with a new German technique that shapes metals, plastics, pressed wood and glass into sheets having raised surfaces. It is claimed that the new technique increases ductility making the material 80 to 100% more impact resistant than ordinary sheet materials. Two or more sheets can be joined into a

What's new IN MATERIALS

single panel having buckling and bending strengths more than ten times that of similar flat sheet structures.

QUICK IDENTIFICATION OF NONFERROUS METALS is possible with an electronic device. Small enough to be carried in the hand, the instrument contains a calibrated dial that measures electrical resistivity of the material. Metals and alloys can be distinguished provided their specific resistivities are between 1 and 28 microhms per cu cm.

PLASTICS PIANO MECHANISMS are now being made in France. Unlike wood, the plastics mechanisms do not contract or expand under different climatic conditions and are resistant to chemicals and heat. Made of an unidentified plastic, the mechanisms are molded and do not require expensive machining operations.

ALUMINUM AND PLASTICS will be commonplace in the home of tomorrow, according to recent reports. Radiant heating aluminum rugs and wallpaper, as well as plastics plumbing fixtures and molded plastics bathrooms will be found in the future home. Plastics domes covering both house and garden are also projected.

HIGH DENSITY POLYETHYLENE, a new material two years ago, is finding increasing use in toys, hot water pipes, fibers and woven fabrics. Currently, six chemical companies are building facilities for producing this resin. The material, said to be more oil and acid resistant than low density polyethylene, is also finding use in refrigerator trays that won't bend easily, and in containers that can be washed in automatic dishwashers without melting.

AN ELECTRONIC DEVICE utilizing a magnetic ferrite core is being used instead of transistors in Japan. The device, consisting of a coil, magnetic core and condenser, is cheaper to manufacture and has fewer electrical contacts than a transistor.

A NEW CLASS OF TITANIUM ALLOYS is claimed to react to heat treatments "very much like steel." Not yet in commercial use, the new alloys contain titanium, copper, aluminum and tin. They are strong and ductile at temperatures up to 1000 F.

A CERAMIC FOAM MATERIAL is capable of withstanding temperatures up to 1600 F. Compressive strength of the material is above 400 psi at both room temperature and 1600 F. It is recommended as an insulating material for aircraft parts and as a core material for electronic parts. (More details next month.)

ALUMINUM POWDER is being rolled into strip. Additional rolling causes the formation of a reasonably ductile foil by cold welding.

Turn to page 171 for more "What's New in Materials"

MATERIALS BRIEFS

Not Very Attractive

Results of measuring the magnetism of bricks made in 1933, 1465 and 200 A.D. show that today's magnetic field is some 18% weaker than in 1465 and 35% weaker than in the year 200.

Fish Story

Tropical fish are being transported in sealed plastics bags of water in which the air is displaced by pure oxygen. The fish can remain in the bag for several days without harm.

Blades for Bamboo

Japanese craftsmen use 400-year-old samurai swords as knives for carving bamboo. They say that steel forged after 1596 is inferior for cutting the extremely hard wood.

Look! No Holes

An epoxy coating 0.001 in. thick may be used on teeth someday to prevent cavities. The coating would be applied by a dentist every six months.

'Drag' for Junior

A rear-engine sports car made of reinforced plastics is the latest thing in toys. Complete with lights and dual exhausts, the car will do a cool 30 mph.

Cool Audience

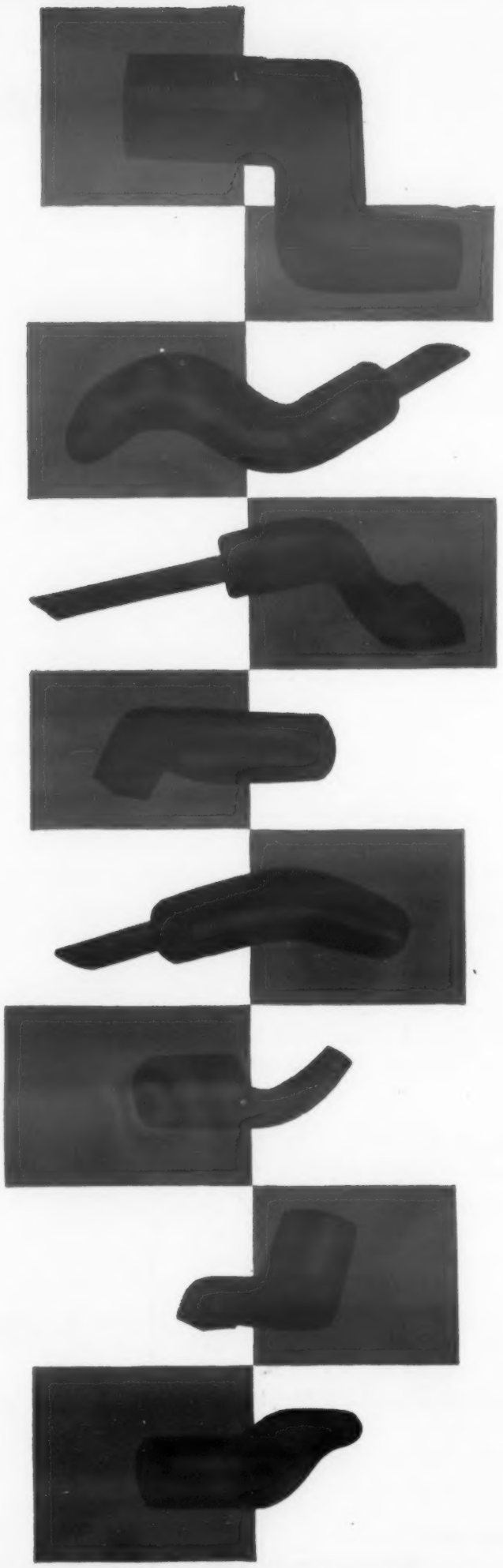
The Navy has developed a dummy that listens. Used to test ear protection devices, the dummy is a plaster replica of a human head and can endure noise volumes that would injure a human ear.

Armored Boots

Flexible steel mesh is being used in woodsmen's boots to provide protection against accidental cuts or slashes from flying axes.

Pick Your Special Electrodes

From Hundreds of Existing MALLORY Designs



Need odd-shaped electrodes for resistance welding around corners, inside channels, or other out-of-the-ordinary places?

Before you go to the time and expense of ordering custom-made special electrodes, see what Mallory existing designs can do for your job. We have flexible tooling available for hundreds of different odd-shaped electrodes. What you consider a "special" may well be an existing Mallory type that you can get on prompt delivery . . . and at economical cost.

Included in the Mallory line are cold formed single bend and double bend types. Also, cast and forged offset designs. You have a wide choice of nose shapes, tapers and lengths. Bent electrodes are made by an exclusive Mallory cold-forming technique which develops maximum strength and hardness, to assure long life. Both single and double bend types can be supplied with fluted cooling holes and water tubes bent in place*, to assure highly efficient cooling right up to the welding face. All types use specialized alloys and manufacturing methods which Mallory has developed during thirty years of pioneering and leadership in the resistance welding field.

Stock Mallory straight electrodes, holders, seam welding wheels, dies, forgings and castings are listed in the latest edition of our Resistance Welding Catalog. Write today for this valuable reference book . . . and see your local Mallory welding distributor for prompt delivery of high quality welding supplies.

*Patent No. 2,489,993.

30 Years of Resistance Welding Leadership

In Canada, made and sold by Johnson Matthey and Mallory, Ltd.
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Electromechanical—Resistors • Switches • Tuning Devices • Vibrators
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For information on titanium developments, contact Mallory-Sharon Titanium Corp., Niles, Ohio

For more information, turn to Reader Service Card, Circle No. 450

MATERIALS AT WORK

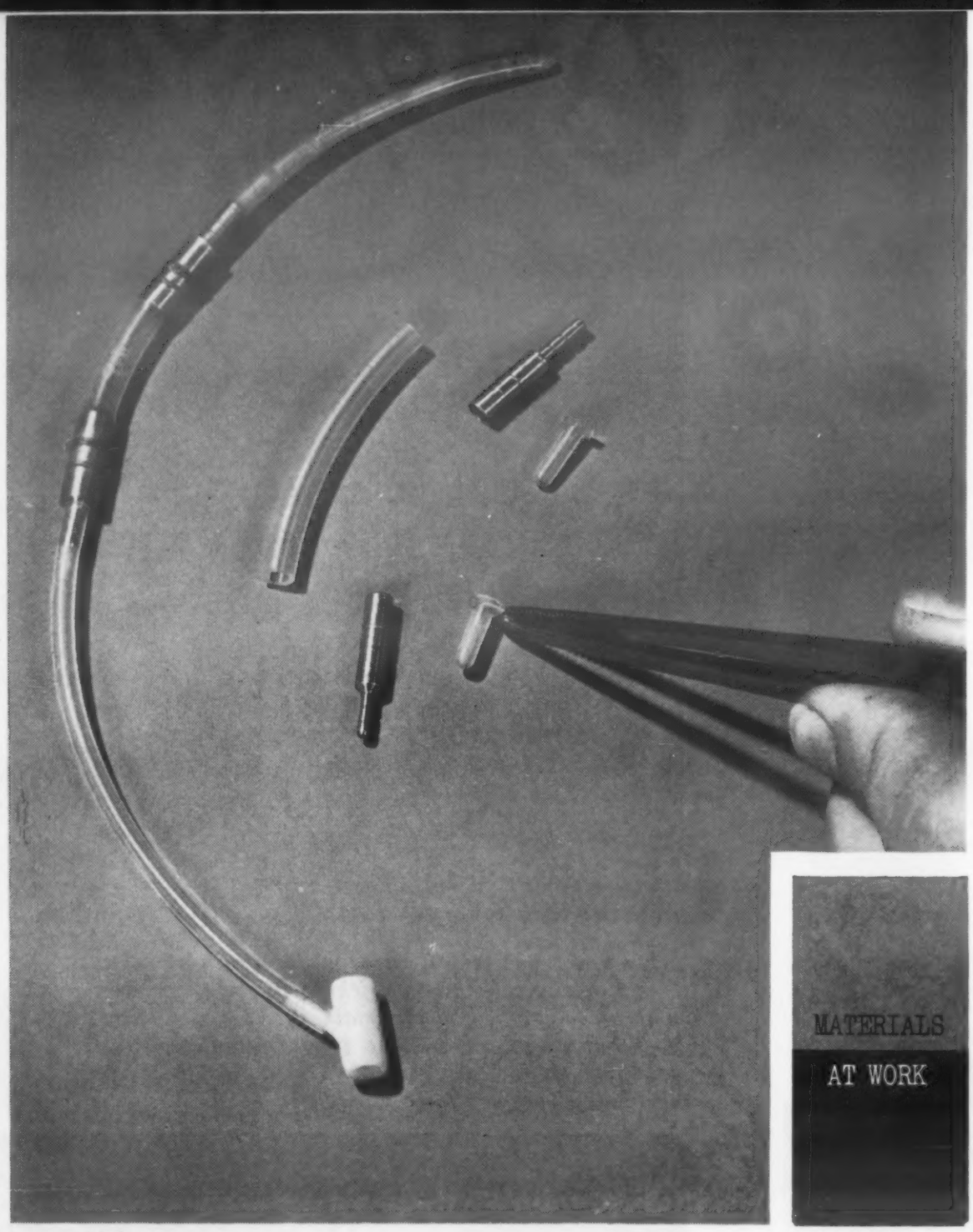
New and interesting applications of engineering materials

Propane tank covers . . .

. . . and ventilation crowns *for grain storage bins are degreased with trichloroethylene, primed with a compatible zinc chromate, then sprayed with gold butyrate lacquer. The propane tank covers, after air drying only 15 min, get a final coat of clear alkyd lacquer for a high sheen finish.*

Gold butyrate lacquer stays tarnish-free

A gold-pigmented lacquer based on Eastman Chemical's half-second butyrate is now used on process equipment made by Black, Sivalls & Bryson, Inc. The gold coating used previously had tarnished and deteriorated rapidly when exposed to outdoor weather.



MATERIALS AT WORK

Silicone rubber solves medical problem

Silicone rubber is the essential element in a new automatic brain valve which is expected to save the lives of from 10,000 to 15,000 people yearly.

The valve was specifically invented to treat hydrocephalus, a fatal children's disease in which spinal fluid that normally drains into the system gradually accumulates in the head. Previously a plastics tube was inserted into the brain to drain the fluid to the abdominal cavity. However, when the child outgrew the tube, scar tissue invariably clogged the opening. A better idea was a short tube draining into the jugular vein, but it called for an unbelievably precise plastics valve to prevent backflow of blood.

The new valve uses two side-slit directional nipples of silicon rubber —accurate to 0.0003 in.—inside stainless steel cases (see photo). Connected with a silicone rubber housing, the valves open at the slightest input pressure but provide a double seal against fatal flowback. The rubber material, supplied by Dow Corning Corp., is soft, resilient, translucent and nontoxic. Other advantages: 1) it will not rupture delicate body tissues, 2) it will not encourage growth of tissues by reacting chemically with them, 3) it is easily molded, and 4) it resists sterilization temperatures.

"Do-it-yourself" neon signs

A new concept in the design of neon signs makes use of interchangeable neon-lighted letters which "plug" into a molded phenolic base.

Manufactured by U-Change Neon, Inc. and molded of a Durez phenolic, the sign bases are static-free, lightweight, nonconductive, unaffected by temperature changes and waterproof. In the event of breakage only the individual glass letters need be replaced.

In order to maintain weatherproofing, a pliable seal fits on the electrode and seals off moisture, and caps cover letter sockets not in use. Signs come in six neon colors.

Aluminum wheel better than steel

An aluminum wheel, die cast as an integral unit including hub and brake drum, offers improved brake performance, greater strength and lighter weight compared to a conventional steel wheel assembly.

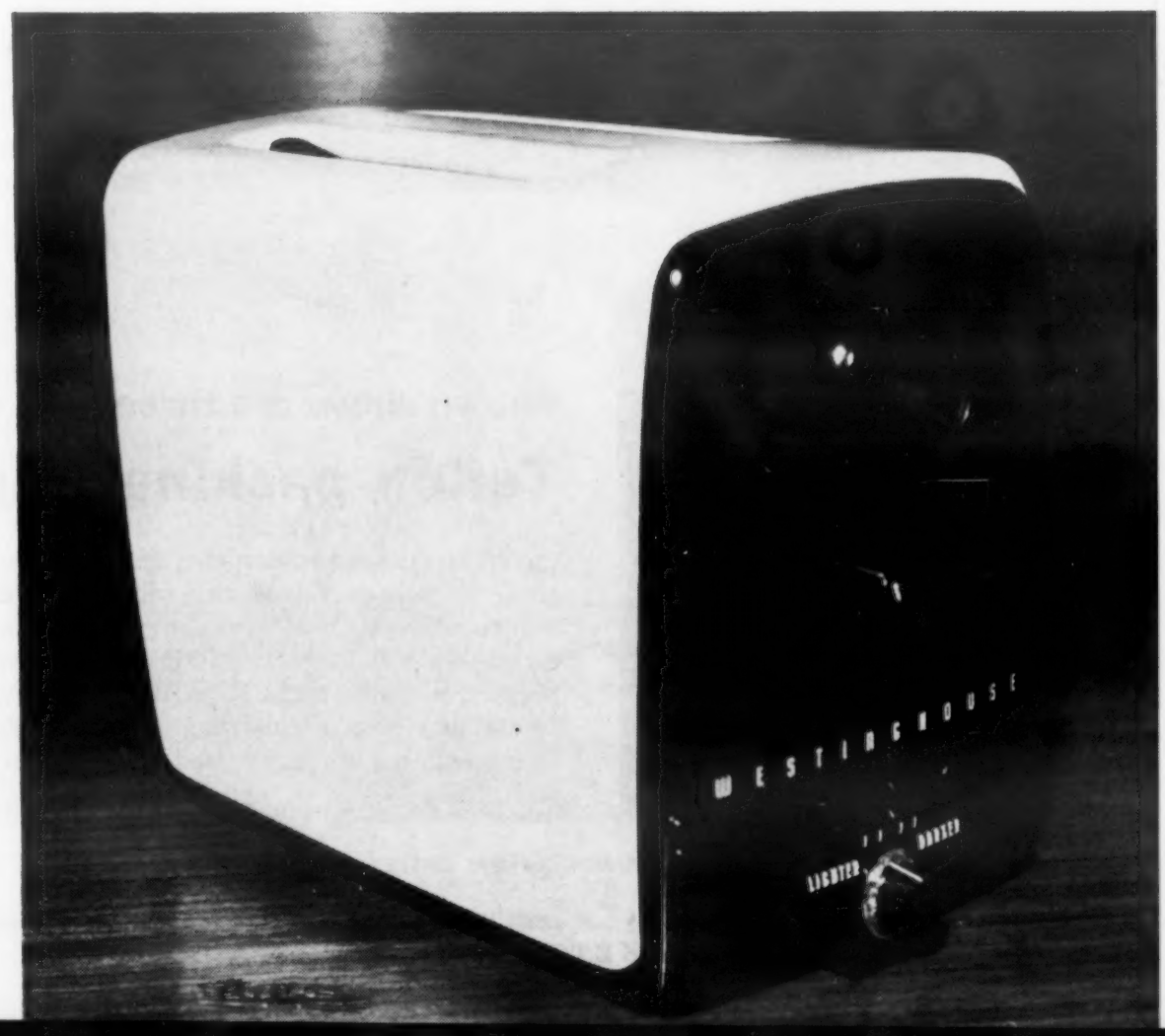
Kaiser Aluminum, who developed it, says tests indicate that the aluminum wheel surpasses accepted standards for wheels in both brake performance and durability. One outstanding advantage of the use of aluminum is that there is less brake fade. This is attributed to aluminum's rapid heat dissipation and to design features that provide a more direct heat-flow path to the cooling area. Radial ribs on the surface of the wheel establish direct air flow over the periphery of the drum in addition to providing rigidity.

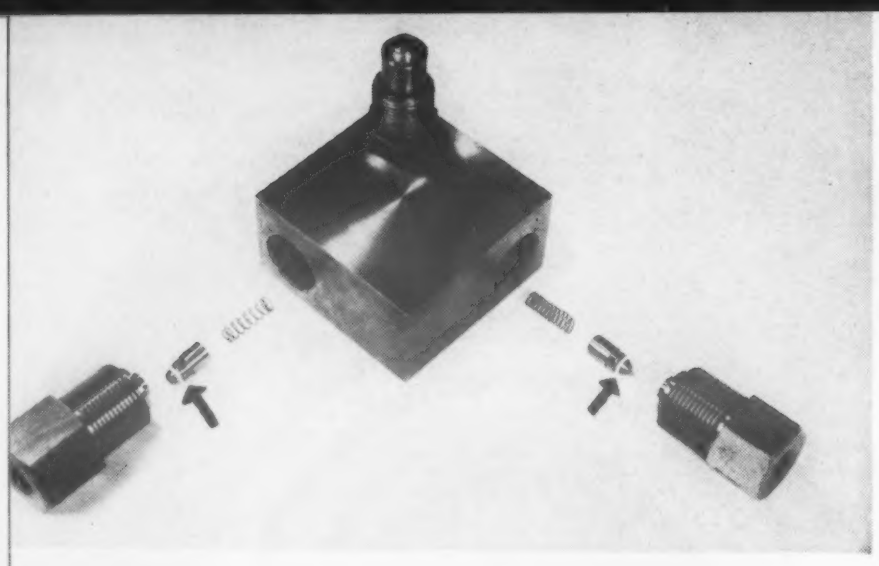
The braking surface of the wheel can be either a metallurgically bonded iron liner, a cast-in iron liner, or a metallurgically bonded metal spray liner. The wheel, complete with 14-in. dia steel rim, weighs only 30 lb as compared to 42.6 lb for a comparable steel wheel, hub and brake drum assembly.

Porcelain enamel used for toaster

In the toaster shown at the right, a porcelain enamel coating was successfully fired at 1300 F to 0.032-gage steel. The coating has a maximum thickness of 0.008. The firing operations on both ground and cover coats were accomplished in the same furnace conveyor at the same temperature.

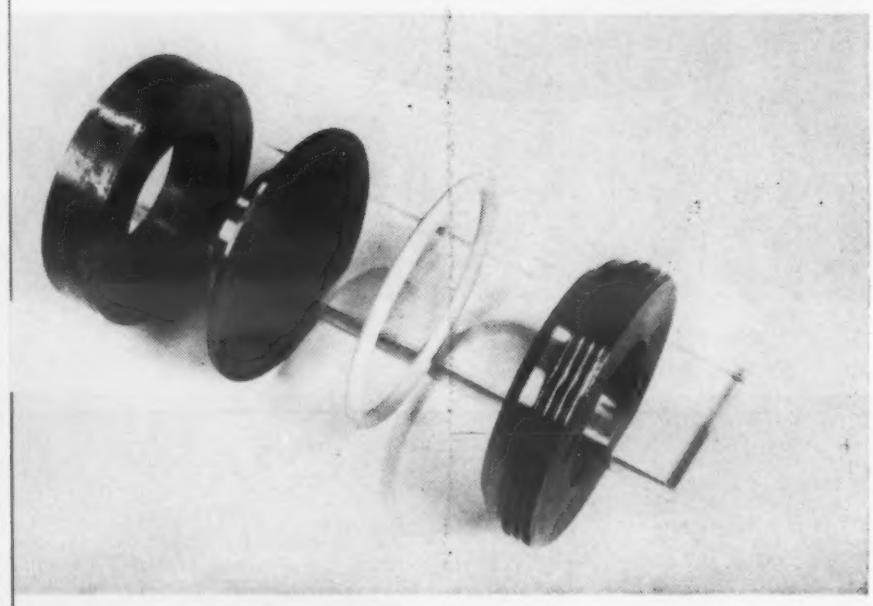
Developed by Westinghouse Electric Corp. and the Irvite Corp., the new low-firing enamel offers the design engineer considerable flexibility in the design of small appliances. For one thing, thinner gage steel can be used without fear of buckling; in addition, extremely thin coatings are possible.





***Poppet valve**—The use of PTFE packing rings in poppet valves makes it possible to pump organic liquids and catalyst solutions which would swell and disintegrate other synthetic elastomers customarily used in poppet valves. However, PTFE is a thermoplastic and it requires special treatment: when the packing ring is forced into the retaining groove, it is deformed by stress. This strain is removed by heating the completed assembly at 350 F for 30 min. When prepared in this manner, poppet valves operate satisfactorily in 15,000-psi pumps.*

***Self-sealing closure**—This packing ring is used in a self-sealing closure which holds 22,500 psi pressure in a 1-in. dia chemical reaction vessel. The packing ring is placed in the 45-deg angular space between the flanged tube liner and the beveled head button. Initial sealing is accomplished by hand torque on the head nut. Thereafter the self-sealing principle applies and increases the tightness of the seal in proportion to the increase of pressure in the vessel.*



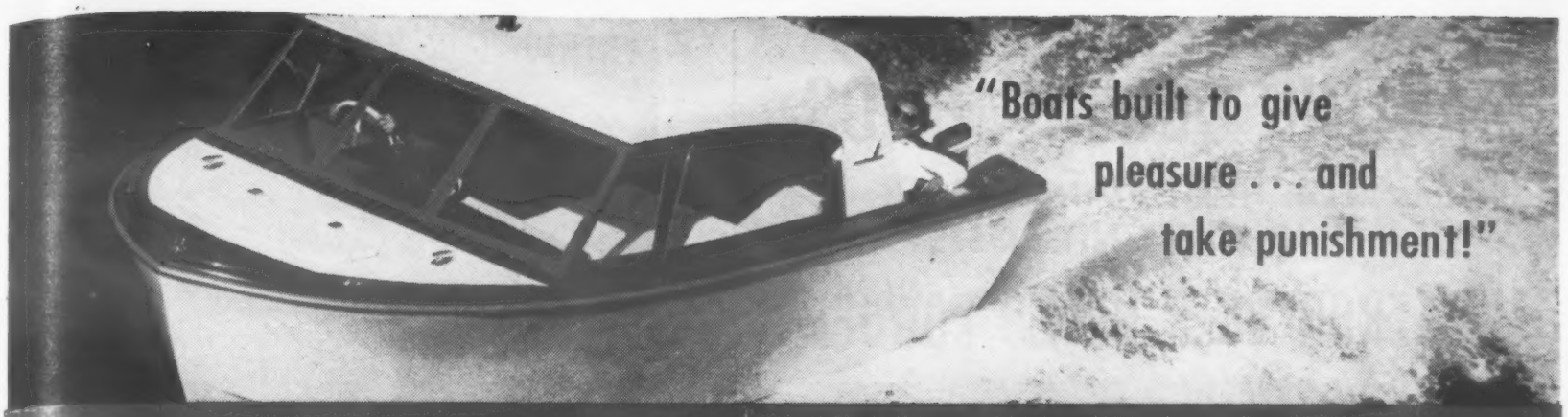
***Rupture disk closure**—A rupture disk closure assembly consisting of a shear block, a rupture disk, a 2¼-in. dia packing ring of PTFE and a beveled retaining ring was installed in the pressure side of an autoclave bottom cover. The initial seal was made by hand torque applied to the retaining ring. The high pressure seal was made by increasing the internal pressure in the autoclave. The same PTFE packing ring was used 110 consecutive times.*

MATERIALS AT WORK

Shown above are three uses of . . .

Teflon packing rings

Teflon (polytetrafluoroethylene) is now being used for packing rings in poppet valves and self-sealing closures in high pressure pumps and chemical reaction vessels. In addition to eliminating metal-to-metal contact, PTFE offers a combination of outstanding properties which make it particularly suitable for this application: 1) stability over a wide range of temperatures, from –100 to 300 F, 2) exceptional strength, and 3) excellent resistance to chemicals and water.



● Bumps and bruises that would often splinter an ordinary craft are shrugged off by these sturdy boats made with RCI POLYLITE polyester resin. Plastic Fabrications, Inc., Miami, Florida, reports that the inherent resiliency of RCI POLYLITE reinforced with fibrous glass allows a hull to "give" under pressure instead of offering stiff resistance — thus improving the overall strength and safety factor of their products.

In addition, a molded boat permits more attractive and complicated hull and deck structure — usually expensive features — at reasonable cost . . . and eliminates sharp edges that are dangerous in angry waters.

"In production, our primary requirement is a base material with consistent formulation," says J. A. "Woody" Woodson, Plastic Fabrications' president, in explaining why his firm uses RCI POLYLITE. "The curing and weathering characteristics must not vary from batch to batch. If a resin does not cure, our time and labor is lost and the section must be discarded."

"Another 'plus' for Reichhold POLYLITE," continues Mr. Woodson, "is *dependable* distributor arrangements. Our POLYLITE orders are delivered *on time*, so that costly production delays are a thing of the past."

Products possessing the unique advantages possible with RCI POLYLITE — lightweight strength, durability, and easy maintenance — are becoming increasingly popular and profitable in today's market. For additional information about how RCI POLYLITE can be incorporated into one of *your* products by laminating, molding or other plastic applications, write for free *Booklet A.*

Constructed economically with
UNIFORM QUALITY **POLYLITE** RESINS

REICHHOLD CHEMICALS, INC., RCI BUILDING, WHITE PLAINS, N. Y.

For more information, turn to Reader Service Card, Circle No. 594

Humidity indicator questioned . . .

To the Editor:

We are interested in an item in the November issue of MATERIALS & METHODS. It appeared in the "Materials Outlook" section and concerned a ceramic that indicates humidity change.

The response time indicated is not very fast. Most government specs require a response time of 10 sec, although we must define what response time is. We wonder if this is not the carbon black hygrometer developed by Arthur D. Little for the Signal Corps five or six years ago.

ROBERT G. CLARK
Clark & Co.
Salisbury, Md.

. . . and now clarified

To the Editor:

In regard to whether this is the carbon black hygrometer developed by Arthur D. Little, I can state that it is not. It is a newly discovered material of a ceramic nature and was the result of an investigation in the laboratories of Horizons, Inc.

The question of response time of the detector is a different situation, and our original statement was misleading. This situation arose because of the way we defined response. We have now restated it in more conventional and explicit terms.

Response times of less than 10 sec for indicating 90% of an abrupt change of 50% relative humidity have been observed. In this respect the material appears to approximate the characteristics of the National Bureau of Standards' evaporated elements reported in a *Journal of Research of the National Bureau of Standards* article entitled "A Fast Responding Electric Hygrometer," by A. Wexler et al (vol. 55, no. 2, p 71, Aug '55).

We are at present preparing more complete technical data for release to interested parties.

EDWARD F. MAYER
Department Head, Physics
Horizons, Inc.
Cleveland, Ohio

We're out of step, it seems

To the Editor:

In the January, 1957, issue of your fine magazine there appears an article entitled "Stepped Extrusions—A New Metal Form," by a member of Kaiser Aluminum and Chemical Corp. Both the title and the subhead contain extremely misleading information.

Although we may be measuring time by different yardsticks, we don't think you properly can consider stepped extrusions as a new metal form. An article entitled "Stepped Extrusions" by Kirby F. Thornton

compare with the standard

...in high speed steels the standard's REX

Ever since grandad's day, Crucible's REX® high speed steel has been *the standard by which all other high speed steels are compared.* And now the quality and uniformity of REX are even *better,* thanks to improved manufacturing techniques at Crucible.

Don't take our word for it. Prove for yourself how REX leads in structure, uniformity, response to heat treatment, and fine tool performance.

Ask for REX at your nearby Crucible warehouse — or order it through prompt mill shipments. And, for a list of available data on all Crucible special purpose steels, write now for a free copy of the "Crucible Publication Catalog". *Crucible Steel Company of America, The Oliver Building, Mellon Square, Pittsburgh 22, Pa.*

CRUCIBLE first name in special purpose steels

Crucible Steel Company of America

For more information, turn to Reader Service Card, Circle No. 505

(*Mechanical Engineering*, July '44, p 443) reported Alcoa's activities in developing and producing stepped extrusions.

Your subhead states it is *now* possible to obtain an aluminum extrusion having two or more different cross sections. Naturally, an extrusion with one step will have two different cross sections. This type has been common at Alcoa since 1944.

Regarding two, three or more steps, your article says merely that it *may* be possible to produce an extrusion with more than one step. In 1944 Mr. Thornton stated that it is technically feasible to produce extrusions with as many steps as might be required. Since extrusions containing more than one step could have been produced in 1944, it is improper to suggest that such an extrusion is *now* possible.

We merely want to keep the record straight, and since Alcoa pioneered the development of stepped extrusions, I'm sure you can appreciate our position. And I want to emphasize that the objection is to the title and subhead, and not to the information restated in the article.

WILLIAM K. KINNER
Public Relations Dept.
Aluminum Co. of America
Pittsburgh 19, Pa.

We must admit that we were not aware of the facts stated by Mr. Kinner, and we take this opportunity to call the previous literature cited to our readers' attention.

Bouquet for the prices department

To the Editor:

As a faithful reader of MATERIALS & METHODS I would like to congratulate you on the new and logical presentation of your publication, which increases its use and readability.

Your new section on prices was of particular interest to me, especially the prices of nonmetallics, which, to my knowledge, are not to be found anywhere else in an organized form.

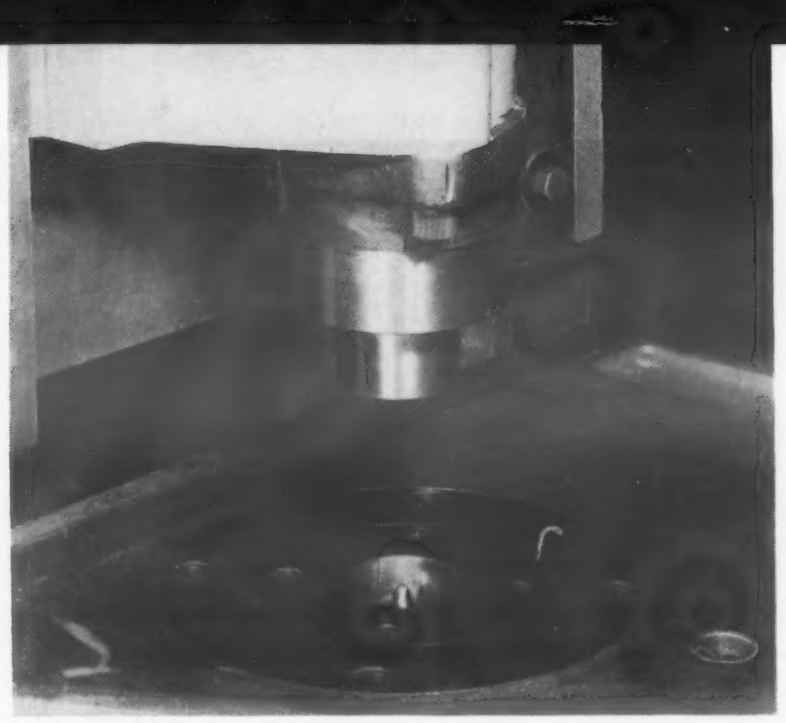
I should like to submit two suggestions for your consideration with respect to plastics prices in particular:

1) It is my hope that you will eventually be able to do away with the vagueness attendant upon the quotation of a range of prices rather than specified prices. This will no doubt take place as your list becomes more detailed, yet I trust you will make an effort to follow the prices of a few typical formulations rather than those of a host of different subtypes.

2) I believe it would also be very useful for your readers to have some idea of the past evolution of specified plastics prices. This might take the form either of a table or a graph.

I trust you will take these suggestions as an expression of my appreciation for the work you are doing.

J. H. ROBERT
Aluminum Union Ltd.
Montreal, Canada



Preview

Metal Powder Show Annual MPA Meeting

"New Horizons in Powder Metallurgy" is the theme around which the Metal Powder Assn. will conduct its 13th annual meeting at the Drake Hotel in Chicago, Apr 30-May 1.

This year the meeting will have two types of technical sessions: there will be four powder metallurgy sessions on Tuesday and Wednesday and two special sessions on ferrites and electronic cores on Tuesday. Highlight of the technical sessions will be a panel discussion on presses for compacting metal powder.

The Metal Powder Show, at which latest developments in materials, equipment and parts will be exhibited by more than 25 leading manufacturers, will be open from 9 a.m. until 6 p.m. on both Tuesday and Wednesday. A cocktail hour and banquet will be held Tuesday evening.

A detailed program of the technical sessions and a list of exhibitors are given below.

Program

Tuesday, April 30

9:00 a.m.

Metal Powder Show exhibit opens

9:30 a.m.

(two concurrent sessions)

Powder Metallurgy—Ballroom

9:30—"Activated Sintering," M. EUDIER, La Métallurgie des Poudres

10:00—"Production and Characteristics of Chemically Precipitated Nickel Powder," K. O. COCKBURN, R. J. LOREE and J. B. HAWORTH, Sherritt Gordon Mines, Ltd.

10:45—"Production and Characteristics of Chemically Precipitated Copper Powder," V. S. RYAN, Whitaker Metals Corp.

11:30—"Current Developments in the Rolling of Both Ferrous and Nonferrous Powders," J. D. SHAW and W. V. KNOPP, S-K-C Research Associates.

Ferrites and Electronic Cores—Goldcoast Room

9:30—"How to Take Advantage of Magnetic Core Materials," J. A. ROBERTS, A. SCHMECKENBECHER and G. LUDEWIG, Antara Chemicals Div., General Aniline & Film Corp.

10:15—"Magnetic Cores in Miniature Electronic Circuits," D. M. HODGIN, Collins Radio Co.

(continued on p 21)

Glidden formula for your profit:

CHANGE METAL POWDER TO PRECISION PARTS

Proved way to cut costs on high-volume production of precision parts: Glidden Powder Metallurgy! That's why Glidden *Resistox*® Metal Powders are so widely used for bearings, friction materials, brushes and other parts.

Leading fabricators like The United States Graphite Company, Division of the Wickes Corporation, Saginaw, Michigan (producers of GRAMIX® sintered metal parts), look to Glidden as a primary source for metal powders.

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2:00 p.m.
(two concurrent sessions)

Powder Metallurgy—Ballroom

2:00—"Fiber Metallurgy," C. H. SUMP and W. POLLACK, Armour Research Foundation

2:45—"Primary Consideration in the Design and Use of Sintered Metal Parts," R. TALMAGE, Powder Metallurgy Consultant

3:30—Panel Discussion on Presses for Compacting Metal Powders. Moderator: J. D. SHAW, S-K-C Research Associates. Panel: W. GORT, Arnhold Ceramics, Inc.; B. B. BELDEN, Baldwin-Lima-Hamilton Corp.; J. J. KUX, Kux Machine Co.; C. C. SUTINEN, Mannesmann-Meer Engineering & Construction Co.; G. G. KARIAN, F. J. Stokes Corp.; H. E. ELLIOTT, Watson-Stillman Press Div.

Ferrites and Electronic Cores—Goldcoast Room

2:00—"Characteristics and Applications of Ceramic Permanent Magnets," C. A. MAYNARD, Indiana Steel Products Co.

2:45—"Characteristics and Present Requirements of Ferrites," R. D. HARRINGTON, National Bureau of Standards

3:15—"Latest Developments in Magnetic Storage and Switching Applications," J. W. SCHALLERER, General Ceramics Corp.

4:00—"Thermal Expansion of Ferrite Materials at Temperatures Near the Curie Point," W. R. BUESSEN, Pennsylvania State Univ. (research sponsored by Stackpole Carbon Co.)

6:30 p.m.
Reception and cocktail hour—Grand Ballroom

7:30 p.m.
Banquet—Goldcoast Room

Wednesday, May 1

9:00 a.m.
Metal Powder Show exhibit opens

Powder Metallurgy—Ballroom

9:00—"New Developments in Metal Powder Filters," L. H. MOTT, Cuno Engineering Corp.

9:30—"New Developments in Diamond Products Using Metal Powders," L. KUZMICK, J. K. Smit & Sons, Inc.

10:15—"Metal Powders in Brazing and Soldering," P. D. JOHNSON, Glidden Co.

(continued on p 23)

KUX

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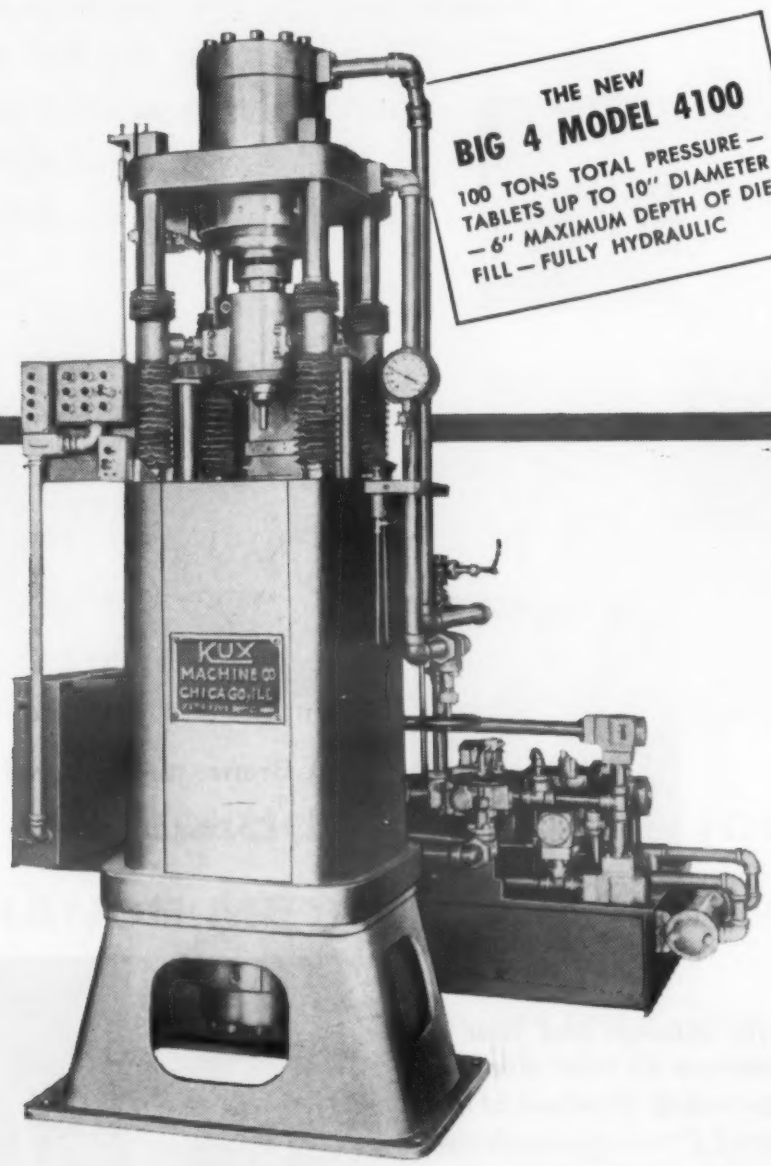

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100 TONS TOTAL PRESSURE — TABLETS UP TO 10" DIAMETER — 6" MAXIMUM DEPTH OF DIE FILL — FULLY HYDRAULIC

- **Fully Hydraulic**—applies pressure to tablet with both upper and lower punches. Lower punch ejects tablet with full forming pressure.
- **Completely Automatic**—pushbuttons operate machine continuously or through a single cycle with an automatic stop position.
- **Accurate Dimensional Thickness of Tablets**—upper and lower punches come to a positive mechanical stop position, holding thickness of each tablet.
- **Always True Density**—upper and lower punches can be adjusted to come to a hydraulic pressure stop position, applying exact pressure on the tablet to give true density regardless of variation in die fill.
- **Perfect Punch and Die Alignment**—take-up bushings on tie bars permit punches and die to be held in perfect alignment.
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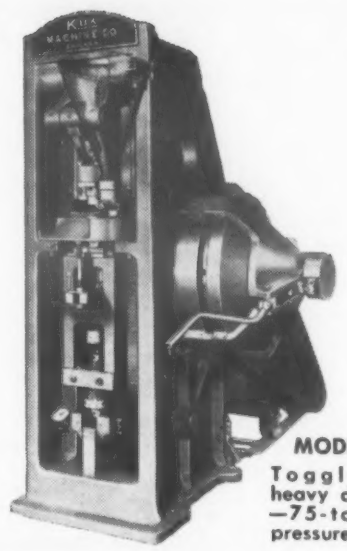
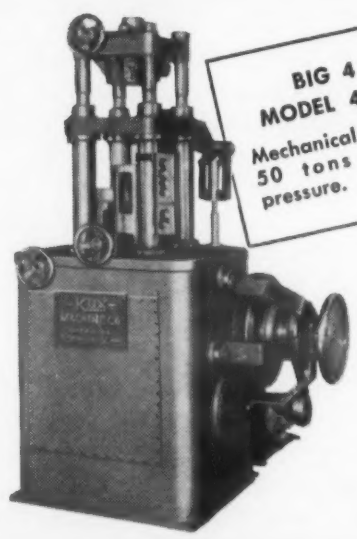
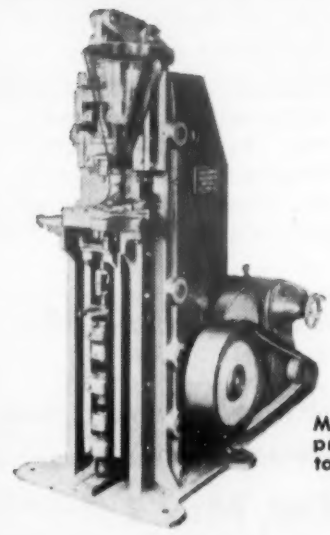
- **Quick, Easy Tool Changeovers**—because punches, die and core rod mountings are readily accessible.
- **Accurate Die Filling**—with hydraulically operated shuttle-type shoe. Controlled speed of movement.



MODEL 65B
Toggle type heavy duty press —75-ton total pressure.



BIG 4
MODEL 450B
Mechanical press 50 tons total pressure.



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M'A SHOW

11:00—"Metal Powders in Pyrotechnics and Explosives," J. SACHSE, Metals Disintegrating Co., Inc.

2:00 p.m.

Powder Metallurgy—Ballroom

2:00—"Superfine Iron Powders," M. W. FREEMAN, M. W. Freeman Co., and J. H. L. WATSON, Ford Institute for Medical Research

2:45—"Fundamentals of Powder Metallurgy," G. KUCZYNSKI, Notre Dame Univ.

3:30—"The Sintering of Iron-Copper-Carbon," P. ULF GUMMENSON, Hoeganaes Sponge Iron Corp.

4:15—"Powder Metallurgy in the Manufacture of Roller Chains," C. L. RICHARDS, Whitney Chain Co.

Exhibitors

Alloy Metal Powders, Inc.
American Society for Metals *(Metal Progress)*
Antara Chemicals Div., General Aniline & Film Corp.
Arnhold Ceramics, Inc.
Arnold Engineering Co.
Baldwin-Lima-Hamilton Corp.
Drever Co.
Easton Metal Powder Co.
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Haller, Inc.
Charles Hardy, Inc.
Harper Electric Furnace Corp.
Hoeganaes Sponge Iron Corp.
Ipsen Industries, Inc.
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MATERIALS & METHODS
New Jersey Zinc Co.
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Plastic Metals Div., National-U. S. Radiator Corp.
Precision Metal Molding
Republic Steel Corp., Metal Powder Div.
Sintered Metal Components, Ltd.
Stackpole Carbon Co.
F. J. Stokes Corp.
United International Research, Inc.
Vanadium-Alloys Steel Co.
Whitaker Metals Corp.

A Boeing B-47 Stratojet medium bomber gets a take-off assist from 30 Phillips Petroleum Company M15 JATOs.

N-A-X HIGH-TENSILE is readily formed and welded. Here, before welding, a worker sizes the container's aft head, drawn by a 250-ton press. Bottom forging is locked in.

N-A-X HIGH-TENSILE STEEL FORMS AND WELDS READILY

Formability: Even at the higher strength levels (50% greater than mild carbon steel) this material can be cold formed and drawn into very difficult stampings and cold formed shapes.

Weldability: Its weldability by any process is excellent, maintaining toughness through a wide range of temperatures. Under-bead cracking tests are excellent. Using American Welding Society standard bead-weld testing, shows under-bead hardness rises only to 95 Rockwell from 80-85 Rockwell prior to welding.

ONE POINT OF VIEW

Engineering aides: We need more

One of the common complaints of engineers is that they must spend too much of their time performing routine tasks that do not require the talents of a professional engineer. During the past several months we have published letters from readers suggesting that one way to eliminate this inefficient use of engineering manpower is for engineering departments to use engineering technicians or aides.

Roadblocks exist

We agree that this is an effective way of conserving our engineers' valuable (and expensive) time. Unfortunately, there are at least two obstacles in the way of wider use of engineering aides by industry. One of these is the reluctance of many companies to make use of them. Much of industry's reluctance stems from lack of knowledge about engineering aides and where and how they can be used. A common misconception is that their training and qualifications are comparable to those of vocational school graduates. But this is not true. Qualified engineering technicians receive at least one full year of post-high school training in an accredited technical institute. The program of instruction is essentially technological in nature and specifically designed to prepare them for work in the field of engineering.

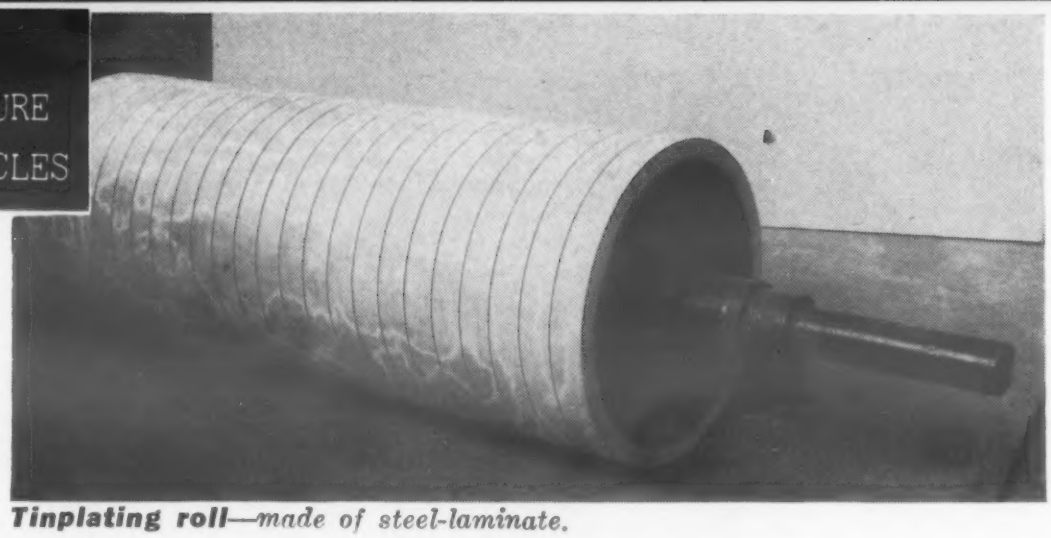
The other, and more serious, obstacle to wider use of engineering aides is the shortage of acceptable training facilities. At present only 32 institutions have curricula that are accredited by the Engineers' Council for Professional Development. Despite the present limited acceptance of engineering aides by industry, these few schools cannot meet the demands for qualified personnel. Demand will increase more rapidly as the rate of our technological advance increases.

But something's being done

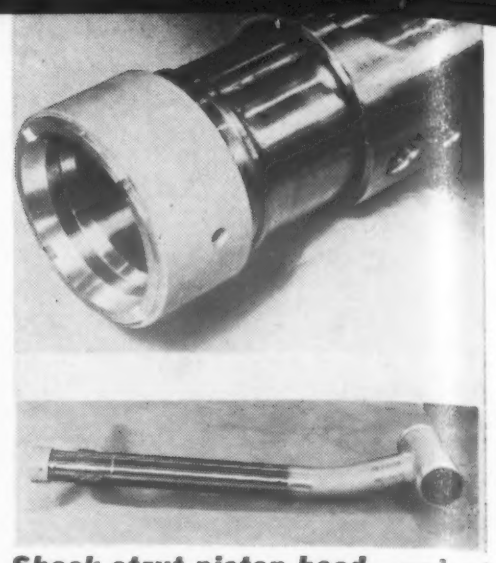
Until recently little time and attention has been given to the subject of engineering technicians. However, in the last twelve months there have been signs of activity. Early last year the Engineers Joint Council sponsored a conference on the engineering technician. Also last year, the President's National Committee for the Development of Scientists and Engineers organized a committee to establish a program for developing more and better qualified engineering technicians. Finally, the Technical Institute Div. of the American Society for Engineering Education has obtained money from the Carnegie Fund to undertake a study of technical institute education.

Activities such as these are a good beginning, and they are indicative of growing interest in the problem. We hope that they will quickly lead to much needed constructive action.

FEATURE ARTICLES



Tinplating roll—*made of steel-laminate.*



Shock strut piston head—*made of aluminum-laminate.*

Plastics Laminates Bonded to Other Materials

Thermosetting plastics laminates themselves provide a wide choice of properties but sometimes they work better when combined with other materials such as steel, aluminum or rubber.

by Norman A. Skow, *Director of Research, Synthane Corp.*

■ The advantages, as well as the limitations, of high pressure plastics laminates are rather well known (see M&M, Feb '57, p 121-140). But combine them with other materials such as steel, aluminum, copper, rubber, cork, plastics films or vulcanized fibre and the result is essentially new materials combining the desirable properties of plastics laminates with those of the material to which it is bonded. Thus the designer can specify a combination of physical, mechanical and electrical properties that is unavailable in a single engineering material.

Specific design advantages offered by combination laminates include:

1. Better strength-weight ratios.
2. Increased resistance to corrosion and chemicals.
3. Greater range of electrical characteristics.
4. Dimensional stability over a wide temperature range.
5. Increased rigidity and strength for soft sealing materials.
6. Improved bearing surfaces.
7. Greater range of frictional characteristics.
8. Improved fabrication characteristics, and reduced production costs.

Materials and forms available

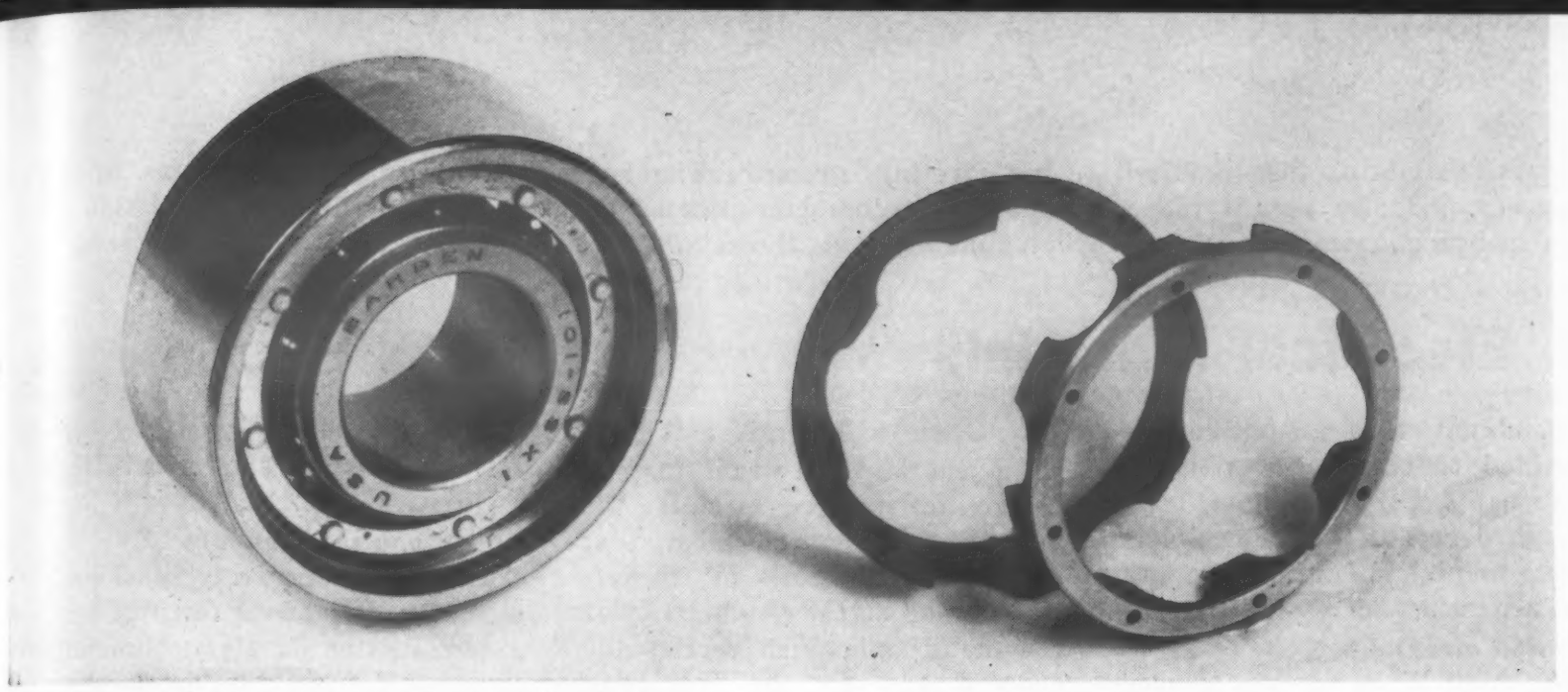
Theoretically any material can be combined with plastics laminates by adhesive bonding. However, because of similarities in design requirements for various types of end uses, several combinations have become somewhat standardized.

The most common plastics laminates used are the paper-base phenolics such as NEMA Grades XXXP, XX, XXP and XP. Grade G-10, epoxy-glass, has received increasing attention for printed circuit applications. Fabric-base phenolics, such as Grades C and L, are used where impact resistance is required or where impregnants such as graphite or molybdenum disulfide are used to provide self-lubricating qualities. For specialty applications, melamine laminates may be specified where better arc or alkali resistance is required, or silicone laminates where exceptionally high temperatures are to be encountered.

The most common materials supplied in combination with plastics laminates are: copper, natural and synthetic rubbers, cork, steels, aluminum alloys, vulcanized fibre, and polyester and cellulose acetate films. Two grades of plastics laminates can be bonded together where the properties peculiar to each are required.

Adequate bonding of combination laminates is always an important consideration. However, for certain types of materials adhesive formulations have been developed to the point where the actual strength of the bond is seldom a problem.

Combination laminates can be specified in sheet, rod or tube form. In sheet form, the plastics laminate can be specified on one or both sides, or sandwiched between lamina of the other material. Where a tubular form is used, the combination material usually consists of a plastics laminate covering a metal tubular core. In rod form a solid core of one of many types of metal can



Bearing retainers—*made of aluminum-laminate.*

be covered with a laminate.

Sizes of materials available are limited by the facilities of the materials supplier. Synthane, for example, is producing combination sheets in standard 36 x 36-in. sizes. Facilities are also available for producing sheets in 36 x 72 and 24 x 96-in. sizes. Tube o.d.'s range from ¼ to 26 in., and lengths up to 36 in. In some sizes lengths up to 96 in. can be provided, and greater lengths can be obtained by making use of mechanical joints.

Use them as 1. Structural Materials

Steel or aluminum in combination with plastics laminates is usually used where structural strength is required. Sometimes Grade XX paper-base laminates are used with metals, but more commonly either coarse or fine-weave cotton fabric laminates are used for optimum strength.

Plating rolls

A variety of design requirements exist in the different types of rolls used for electrolytic tin plating of steel strip. The rolls control a 42-in. wide continuous strip of steel which is pickled, plated and polished while traveling at speeds up to 4100 ft per min.

Developed in cooperation with Steel Plant Equipment Corp., the rolls replace the conventional rubber covered rolls. They consist of steel cores covered with fabric reinforcement impregnated with several types of resins. The selection of the fabric and the resin is dependent on the needs of each individual roll. Bridle rolls, which prevent the steel sheet from buckling as it uncoils, have hard, abrasion resistant surfaces. Holddown rolls are made to withstand effects of sulfuric acid at temperatures up to 200 F. This laminate also insulates the roll from the electric current, preventing electrolytic deposition of tin on the rolls. Wiper rolls are formed with a surface soft enough to remove moisture, yet firm enough to resist wear.

In service, the laminate-covered rolls last more than three times longer than the rubber-coated rolls. Also, in comparison with the rubber rolls, they are more resistant to acids; denser, eliminating embedment in the rolls of foreign particles which might mar the surface of the plate; and tougher, reducing the extent of edge cutting and gouging that results in excessive vibration and chatter during the high speed plating operation.

Shock strut piston heads

A fabric-base phenolic laminate bonded to a 2024 aluminum tube forms a hydraulic piston head in aircraft shock struts developed by Cleveland Pneumatic Tool Co. The shock strut utilizes piston-activated hydraulic fluid and compressed air to absorb the impact of a plane's initial contact with the ground. The pistons in the strut must be lightweight, mechanically strong, shock resistant, impervious to hydraulic oils and stable over a wide temperature range. The most important reasons for using a plastics laminate bonded to aluminum are to eliminate metal-to-metal contact between the head and the cylinder and to prevent scoring of the cylinder wall by impurities in the hydraulic fluid. The laminate is sufficiently resilient to permit impurities to embed themselves in the laminate instead of abrading the sealant wall. This combination material is being used as piston heads in sizes ranging from 3 to 10 in. dia.

Precision bearing retainers

Retainers for precision bearings produced by the Barden Corp. also make use of the stability, strength and light weight of an aluminum-laminate combination. Retainers are machined from a combination sheet consisting of a plastics laminate with an aluminum facing bonded to one surface. The re-

tainers maintain the required accuracy and also permit reduction in bearing size while retaining riveting strength. The heat dissipation characteristics of the aluminum permit the retainers to be used at temperatures up to 300 F continuously and 350 F intermittently.

2. Electrical Materials

Combination laminates can be specified to obtain a variety of electrical properties ranging from a high degree of surface conductivity to high dielectric strength and arc resistance.

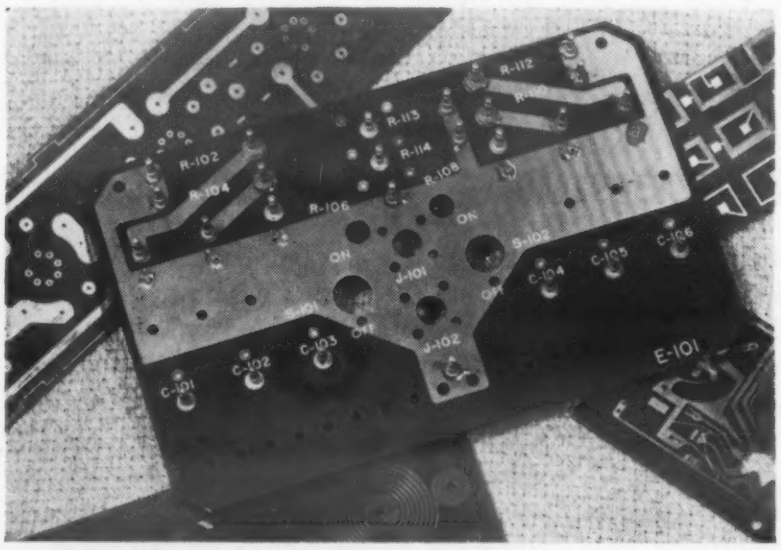
Printed circuits

Probably the most widely used electrical combination material is the copper faced laminate used for printed circuits. Since a great deal has been published about this type of application (see M&M July '55, p 94; Feb '57, p 136). little space will be given it here.

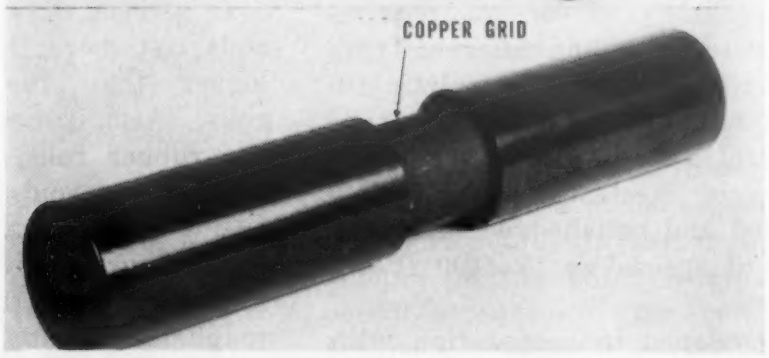
In general, when specifying materials for printed circuits, the engineer should remember that over-all requirements of the circuit depend on the conductivity of the metal foil which carries the current and on the insulation resistance, chemical resistance, moisture absorption characteristics and mechanical properties of the base laminate. The adhesive must provide good bond strength and high surface resistivity as well as resistance to blistering when the circuit elements are soldered.

Telephone relay spools

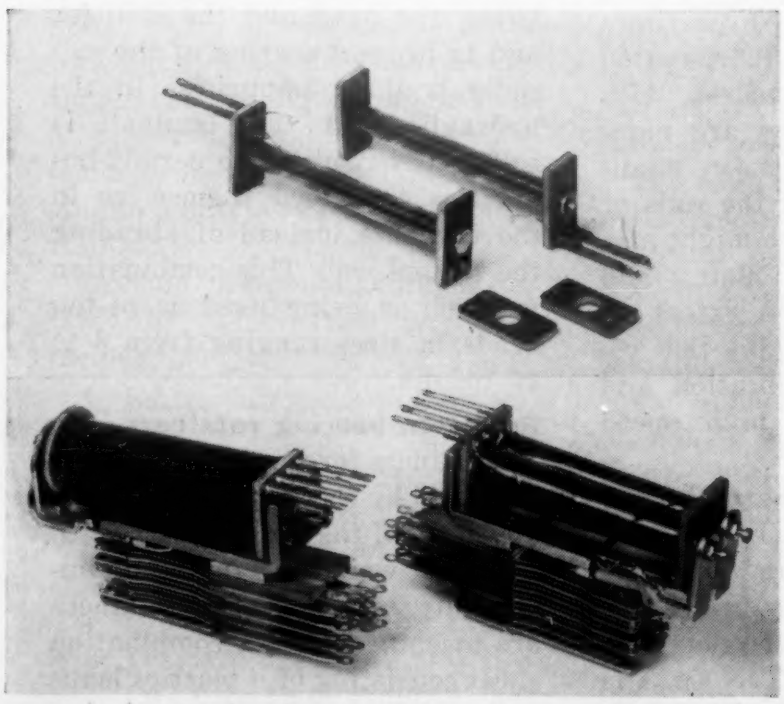
In a telephone relay spool produced by Stromberg Carlson Div. a combination of Mylar film and Grade XXP laminate is used as end plates. The plastics laminate provides required structural strength as well as dielectric properties; the polyester film serves as a moisture barrier. Barriers are necessary to prevent



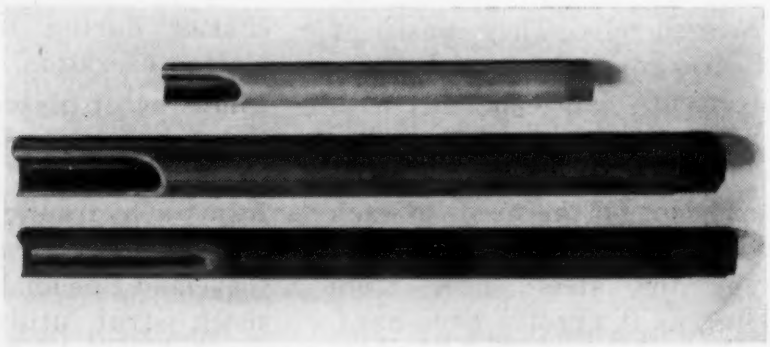
***Printed circuit**—made of copper-laminate.*



***Circuit breaker bushings**—made of copper-laminate.*



***Relay spool end plates** — made of polyester film-laminate (top). Below is finished telephone relay spool.*



***Fuse cases**—made of vulcanized fibre-laminate.*

corrosion of the wiring on the spool. Acetate washers were originally used; however, the combination of film and laminate as an integral unit provides a substantial labor saving in production.

Circuit breaker bushings

In bushings for three-phase circuit breakers manufactured by I-T-E Circuit Breaker Co., graphite-impregnated plastics laminates and copper are used to provide a combination of insulation and conduction. A graphitized phenolic layer is deposited on the i. d. of the laminated tube to provide corona protection when a copper protector bar is inserted. The laminated tube is then wound in the conventional manner, and at a specified position in the wall copper foil approximately 0.0015 in. thick is inserted to supply the necessary ground shield. The tube is machined to expose a portion of the ground shield which is then coated with graphitized resin to provide positive contact. The ground shield permits equalization of the electrical charge throughout the bushing.

Fuse cases

Electrical distribution transformers serving residential areas are protected by power fuses rated up to 12,000 amp interrupting capacity. Power fuses made by the R. & I. E. Equipment Div. of I-T-E Circuit Breaker Co. are protected by a fuse case made of phenolic tubing lined with vulcanized fibre. When the elements melt and the ends arc under short circuit or overload conditions, the fibre is heated and generates sufficient gas to snuff the arc. The fibre also prevents the arc from "tracking." The plastics laminate protects the fibre from moisture and contributes the mechanical strength necessary to protect the fibre lining from distorting or rupturing.

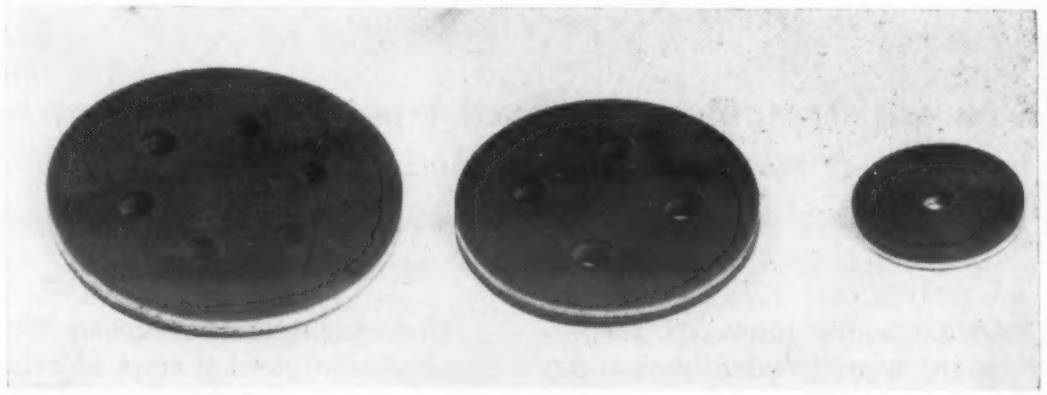
3. Sealing Materials

Laminates bonded to cork or to a variety of types of rubber can be used where soft sealing characteristics must be coupled with rigidity. In addition to Red Buna S, chloride and sulfate-free Buna S are available in combination with plastics laminates where this type of purity is essential. Other rubbers that can be combined with plastics laminates include Buna N, a nitrile type rubber with good oil resistance and freedom from chloride and sulfates, and neoprene, which has good oil and heat resistance.

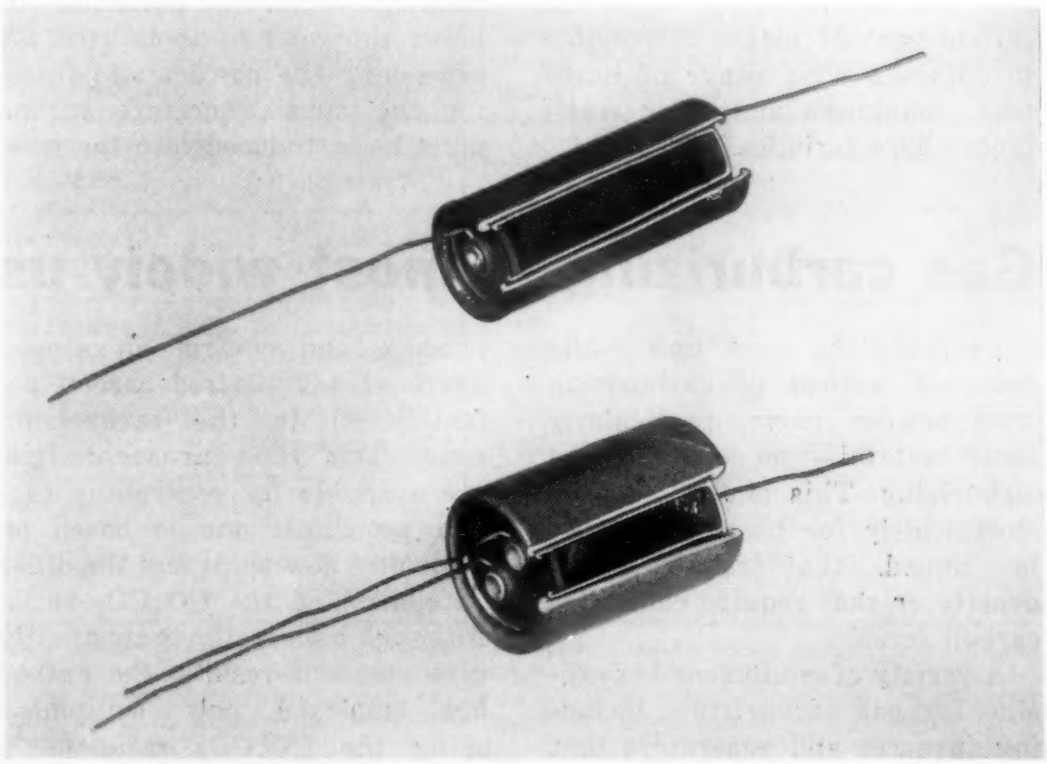
Condenser seals

Washers consisting of Grade XP laminates bonded to Red Buna S rubber are used by Ajax Condenser Co. as end seals for aluminum cans encasing electrolytic condensers and capacitors. The most common washer consists of a 3/64-in. thick laminate bonded to a 1/32-in. thickness of rubber. The laminate side of the washer rests on a bead on the interior wall of the can and the aluminum is spun down into the rubber, forming a hermetic seal. Terminals entering through punched holes in the washer are riveted, also providing hermetic seals against the rubber.

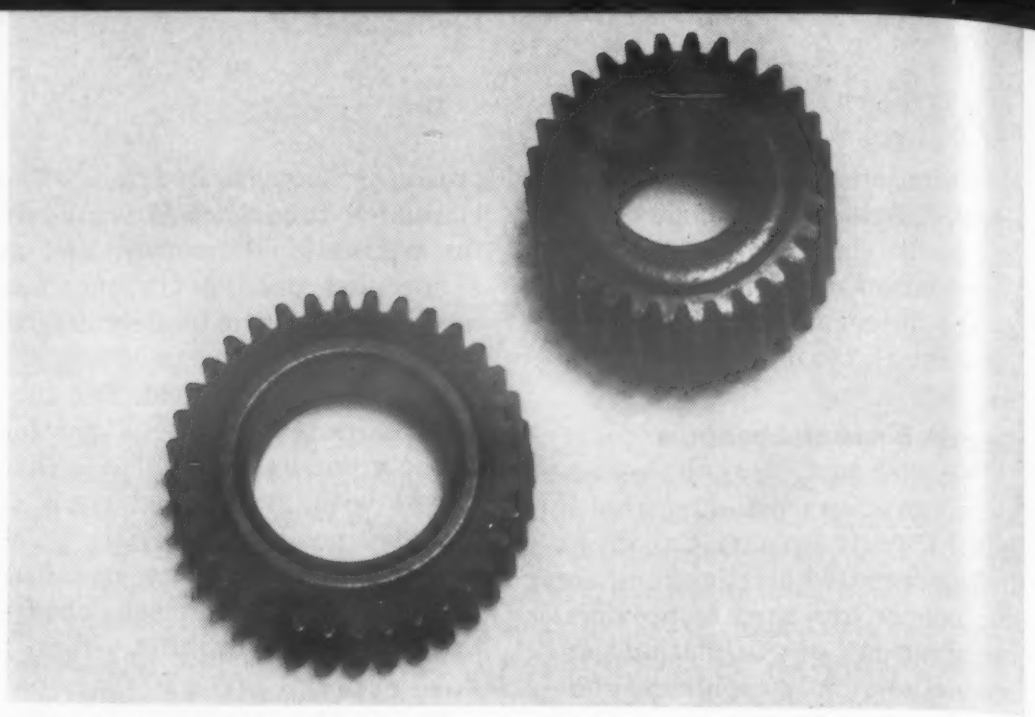
In oil field capacitors neoprene is used instead of Red Buna S because of its superior oil resistance. Prior to the introduction of these rubber-laminate washers, wax was used to seal capacitors and condensers. Labor costs were relatively high and wax seals tended to deteriorate over long periods of time.



Condenser seals—*made of rubber-laminate (above). Cut-away views of assembled condensers are shown below.*



Six gas carburized parts



1 **Commercial class 4 gears** *pressed from electrolytic iron powder to a minimum density of 7.5 gm per cu cm, carburized at the 0.90% carbon level to a depth of 0.030 in., and tempered to Rockwell C45-50.*

What you should know about Carburized

You can strengthen iron powder parts by adding carbon, but there is more than one method. The method you choose will have an important effect on the properties of the finished part.

■ Demands for improved properties in iron powder parts can frequently be met by modifying the composition of the part. Carbon is the most effective element that can be added; control of the carbon content makes it possible to obtain a wide range of hardness, toughness and wear resistance characteristics.

Unfortunately the carbon content of iron powder must be relatively low so that the particles are soft and ductile enough to be easily pressed into shape. In addition, the softer the particles, the lower the wear of tools used for processing the powder and forming the parts. Therefore, carbon must be introduced into the powder mixture or into the part after it has been pressed.

There are several methods of introducing carbon into a powdered iron part. They include carburizing by gas, liquid salt bath or pack methods, and mechanical mixing followed by heat treatment. Each has its particular advantages and limitation.

Gas carburizing is most widely used

Probably the most universally accepted method of carburizing iron powder parts, particularly those containing no copper, is gas carburizing. This method is used most widely for parts that must be coined, that require high density or that require controlled carbon levels.

A variety of equipment is available for gas carburizing, including furnaces and generators that produce and control an atmosphere at any desired carbon potential within the carburizing range. Two basic furnace designs are available for controlling carbon potential; one is based on control of dew point and the other on control of the $CO:CO_2$ ratio. Although both methods apparently give excellent results, the author has employed only equipment using the $CO:CO_2$ ratio as a method of carbon potential control, specifically a Leeds and Northrup furnace having Microcarb control. This type of furnace is very reliable and consistently controls carburization within $\pm 0.03\%$.

An accompanying table compares the mechanical properties of electrolytic iron parts carburized to several carbon levels with the properties of AISI steels hav-

2 ***Precision class 1 gears*** *pressed from electrolytic iron powder to a minimum density of 7.5 gm per cu cm, through carburized at the 0.45% carbon level, and tempered to Rockwell C48-52.*

3 ***Business machine part*** *pressed from electrolytic iron powder to a min density of 7.1 gm per cu cm and carburized at the 0.90% carbon level to a depth of approx 0.005 to 0.008 in. Full hard surface required for wear resistance.*

Iron Powder Parts

by W. J. Doelker,
Chief Metallurgist, Supermet Div., Globe Industries, Inc.

ing similar carbon contents. These figures do not give a true comparison because the metal powder test bars were carburized through only about 80% of the cross section, but they indicate the possibilities. Tensile and yield strengths of the carburized and hardened iron powder parts closely approximate those of the corresponding steels, but their ductility is lower.

Advantages

Clean, uniform parts—Gas carburizing is an extremely clean, uniform method of heat treating iron powder parts. It leaves no salts or other foreign material in the pores — a characteristic of some other methods, particularly on medium or low density parts. The integrated quenching bath usually found with this type of equipment makes it possible to carburize, cool to the proper quenching temperature, and quench the parts—all under the protection of the same atmosphere.

Homogeneity — High density iron powder parts can be homogeneously carburized if they are not so thick that the process is uneconomical.

Carbon control — Any desired carbon level can be obtained through use of carbon potential control equipment.

Close tolerances — In making high density electrolytic iron powder parts, size variations can often be held to very close tolerances. Close dimensional control results from several factors: 1) since these high density parts are solid for practical purposes, uniform expansion occurs on heating, 2) use of a high sintering temperature leaves the parts in a fully annealed and stress relieved

CARBURIZED IRON POWDER PARTS VS WROUGHT CARBON STEELS [a, b]

Material[a]	Heat Treatment	Tensile Strength, 1000 psi	Yield Strength, 1000 psi	Elong, %	Rockwell Hardness
Iron Powder (0.95%C)	Oil quenched,	170	160	1	C48
AISI C-1095	tempered at 600 F	182	119	10	C42
Iron Powder (0.95%C)	Oil quenched,	138	120	2	C36
AISI C1095	tempered at 800 F	175	112	12	C36
Iron Powder (0.95%C)	Oil quenched,	100	86	4	C25
AISI C1095	tempered at 1000 F	158	98	15	C31
Iron Powder (0.80%C)	Oil quenched,	160	155	4	C46
AISI C1080	tempered at 600 F	189	143	11	C39
Iron Powder (0.40%C)	Oil quenched, tempered at 400 F	125	104	3	C50
AISI C1040	Water quenched, tempered at 400 F	130	97	16	C51

[a]Iron powder is electrolytic type, pressed to a minimum density of 7.5 gm per cu cm. Carbon contents inficated for iron powder test bars were obtained by carburizing.
[b]Metal powder parts tested on bars having ¼ by ¼ in. cross section; steel properties are for bars ½, 1, 2 and 4 in. round. Data therefore indicate only relative properties of the materials.

condition, and 3) closely controlled carburizing conditions yield uniform and predictable dimensional changes.

Many parts, particularly the smaller ones, are held to a total tolerance of 0.0005 in., and a tolerance of 0.001 in. is commonplace on most parts. For example, a small, heat treated precision gear with a production rate of about a million per year is held to an A.G.M.A. precision, fine pitch gear standard of Class 1, i.e., a maximum total composite error of 0.001 in. and a maximum tooth-to-tooth composite error of 0.0004 in.

Case depth control—It is possible with high density parts to hold the case depth within relatively close limits. With carbon potential control, the case can be held to any given carbon level but, as in all carburizing operations, the level drops from the surface to point of deepest penetration.

Gas carburizing, like other methods, carburizes low and medium density parts all the way through. On medium density parts of heavy section it is possible with carbon potential control to generate a case having a specified carbon level, but the depth cannot be accurately controlled.

Disadvantages

Copper barrier — During infiltration or sintering, any copper that does not alloy with the iron spreads over the surface and acts as a shield that carbon monoxide cannot penetrate. Parts containing copper, whether added to the powder blend or as an infiltrant, will not carburize uniformly because of this shielding effect; the gaseous atmosphere has no stripping effect on copper.

Quenching baths limited — Because of the effect of water vapor upon the carbon potential of the atmosphere, integrated quenching baths in gas furnace units are restricted to oil or liquid salts. However, this limitation is usually not too serious, as there are a variety of oils having quenching rates close to that of water. The majority of powder metal parts are relatively small, and a fast quenching oil will quench them at a rate sufficient to develop the desired hardness.

Liquid carburizing is best for iron-copper parts

Iron powder parts containing copper added either in the powder blend or by infiltration are usually carburized by the liquid method.

Advantages

Copper removal—The salts used in liquid carburizing have a high affinity for copper and strip it from the surface of the iron, thus exposing the surface to the carburizing action of carbon monoxide generated in the salt bath. This is a major advantage because other methods of carburizing are relatively ineffective when used on parts containing copper.

Case depth control—Liquid carburizing can be used very successfully on high density parts to maintain a case depth to a high degree of accuracy.

The liquid method usually carburizes low and medium density parts all the way through because of their porosity. However, the high carburization rate characteristic of liquid carburizing makes it possible to form a carburized case on medium density parts of heavy cross section. The process is not controllable to the extent that specific case depths can be generated and maintained within close limits.

Disadvantages

Salt penetration — The major disadvantage of liquid carburizing lies in the fact that most iron powder parts are porous and allow the liquid salts to penerate into the compact. Upon quenching, the salts solidify, and the nature of the pores makes it practically impossible to remove them from within the part. Carburizing salts are normally hygroscopic, and the water pick-up tends to create an accelerated corrosion condition that often makes it impossible to use the parts. This problem is confined primarily to low and medium density parts; high density parts do not have intercommunicating porosity, and it is possible to wash them completely free of salt.

Lack of carbon control—Carbon concentration cannot be controlled in liquid salt baths, i.e., carburization takes place at a concentration normally somewhat in excess of 1.0%. Where a case can be generated, the normal gradation of carbon content from surface to point of deepest penetration occurs, but the surface always tends to have a carbon concentration of more than 1%. If parts were to be homogeneously carburized, the carbon content would have to be in this range, rather than 0.4, 0.6 or 0.8% as can be achieved by gas carburizing.

Pack carburizing is used to harden coined parts

Pack carburizing can be used advantageousiy to carburize iron powder parts, but is gradually being replaced by the cleaner, more economical gas carburizing methods. It is used primarily to harden parts after coining.

Advantages

Clean parts — Pack carburizing eliminates the problem of entrapment of foreign material in the pores of medium or low density compacts that occurs when liquid baths are used.

Selective hardening—Parts can be carburized, cooled in the pack at a rate slow enough to prevent hardening, and subsequently local-

ly reheated and quenched to obtain hardness at specific points rather than over the entire part.

Disadvantages

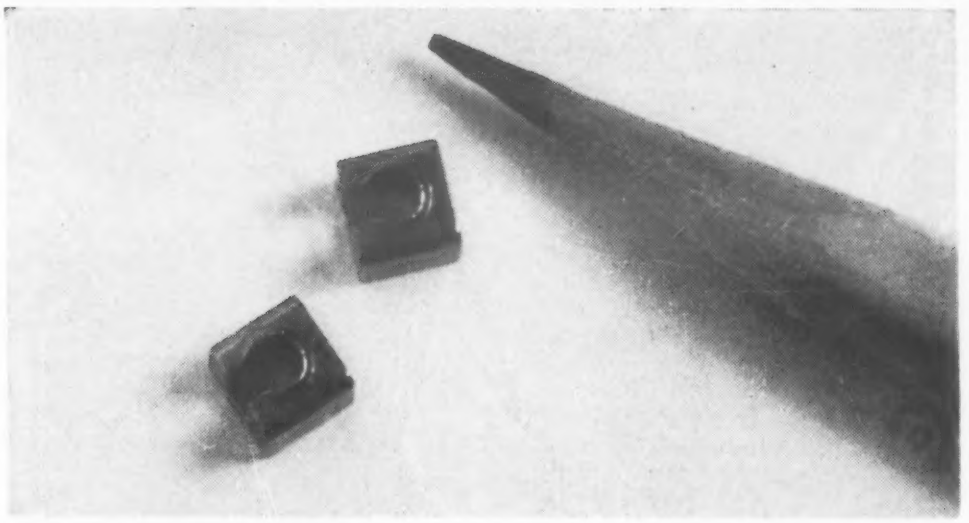
Copper barrier—Pack carburizing is not recommended for parts in which copper is used, either as an additive to the powder blend or as an infiltrant, because the copper acts as a barrier to carburizing. The materials used in this process do not react with copper to strip it from the iron particles, and spotty and uncontrollable penetration results.

Poor case depth control—When low and medium density parts are carburized by the pack method, they are carburized all the way through, because of their porosity. Some semblance of a case might be obtained on heavy sectioned, medium density parts by very close control of the carburizing cycle, but it would be practically impossible to control such a case within relatively close limits.

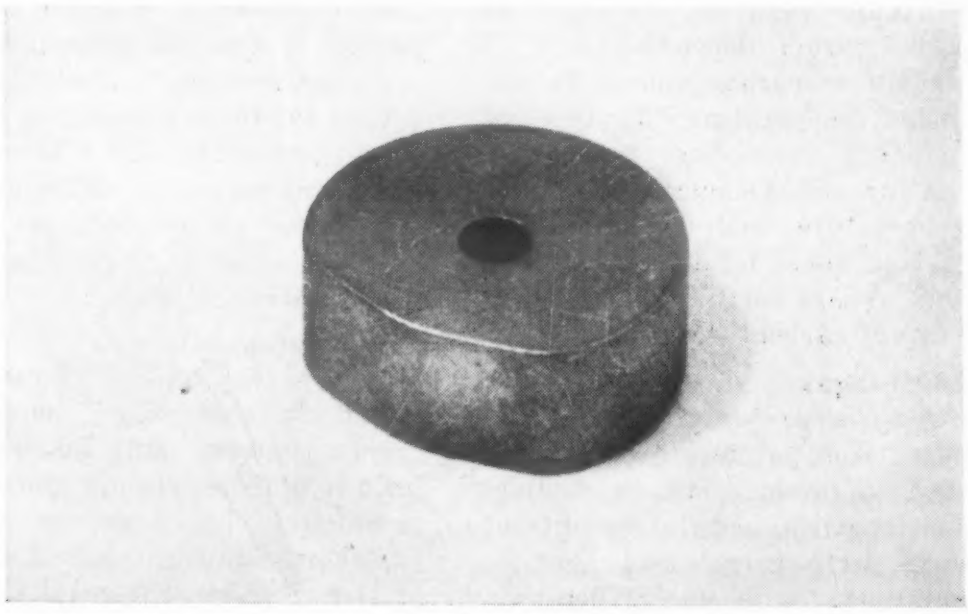
Limited carbon control—Carbon concentrations are normally in excess of 1.0% because the packing material is designed to develop and maintain such a potential. It is impossible to control the carbon potential at a lower level because of constant changes as the carburizing material burns out.

Decarburization—This is an extremely important factor. The carbon potential of the atmosphere generated by the carburizing material decreases as the temperature drops. As a result, parts made of high purity iron powders (e.g., electrolytic), which are pack carburized and allowed to cool in the pack, suffer severe surface decarburization. Investigation indicates that parts made of electrolytic iron tend to decarburize as fast as, if not faster than, they carburize, probably because electrolytic iron contains no impurities or alloying elements that tend to slow down decarburization.

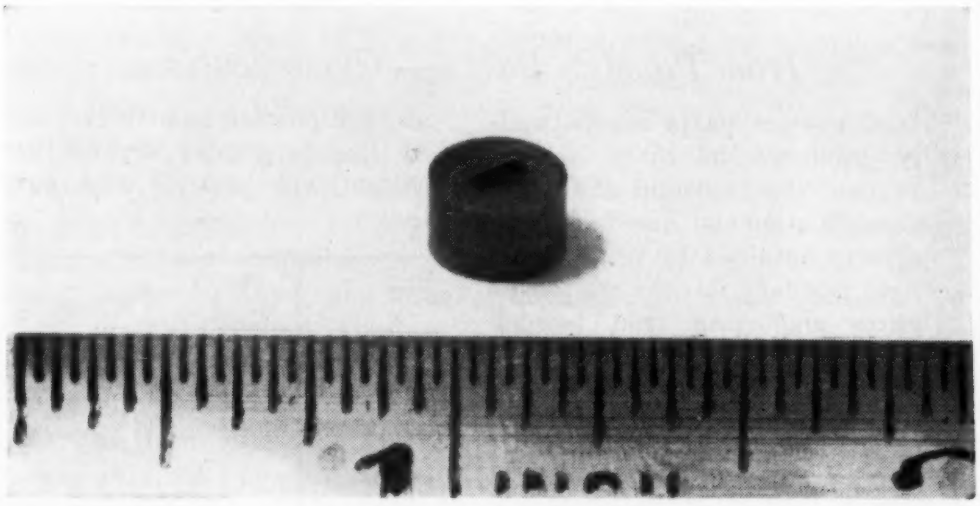
If the parts are quenched directly from the pack, most of this trouble can be eliminated, but exposure to air during transfer from pack to quench can produce slight surface decarburization. High density parts made from



4 **Cigarette lighter parts** *pressed from electrolytic iron powder to a minimum density of 7.0 gm per cu cm and carburized at the 0.90% carbon level to a case depth of approx 0.007 in. Full hard surface required for wear resistance.*



5 **Cam** *pressed from reduced iron powder to a minimum density of 6.9 gm per cu cm and carburized at the 0.070% carbon level. Case depth not specified because low density leads to uncontrollable penetration. Carbon level selected to obtain a surface combining wear resistance with toughness.*



6 **Coupling** *pressed from electrolytic iron powder to a minimum density of 7.0 gm per cu cm and carburized at the 0.90% carbon level to a depth of 0.015 in. (hardness: Rockwell C60 min). On this part concentricity is held to 0.001 in. max TIR.*

electrolytic iron can be quenched from the pack and a satisfactory surface with controlled case depth maintained.

Reduced iron powders that contain manganese, silicon, sulfur, phosphorus and possibly other metallic elements do not appear to be as susceptible to this reaction, although it is possible that decarburization could occur in such parts also.

Mechanical premixing gives more ductile parts

This method of adding carbon to iron powder parts is widely used in producing low and some medium density parts. Carbon is added, usually as finely divided graphite, directly to the iron powder blend. Parts are pressed to shape with this uniformly distributed carbon as an integral part of the compact. Alloying of the carbon takes place during the sintering operation, the extent of carburization depending on: 1) amount of carbon added, 2) sintering temperature, 3) type of reducing atmosphere present in the furnace, 4) length of time at temperature, and 5) amount of carbon monoxide and rate at which it is generated by the particular form of carbon used.

Advantages

Limited carbon content — Reduced iron powders are normally used to produce low or medium density parts, and the ductility of such parts is relatively low in comparison with steel. When they are carburized to a high carbon level, such parts have practically no ductility, even if they are not fully hardened. Mixing is usually employed when a combined carbon content of less than 1% is desired to modify the brittleness commonly associated with carburized and hardened parts of low or medium density. The lower combined carbon level results in an increase in strength together with retention of some ductility.

Low cost—Carburization occurs as part of the sintering cycle, thereby reducing the cost. Addition of carbon or graphite to the powder is a simple procedure.

Easier pressing—Admixture of carbon improves lubrication properties, promoting easier pressing.

Greater porosity — Burn-out of the carbon or graphite particles helps produce a highly porous product when desired.

Disadvantages

Poor carbon control—To obtain maximum control of combined carbon content, many fabricators have established rigidly controlled techniques. There are so many variables, however, that it is almost impossible to control within close limits the amount of carbon that combines with the iron. Slight variations in the major control factors of sintering temperature and time, atmosphere composition, and type and amount of carbon added to the powder blend have pronounced effects upon combined carbon content.

Coining difficult — Combination of carbon with the iron in the sintering operation produces a part that is hard and tough, similar to a high carbon steel. It is exceedingly difficult to coin such a part to any appreciable extent. Therefore, it is normally advisable to use this process for parts that do not require coining to control dimensions or increase density.

Residual carbon — Depending upon the amount of carbon added and the sintering conditions, some uncombined or unburnt carbon may be present in parts carburized after premixing. Residual carbon may or may not be a disadvantage. If lubricating properties are desired, the presence of free carbon or graphite may be decidedly advantageous. If strength is of prime importance, the presence of these particles is a disadvantage, as they tend to create planes or areas of weakness. The presence of additional voids created by carbon burn-out may also be a disadvantage when porosity is not a requirement.

Infiltration difficult—Parts that are to be subsequently infiltrated with copper to develop additional strength may pose a problem if they have been carburized after premixing. It is well known from copper brazing work that copper will not adhere as satisfactorily to steel having appreciable carbon content as it will to low carbon steel. Similarly, in high carbon iron powder parts infiltrated with copper it is possible that the copper actually acts only as a filler material, and the additional strength normally resulting from alloying of copper and iron is not obtained.

Iron Powder Parts — Classification

Iron powder parts are normally produced in three density ranges: low, medium and high. Classification is based on the density obtained by using 100% iron powder; it does not cover parts employing iron powder mixed or infiltrated with copper. In iron-copper parts the higher specific gravity of copper leads to erroneous and confusing density figures, because the density depends on the relative weights of iron and copper present. Sufficient copper can be added to an iron powder base to increase its specific gravity beyond that theoretically possible with pure iron.

Class	Density, gm/cu cm		Porosity, %	
	Max	Min	Max	Min
Low Density	6.5	—	—	17.3
Med Density	7.2	6.5	17.3	8.5
High Density	7.65[a]	7.2	8.5	2.5

[a]Practical limit at present.

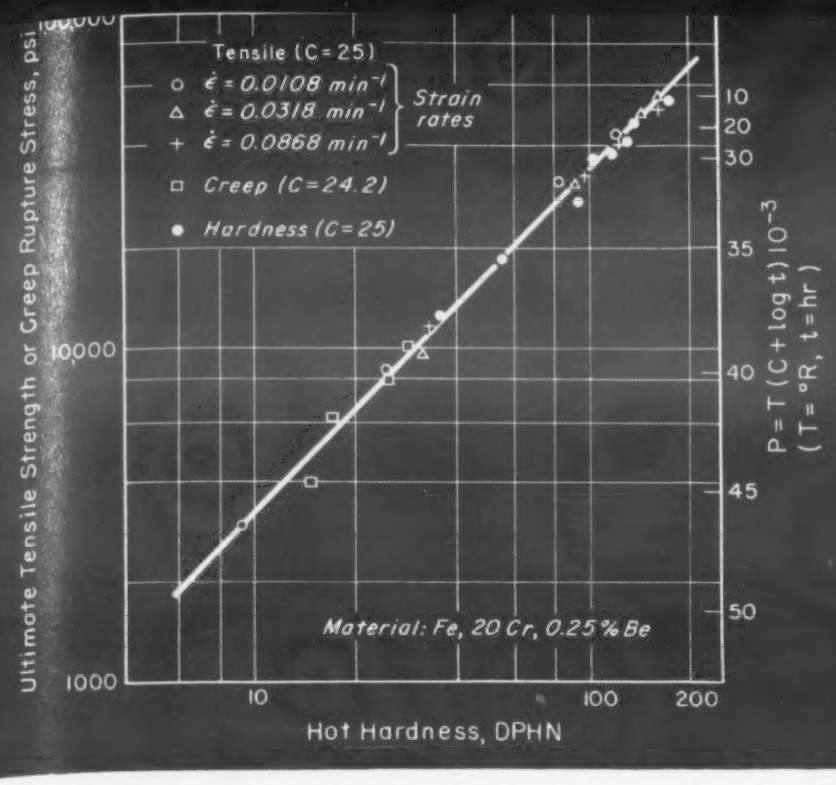


Fig 1—*Final result of Battelle research is a straight-line relationship between creep rupture stress and hardness. If either time or temperature is fixed, the other can be calculated from the right-hand scale.*

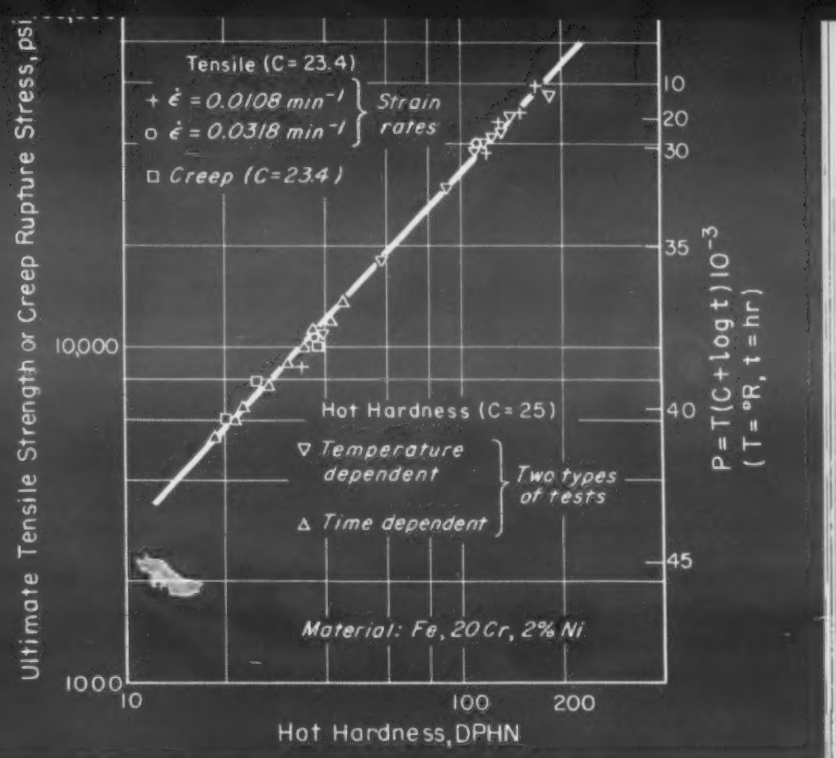


Fig 2—*Curve similar to Fig 1, but plotted for another alloy. On these graphs hardness, as well as tensile strength or creep rupture stress, can be read as a function of time and temperature.*

These curves show how you can determine . . .

Creep Properties from Short Time Tests

by Ervin E. Underwood,
Ass't. Division Consultant, Battelle Memorial Institute

The curve of Fig 1 (or Fig 2) represents a new correlation between hot hardness and strength properties. It can be read in two different ways:

1. If we ignore the right vertical axis entirely and the words "creep rupture stress" on the left vertical axis, what remains is simply a plot of ultimate tensile strength vs hot hardness.

2. If we ignore the words "ultimate tensile strength," we have a two-way plot: we can read creep rupture stress vs hot hardness, and we can also read a value of the parameter P for each rupture stress. This parameter introduces time and temperature, variables which are important in creep but not usually considered in determining ultimate strength by the tensile test. Using this parameter, we can assign a value either to time-to-rupture or to temperature, then calculate the other.

In other words, the meaning of the graph is this: if we know the hot hardness of this particular alloy, we can determine not only the ultimate tensile strength but also the creep rupture stress and the time-to-rupture at a given temperature.

How graph was obtained

The correlation curve of Fig 1 was obtained from standard tests yielding hot tensile strengths, creep rupture stresses and hot hardnesses. Typical data appear as in Fig 3 when plotted simply against the temperature. The stress to cause rupture falls on a vertical line at 1200 F because time is not considered. When these same data are replotted against the parameter P, they fall into two distinct curves (see Fig 4). Note that the tensile tests conducted with different strain rates now yield the same curve. Actually, for practical use, one strain rate would suffice.

In order to justify plotting hardness against P, the time dependency of the hardness data should be demonstrated. (In Fig 1 we can completely ignore the left vertical scale and read hot hardness vs P.) This dependency is shown in Fig 6. However, for most purposes, a normal hardness test with a fixed time is all that is needed. The two sets of hardness data plotted in Fig 5 show that the same hardness curve results whether time or temperature is the variable.

Now that tensile, creep and hardness have been plotted vs P, it is clear that the two curves are parallel and that the sharp break occurs at the same value of P for both the strength and the hardness curves. The flat portion of these curves corresponds to low temperature behavior; the steep portion is associated with a high temperature mechanism of deformation where recovery is operative. The sharp break corresponds to the equicohesive temperature, which may now be thought of

more accurately as the equicohesive parameter point.

The final curves of Fig 1 and Fig 2 are obtained readily from those of Fig 4 and Fig 5 by plotting strength vs hardness at the same P values. Specifically, the horizontal and left vertical scales of Fig 1 are labeled first; then the right vertical or P scale is established by reading opposite any point on the strength curve of Fig 4 the corresponding value of P. The final curve itself can be determined from any two points on either curve (strength or hardness) of Fig 4.

This strength-hardness correlation was developed as a result of research at Battelle on high purity, single phase alloys. Research has since been extended to poly-phase alloys. The similarity of curves of hardness and strength properties vs temperature permits us to predict the general validity of the correlation for the more complex alloys.

If this is true, a master curve can be determined for any alloy by running a few ultimate tensile strength tests, a hardness test, and two or three short creep tests. Then, within the limits of validity of the time-temperature parameter, the short hot hardness test can indicate creep rupture stress or tensile strength. These limits of validity are unknown at present, but for most applications this strength-hardness correlation appears to have wide potentiality as it exists now.

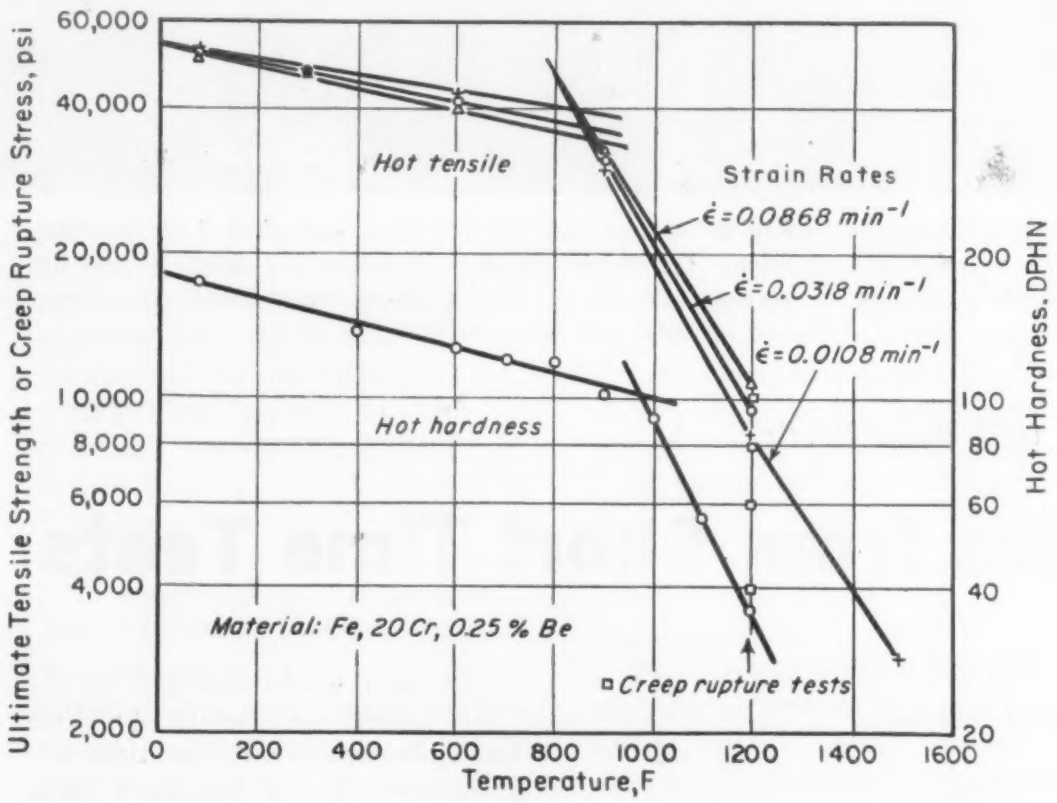


***Fig 3**—Curves obtained by plotting test results against temperature, thereby neglecting time.*

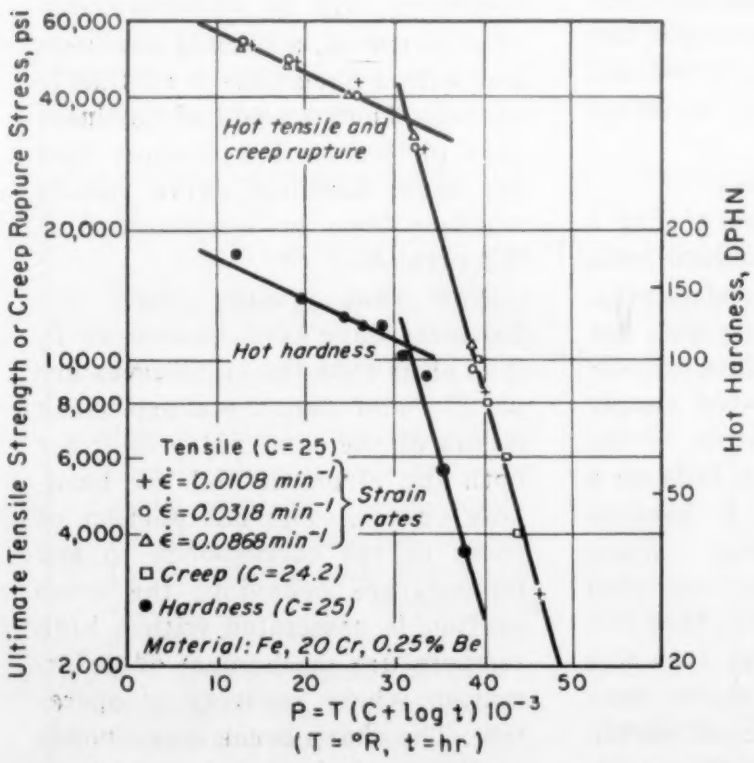


***Fig 4**—Curves obtained by plotting test results vs a parameter involving time and temperature.*

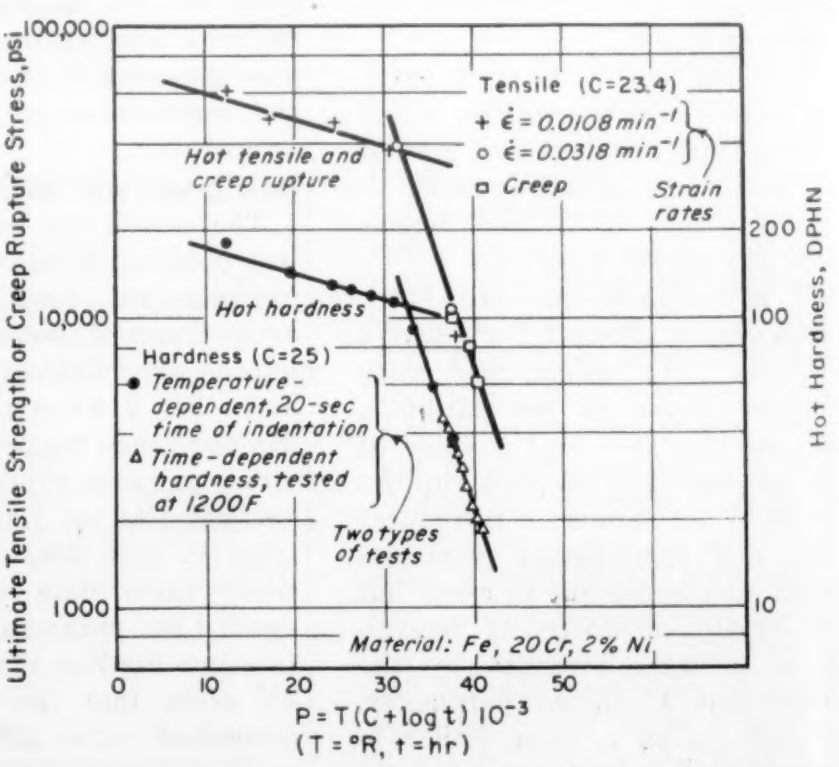


***Fig 5**—Test results for second material with time-temperature dependence of hardness made explicit.*

The background

It is well known that a more or less direct proportionality exists between the tensile strength of a wide variety of steels and the room temperature Brinell hardness. With the current interest in high temperature service, relationships have been sought for evaluating behavior by correlations between mechanical properties, particularly to avoid expensive and lengthy creep tests.

A relationship between hot hardness and stress rupture life

was advanced by *Bens* (Fig 7). He measured the hardness at 1600 F of a wide variety of chromium-base alloys for which the rupture times at the same temperature were known. Although the scatter is considerable, the trend is evident. This relationship was one of the first to suggest a connection between the brief hot hardness test and the lengthy creep rupture test.

A similar attempt to correlate hot hardness with creep rupture stress was made by Smith and co-workers (*Garofalo*) at the U.S. Steel Laboratory. They plotted hot hardness vs stress to cause rupture in a certain time (Fig 8). They not only tested a wide range of steels, but also covered a range of temperatures. It can be seen that if the time factor were accounted for in some way, it would not be necessary to have a curve for each time. Also, it may be significant that the short time correlation appears to have the least scatter.

Smith and co-workers also demonstrated a direct-proportion relationship between hot hardness and hot tensile strength for a variety of steels over a range of temperatures. The results compare favorably with the known relationship between room temperature hardness and tensile strength.

An effort was made to bring time into the picture in such a way as to account for the interacting effects of time of test and temperature of test. In 1952, *Larson* and Miller applied the time - temperature parameter of Jaffe and *Hollomon* to creep rupture data. In one form this parameter can be expressed as: $P = T(C+\log t)$. T is absolute temperature (°R) and t is time to rupture (hr). C is a constant which Larson and Miller took to be about 20, but which varies according to the material being tested. They gave a rather complicated method for determining the value of C, but a simpler way is available. If we consider creep rupture tests, for example, it is apparent that the same parameter value should be obtained from tests at different temperatures—provided the stress is the same. A simple equation can be set up in which C is the only unknown. That is, $P = T_1(C + \log t_1) = T_2(C + \log t_2)$. So, if the two temperatures (T_1 and T_2) and the two rupture times (t_1 and t_2) are known, C can be calculated.

The curve of Fig 9 is a typical example of the correlations obtained by Larson and Miller using C= 20. Note that the hot tensile strengths conform to the master rupture curves.

This work of Larson and Miller was the starting point for the Battelle research described earlier.

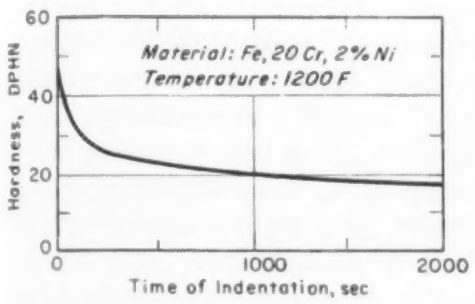


Fig 6—*Hardness dependence on time of indentation.*

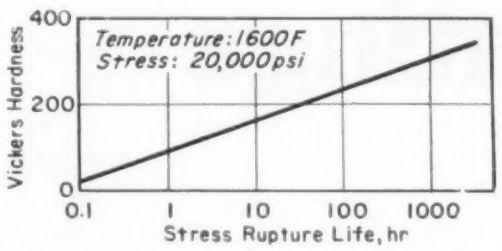


Fig 7—*Trend of stress rupture life in relation to hardness for chromium-base alloys.*

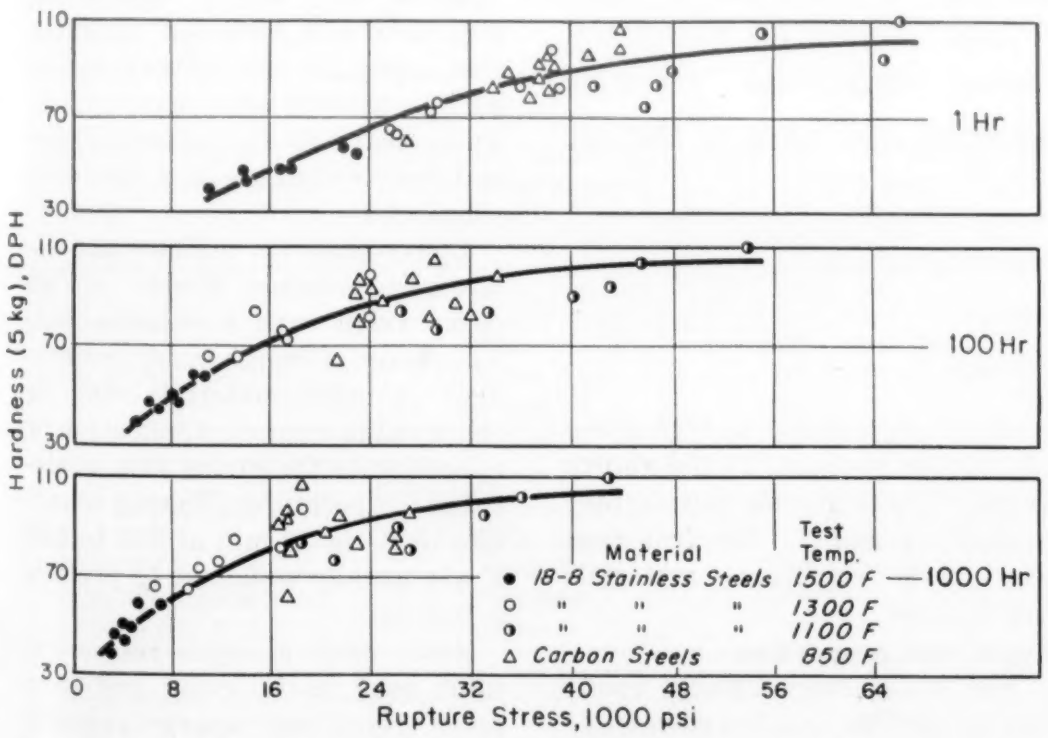


Fig 8—*Stress to cause rupture in stated time plotted vs hardness for stainless and carbon steels.*

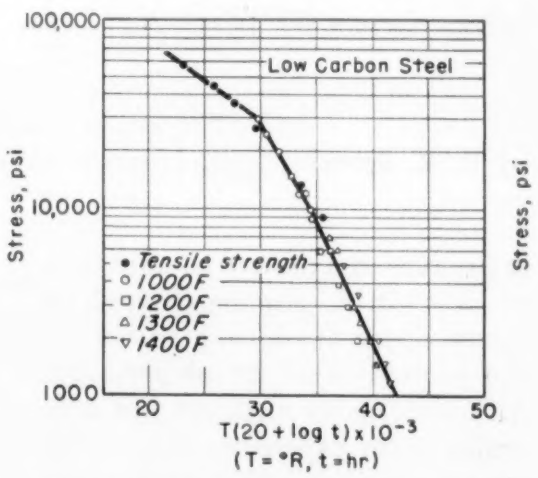


Fig 9—*Example of Larson and Miller correlations between tensile strength or creep rupture stress and the time-temperature parameter of Zener and Hollomon.*

References

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Garofalo, F., Malenock, P. R., and Smith, G. V., "Hardness of Various Steels at Elevated Temperatures," *Trans. ASM*, vol. 45, 1953, p 377.

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Whirlpool-Seeger Corp.

Washing machine *surfaces are given epoxy coating to resist corrosive action of strong detergents.*

Roper Mfg. Co.

Water softener tanks *and heaters are given epoxy coatings to prevent corrosion by acids, organic chlorides and detergents.*

These photos show some current uses of . . .

Epoxy Coatings for Metal Products

These coatings are noted for their excellent adhesion, flexibility, toughness and chemical resistance. Here is detailed information on the properties and uses of the six main types of formulations.

by R. E. Dunbar, *Shell Chemical Corp.*

■ Because of a unique combination of properties, coatings based on epoxy resins are ideally suited for the protection of metal products. Although epoxy coatings are generally more expensive than other organic coating materials on a gallon-for-gallon basis, they provide economical service in many applications. Their higher cost may be offset by savings resulting from: 1) their adaptability to high speed production methods, 2) the ability of thin films to provide satisfactory protection, and 3) the fact that less costly structural materials can be used.

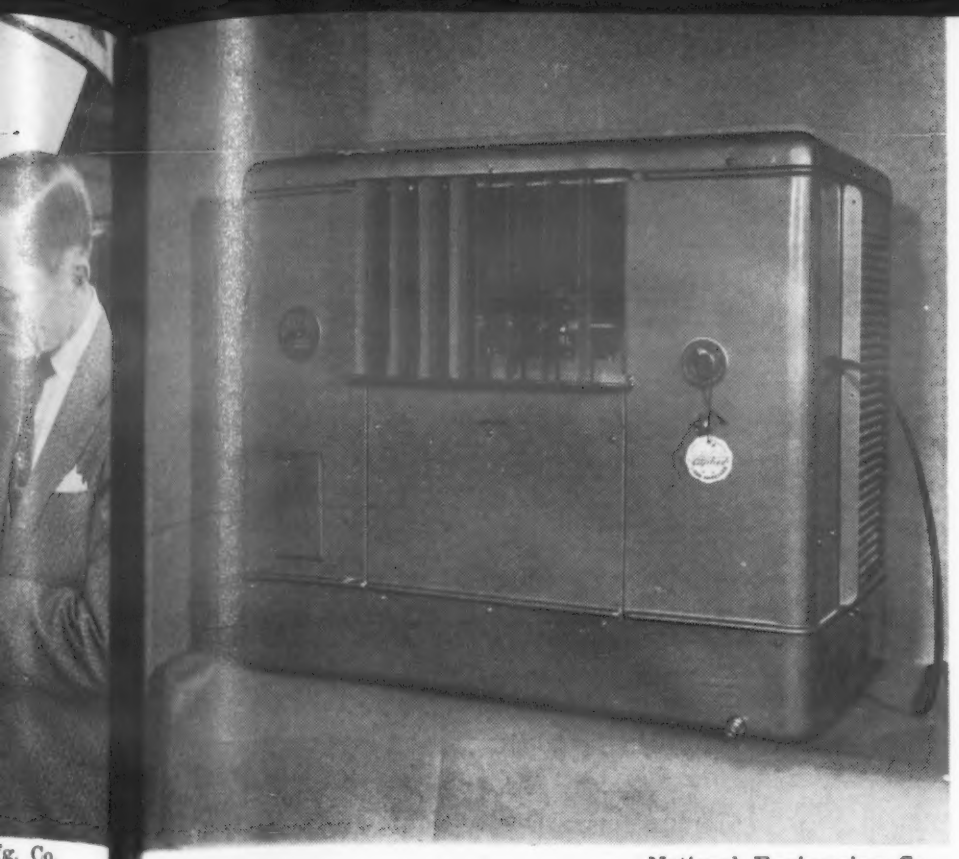
Types and properties

For satisfactory utility, epoxy resins must be modified chemically or blended with catalysts, curing agents or other resins. Epoxy resin finishes of commercial significance can be divided into six general classes of modification: epoxy-phenolics, epoxy-ureas, epoxy-amines, epoxy-polyamides, epoxy resin esters (unmodified), and epoxy resin esters modified with melamine or urea resins. Typical vehicle compositions are shown in Table 1. Comparative information on film properties and methods of application is listed in Tables 2 and 3.

Epoxy-phenolic baking coatings combine outstanding toughness, flexibility and adhesion with the best chemical and solvent resistance obtainable with epoxy resins. These coatings also possess excellent heat resistance and electrical properties.

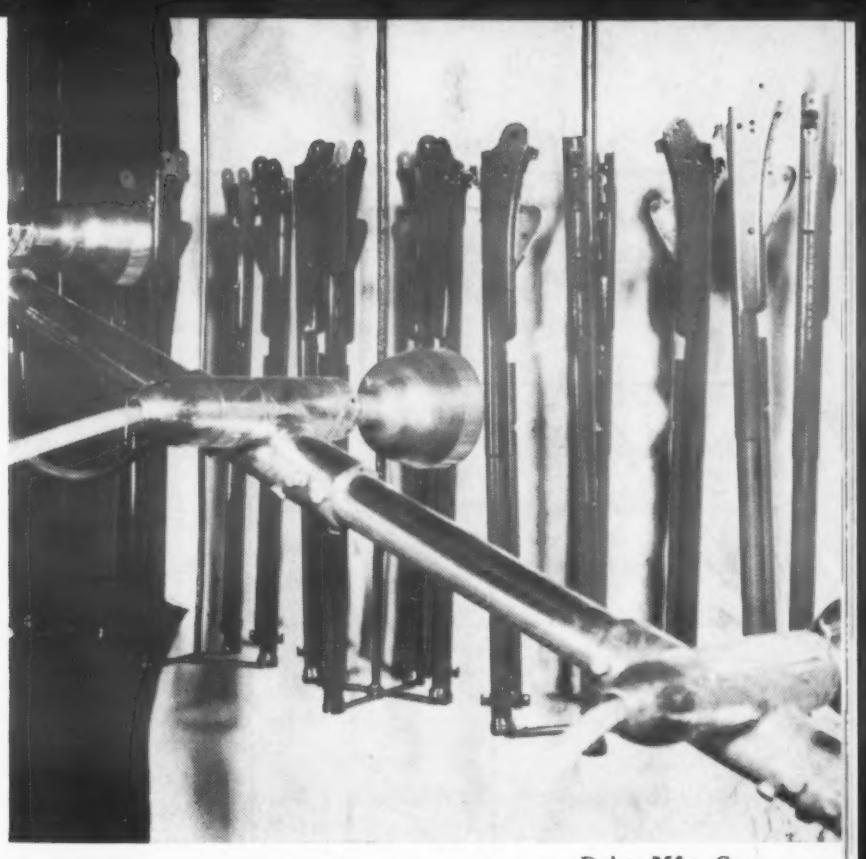
Epoxy-phenolic vehicles are essentially solution blends of an epoxy resin with a suitable phenolic resin, although small percentages of other materials may be employed to improve application or to accelerate the curing rate at elevated temperatures. Baking schedules of 20 to 30 min at 350 to 450 F are usually sufficient to provide a full cure.

Since most phenolic resins exhibit poor initial color and poor color retention, epoxy-phenolic combinations can only be used where the color of the coating is



National Engineering Co.

Air cooler *is given one coat of a tan metallic epoxy finish for decorative appeal and corrosion resistance.*



Daisy Mfg. Co.

Air rifle parts *coated with blue epoxy baking enamel resist impact, wear and corrosion.*

of little importance. Typical applications are can, drum, tank and pipe linings; wire coatings and impregnating varnishes.

Epoxy-urea baking coatings possess physical and chemical resistance properties that approach those of the epoxy-phenolics. They also have the advantage of good initial color and color retention in clear and white finishes.

Certain clear epoxy-urea coatings can be cured by baking for 20 min at temperatures as low as 300 F. Pigmented coatings usually require somewhat higher temperatures.

Typical applications of epoxy-urea coatings are: can linings; appliance primers; clear coatings for brass hardware, costume jewelry and vacuum metallized plastics; and coatings for hospital and laboratory furniture.

Epoxy - amine (amine - cured) coatings are unique in that films cured at room temperature exhibit a degree of chemical and solvent resistance associated normally only with baked coatings. Chemical resistance does not approach that of the phenolic and urea resin modifications, but the amine modifications have excellent chemical and solvent resistance when compared to other air dried coatings.

TABLE 1—TYPICAL COMPOSITIONS OF EPOXY RESIN FINISHES

Solids, % by wt		Solvents, % by wt[a]	
Epoxy-Phenolic			
Epon 1007[b]	73.1	MEK (methylethyl ketone)	15.0
Methylon 75108[c]	24.4	Neosol solvent[e]	25.0
SR-82[d]	1.0	Pine oil	10.0
Phosphoric acid	1.5	Toluene	50.0
Epoxy-Urea			
Epon 1007	70.0	MEK	15.0
Beckamine P-138[g]	30.0	Neosol	25.0
		Pine oil	10.0
		Toluene	50.0
Epoxy-Amine			
Epon 1001[b]	91.5	MIBK (methylisobutenyl ketone)	33.0
Beetle 216-8[h]	2.9	"Cellosolve"[j]	33.0
Diethylene triamine (added shortly prior to use)	5.6	Xylene	34.0
Epoxy-Polyamide			
Epon 1001	66.7	MIBK	33.3
Versamid 115[k]	30.0	"Cellosolve"	33.3
Beetle 216-8	3.3	Xylene	33.4
Epoxy Resin Ester (unmodified)			
Epon 1004[b]	60.0	Xylene	
"9-11" acids[m]	40.0		
Melamine-Modified Epoxy Resin Ester			
Epoxy resin ester	70.0	Xylene	
Melmac 245-8[n]	30.0		

[a]Does not include solvents introduced by raw materials.
[b]Epoxy resin—Shell Chemical Corp.
[c]Phenolic resin—General Electric Co.
[d]Silicone resin—General Electric Co.
[e]Shell Chemical Corp.
[f]For spraying, formulation is reduced to application viscosity with equal parts by weight of diacetone alcohol and xylene.
[g]Urea resin—Reichold Chemicals, Inc.
[h]Urea resin—American Cyanamid Co.
[j]Carbide and Carbon Chemicals Co.
[k]Polyamide resin—General Mills, Inc. Packaged separately from the epoxy resin and mixed shortly prior to use.
[m]Dehydrated castor oil fatty acids—Baker Chemical Corp.
[n]Melamine resin—American Cyanamid Co.

TABLE 2—FILM PROPERTIES OF

Type of Finish	Appearance				Mechanical Properties					
	Color	Color Retention	Gloss	Gloss Retention on Exterior Exposure	Hardness	Adhesion	Flexibility, Impact Resistance	Abrasion Resistance	Cold Water Resistance	Hot Water Resistance
Epoxy-Phenolic (baked)	P-F	F	G	P[b]	E	E+	E	E+	E	E
Epoxy-Urea (baked)	G	G	G	P[b]	E	E+	E	E+	E	E
Epoxy-Amine (air dried)	E	F-G	E	P[b]	G-E	G-E	E initially; embrittles on aging	E	G	F
Epoxy-Polyamide (air dried)	F-G	F-G	E	P[b]	G-E	G-E	E initially; embrittles on aging	E	G	F
Epoxy Resin Ester (unmodified, baked)	G-E	G	G-E	P[b]	G-E	E+	E initially; embrittles slowly on aging	G-E	G	F
Melamine-Modified Epoxy Resin Ester (baked)	G-E	G	G	P[b]	E	E	G-E; may embrittle slowly on aging	E	E	F-G

[a]E+ = generally superior to other organic finishes; E = excellent, but not necessarily the optimum obtainable with other organic finishes; G = good; F = fair; P = poor.
[b]Loss in gloss is due to early chalking; it does not detract from metal protection.
[c]Aside from gloss retention.

Since the curing reaction between amines and epoxy resins takes place at room temperature, the amine curing agent must be packaged separately from the base formulation containing the epoxy resin. The usable life of mixed formulations varies from several hours to several days, depending on ambient temperature and formulation variables. At room temperature, epoxy-amine coatings reach a high degree of cure within 24 hr but require up to seven days to approach maximum chemical and solvent resistance. Curing rates can be greatly accelerated by force drying or baking; a full cure can be obtained by baking for only 10 min at 250 F.

Although epoxy-amine coatings are most widely used in industrial maintenance applications, they are also useful on original equipment when baking is inconvenient or not feasible. Representative applications are linings for transmission pipelines, and coatings for machinery, process equipment and structural steel in chemical plants.

Epoxy-polyamide coatings contain polyamide resins that have amino reactive groups. For this reason, the handling properties, curing requirements and film properties of these coatings closely parallel those of epoxy-amine coatings. In general, the polyamide resin modifications show somewhat poorer solvent resistance and initial color than the amine modifications, but slightly better flexibility on aging.

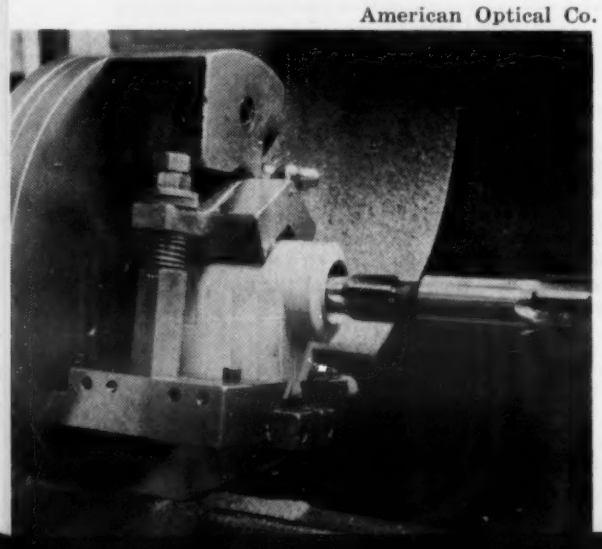
Unmodified epoxy resin ester coatings combine excellent mechanical properties with relatively low cost. As a result, they are the most popular of the epoxy coatings and are widely used as overprint varnishes; as primers for automobiles, appliances and other equipment; and as original and maintenance coatings for structural steel.

Epoxy resin esters closely parallel alkyd resins in vehicle properties and curing requirements. However, the epoxy resin ester coatings generally exhibit better flexibility, adhesion, toughness and chemical resistance than the alkyds, but are slightly more expensive and do not have quite as good color retention.

Coatings based on short-oil length epoxy resin esters are normally used in production line finishing applications. These coatings are ordinarily cured by baking for 10 to 30 min at 300 to 350 F, although they can be cured at room temperature with the addition of conventional driers.

Scuff-proof *epoxy coating applied to scientific and optical instruments prior to machining is not damaged by chucking, boring, reaming and threading operations.*

American Optical Co.



EPOXY RESIN FINISHES[a]

Chemical Properties			Environmental Properties	
Solvent Resistance	Alkali Resistance	Acid Resistance	Heat Resistance	Exterior Durability[c]
E to aliphatics, aromatics and alcohols; G-E to ketones and esters	E+	E to dilute acids; F-G to conc nonoxidizing acids; P to conc oxidizing acids	E	E pigmented, G clear
E to aliphatics, aromatics and alcohols; G to ketones and esters	E	G-E to dilute acids; F to conc nonoxidizing acids; P to conc oxidizing acids	E	E pigmented, G clear
E to aliphatics and aromatics; F-G to alcohols, ketones and esters	G	F-G to dilute acids; P to conc acids	G	E pigmented, F clear
E to aliphatics and aromatics; F-G to alcohols, ketones and esters	G	F-G to dilute acids; P to conc acids	G	E pigmented, F clear
F to aliphatics; P to aromatics, alcohols, ketones and esters	F-G	P	F	E pigmented, G clear
G to aliphatics; F to aromatics; P to alcohols, ketones and esters	G	P-F to dilute acids; P to conc acids	G	E pigmented, G clear

Coatings based on the longer oil length esters cure at room temperature and are generally used on equipment that cannot be baked conveniently.

Modified epoxy resin ester baking coatings, based on solution blends of drying type esters with melamine or urea resins, provide films with better hardness and chemical resistance than the unmodified esters, but with somewhat poorer flexibility and impact resistance. Slightly better initial color and color retention can be obtained when esters made from nondrying acids are used instead of the drying types. Baking schedules of 20 to 30 min at 300 to 350 F are generally required for all of the epoxy ester finishes.

Clear coatings

For copper, brass and silver— Because of the constant handling experienced by hardware, costume jewelry and small appliances, clear coatings for these products must possess excellent adhesion and resistance to abrasion and perspiration. The coatings must also remain free from yellowing for long time periods. Epoxy-urea coating systems exhibit an outstanding combination of these properties. For most copper, brass and silver products satisfactory protection is provided by a single coat of less than 1 mil.

Where baking is impractical because of the size of the part, excellent results can be obtained with a single coat of an epoxy-amine finish which cures at room temperature.

TABLE 3—HOW AND WHERE EPOXY FINISHES ARE APPLIED

Type of Finish	Method of Application	Approximate Solids Content at Spray Viscosity, %		Spray Coat Film Thickness, mils	Typical Curing Schedules	Typical End Uses
		Clear	Pigmented White[a]			
Epoxy-Phenolic	Spray, roller, dip, flow	30	45	0.7-1.1	20 min at 375 F	Can, drum, pipe and tank linings; wire coatings and impregnating varnishes
Epoxy-Urea	Spray, roller, dip, flow	30	45	0.7-1.1	20 min at 300 F[b] 20 min at 385 F[c]	Can linings; appliance primers; clear coatings for brass hardware, jewelry and vacuum metallized plastics; foil coatings; and coatings for laboratory and hospital furniture
Epoxy-Amine	Spray, brush	40	55	1.0-2.0	Air dry (55 F min) or bake (10 min at 250 F)	Linings for transmission pipelines; coatings for machinery, process equipment and structural steel in chemical plants
Epoxy-Polyamide	Spray, brush	40	55	1.0-2.0	Air dry (55 F min) or bake (10 min at 250 F)	Generally same uses as epoxy-amine finishes
Epoxy Resin Ester (unmodified)	Spray, roller, dip, flow, brush	30-35	50	0.7-1.1	Air dry or bake (20 min at 325 F)	Overprint varnishes; primers for autos, appliances and other equipment; foil coatings; original and maintenance finishes for structural steel
Melamine-Modified Epoxy Resin Ester	Spray, roller, dip, flow	30-35	50	0.7-1.1	30 min at 300 F	Generally same uses as unmodified epoxy resin ester finishes

[a]Titanium dioxide, pigment: binder = 1:1. [b]Clear finish. [c]White finish.

For aluminum—Epoxy resin ester coatings exhibit excellent adhesion, flexibility and abrasion resistance over aluminum. Because of their relatively low cost they are generally preferred for use on foil and ornamental vacuum metallized surfaces.

Epoxy-urea coatings, however, provide better protection against corrosion and chemicals over aluminum and are required in some applications. An example is the use of a specially formulated epoxy-urea coating on vacuum metallized flash reflectors. Here the coatings must provide complete protection against corrosion and must be able to withstand rough handling.

For tin plate—Because of their combination of toughness, flexibility and chemical resistance, epoxy resin coatings are well adapted to coating sheet metal prior to fabrication. Typical of the large volume industrial applications in this category is the use of a clear epoxy-phenolic prime coat in lining beverage cans. The coating remains undamaged during welding of the side seams.

Epoxy-urea and epoxy-phenolic coatings are also gaining increased acceptance as linings for lard, meat and other food containers. These coatings have demonstrated superior performance in food packaging, but their growth has been slowed somewhat by the time consuming tests required for government approval.

Overprint varnishes

Epoxy resin esters make ideal overprint varnishes. They are usually specified because the strong solvents required in other epoxy systems dissolve, lift or cause bleeding of lithographic inks.

Epoxy resin esters are essentially colorless in thin films and exhibit superior toughness and abrasion resistance when compared to conventional overprint varnishes. Because of their excellent flexibility and adhesion, they can be applied to lithographed sheet metal prior to fabrication. Application of epoxy overprint varnishes on bottlecaps, can closures, trays and similar products is one of the largest end uses for epoxy coatings.

Pigmented coatings

For steel—Aside from color, pigments in epoxy coatings are employed principally to increase film build-up and exterior durability, and to improve resistance to moisture, chemicals and abrasion. Because of the outstanding protection provided by epoxy primers, and because of certain decorative limitations of epoxy enamels, the best over-all performance on steel surfaces is frequently obtained by using an epoxy primer under an alkyd, lacquer or acrylic topcoat.

Although the color retention of white epoxy enamels is adequate for many products, alkyd topcoats are slightly superior in this respect and are generally preferred for appliances. Good corrosion and abrasion resistance for washing machines is obtained by using a melamine-modified epoxy resin ester primer or an epoxy-urea primer and a conventional alkyd resin topcoat. An epoxy primer alone is usually sufficient to protect interior surfaces.

For products such as office furniture and kitchen cabinets, where mechanical durability is required, melamine-modified epoxy resin ester finishes are the most economical. For hospital and laboratory equipment, where chemical or solvent resistance is also required, epoxy-urea finishes are preferred. In these applications, surface preparation is generally limited to a conventional acid pretreatment.

Epoxy resin coatings also provide excellent durability and corrosion protection to surfaces subjected to outdoor exposure. Although epoxy enamels tend to lose gloss by chalking at an earlier stage than alkyd enamels, loss in film thickness is negligible during extended exposure. If a loss in gloss can be tolerated, a coating system using both an epoxy primer and an epoxy enamel provides excellent outdoor protection.

Where gloss retention is required outdoors, the use of an epoxy resin ester primer under an alkyd, lacquer or acrylic topcoat is finding increased acceptance. Coating systems of this type are widely used for automotive finishing and the primer is applied in a single, 1-mil (dry) coat. For products such as outdoor furniture, less than 0.5 mil of a melamine-modified epoxy resin ester primer is usually required. (This thickness is about half that normally used with alkyd resin primers.) The epoxy resin primers provide good resistance to chipping and corrosion and, because of their excellent adhesion, they inhibit corrosion creepage if film damage occurs.

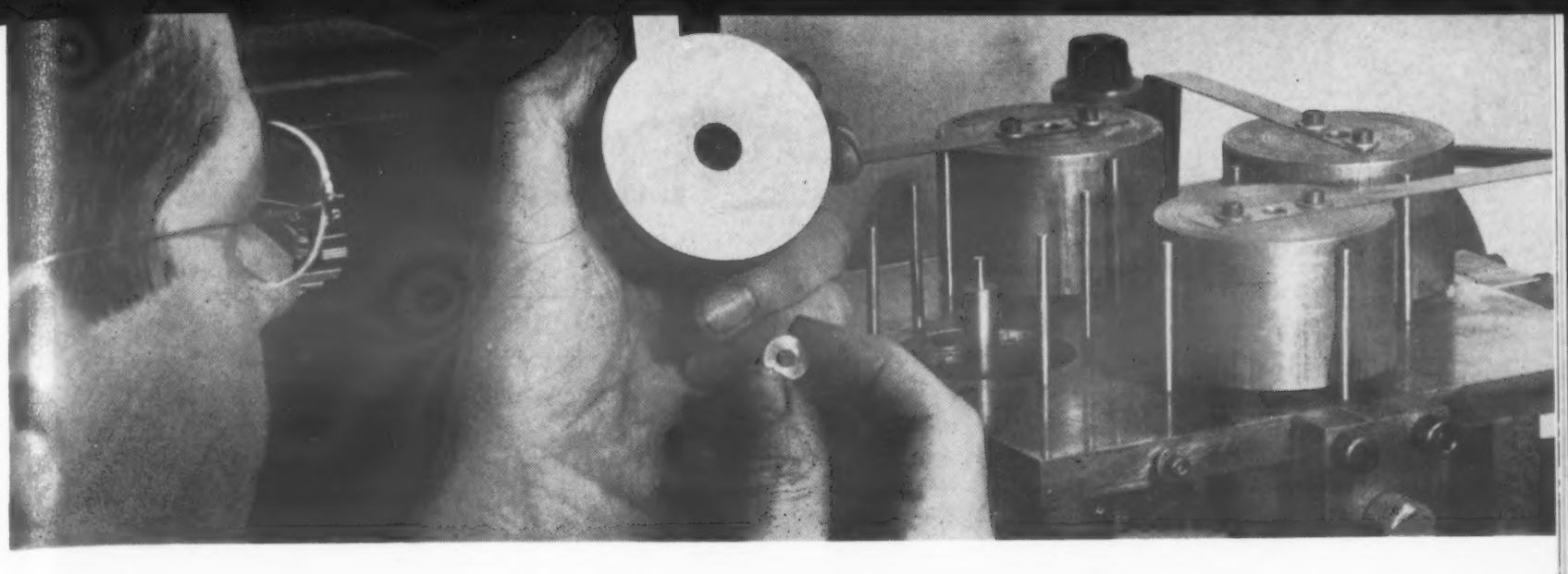
Multiple coats of an epoxy-phenolic system, applied to a sandblasted surface, are widely used to protect steel drums, tanks and pipe in contact with chemicals, hot water and strong solvents. Because of their excellent mechanical properties, these coatings are often preferred over coatings that appear to be superior in straight immersion tests.

Where a high degree of corrosion protection is required, 6 to 7 coats with a total thickness of 5 to 7 mils are frequently specified. A partial bake is given to each coat after application and a final bake is given to the topcoat to complete the cure.

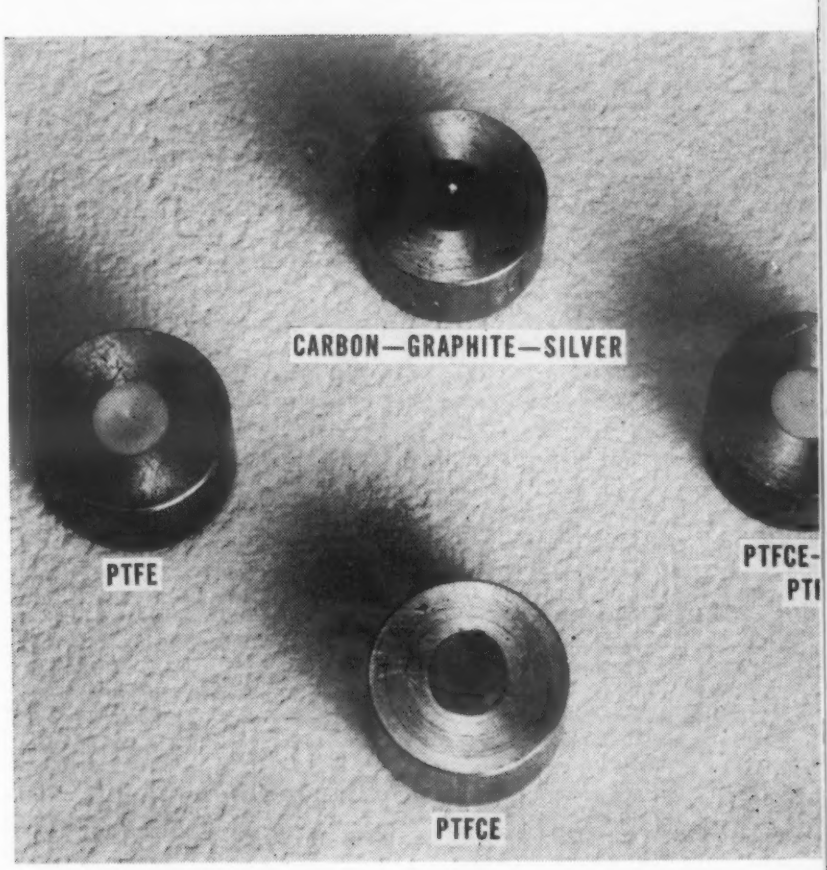
For aluminum — Aside from tinted transparent finishes, the major use for epoxy resin primers and enamels over aluminum has been for aircraft. Epoxy-amine coatings are used primarily because they can be cured at room temperature and because of their excellent resistance to the solvent action of brake and de-icing fluids.

Last of a Series

This is the last in a series of five monthly articles on synthetic resin-base coatings for metal products. Previous articles were devoted to acrylic (Dec '56), phenolic (Jan '57), silicone (Feb '57) and vinyl (Mar '57) coatings.



After 60 days in wear tester (above) these specimens show wide variations — a good reason for careful evaluation in selecting



Materials for Small, Oil-Free Bearings

Here are data on wear rates and friction coefficients of many combinations of metallic and nonmetallic materials.

by Hobart S. White,
National Bureau of Standards

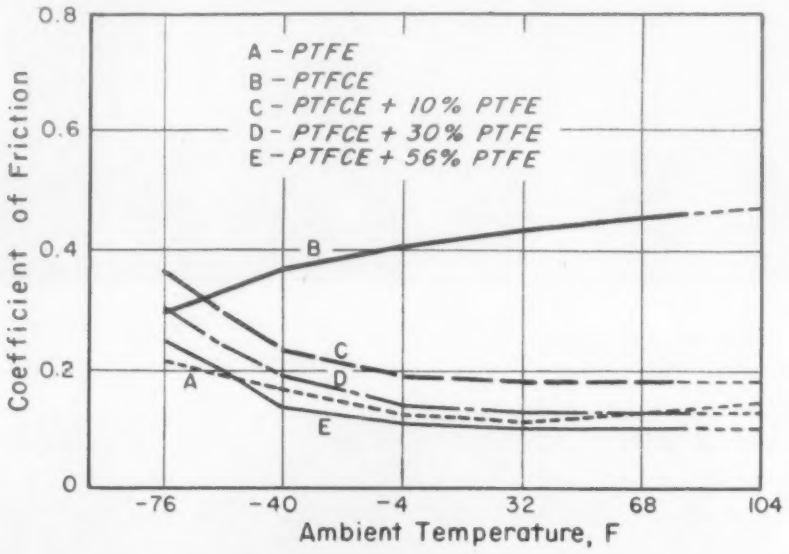
■ It is a well known fact that the increased viscosity and congealing of oils at subzero temperatures produces excessive friction and seriously interferes with the performance of lubricated bearings used in small instruments. In some devices this added friction can be overcome by providing extra driving power. For many instruments, however, this solution is not feasible and the designer must seek out a satisfactory low temperature lubricant or else switch to an oil-free bearing with low friction properties.

Recently there has been developed a number of oil-free bearing materials that provide a low coefficient of friction and low wear over a wide temperature range. These materials also eliminate the need for periodic cleaning and oiling during storage and service.

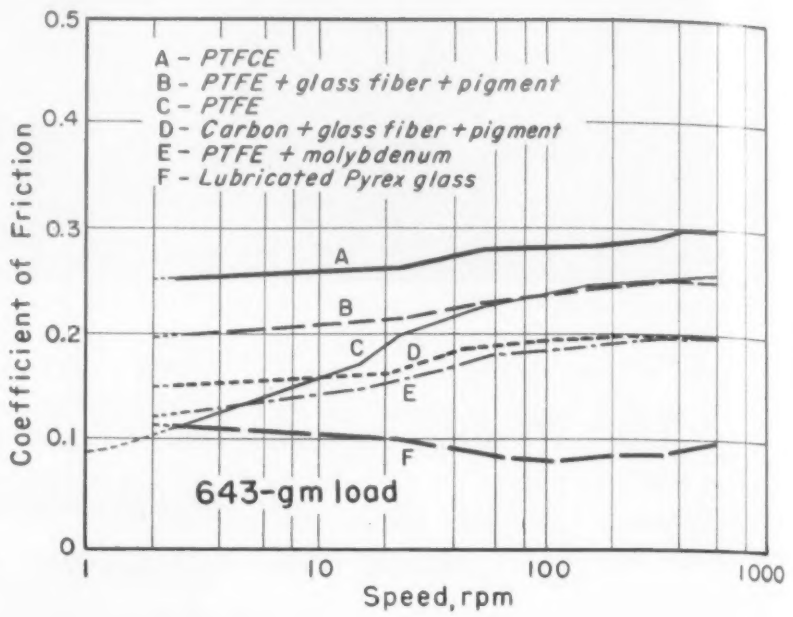
As shown in the accompanying tables and graphs, friction and wear characteristics have been determined for a variety of oil-free bearing materials. In general, these materials can be classified into five main groups as follows: 1) plastics such as polytetrafluoroethylene (PTFE), polytrifluorochloroethylene (PTFCE), nylon and high density polyethylene; 2) plastics with various fillers, such as graphite, molybdenum disulfide, glass fiber, dental silicate, silicon, titanium dioxide, silver, copper,

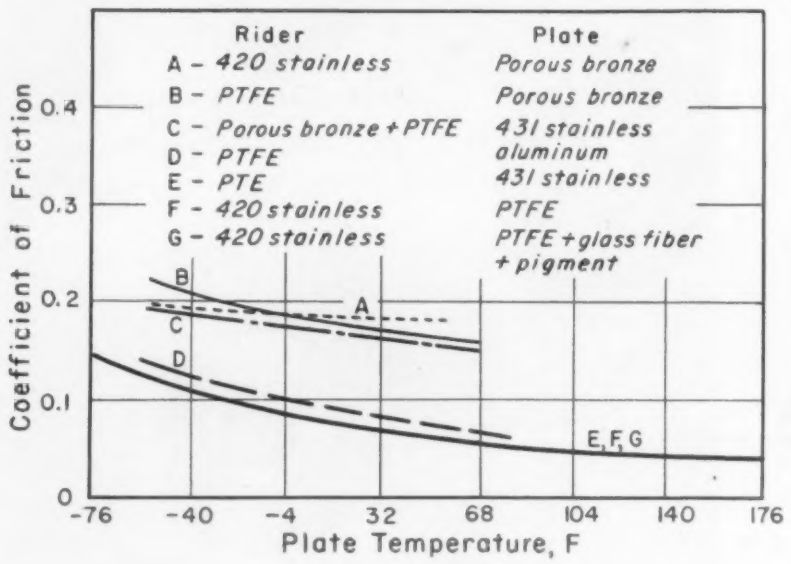
Coefficient of Friction of

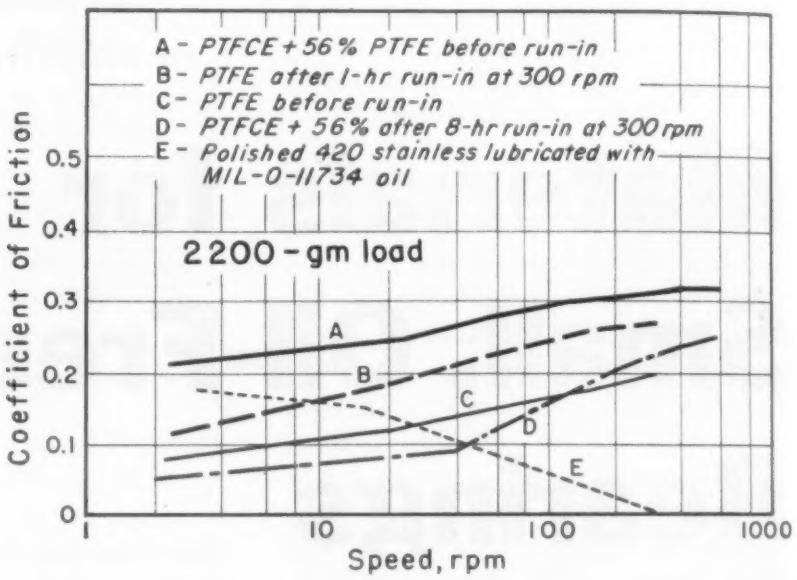
VS TEMPERATURE



VS SPEED







tungsten and molybdenum; 3) bronze impregnated with PTFE, graphite and molybdenum disulfide; 4) graphite and electrographitic carbon impregnated with silver and babbitt; and 5) various other materials such as stainless steel, anodized aluminum, brass, diamond, etc. Principal characteristics of these groups of bearing materials are summarized below.

Plastics

PTFE—Because of its tendency to wear, PTFE is not recommended as a bearing material for small instruments such as clocks and chronometers. The usefulness of this material is also limited by an increase in its coefficient of friction below —4 F. At very low surface speeds and low pressures its wear resistance may be adequate for special applications.

PTFCE—The high friction and wear rate of PTFCE at ordinary temperatures preclude its use as an oil-free bearing material in timepieces. The decrease in friction of this material at low temperatures, however, is a distinct advantage and may make it useful for special low speed applications.

PTFE and PTFCE Coatings—In journal bearings, a fused coating of PTFCE provides good wear resistance but has a relatively high coefficient of friction. A fused coating of PTFE provides lower friction, but at the expense of decreased wear resistance. Both of these coatings wear rapidly when used as thrust bearings. Because of the thickness of the coatings ordinarily used, and the difficulty in producing a uniform coating with a good bond on small parts, these coatings do not seem practical for journals or bearings less than 1/16 in. in dia. However, work at the Naval Research Laboratory indicates that PTFE coatings may be useful for some applications.

Nylon—Nylon has been used as a bearing material in a number of industrial applications (see "Teflon and Nylon Bearing Materials," M&M, Mar., '56, p. 100). How-

Various Bearing Materials

RUNNING AGAINST STEEL SHAFTS[a]

Shaft Material[b]	Coefficient of Friction at 3 Rpm after . . .					
	0 Hr	1 Hr	2 Hr	4 Hr	6 Hr	8 Hr
PTFE						
M	0.06	0.09	0.11	0.12	0.12	0.13
D2	0.10	0.20	0.23	—	—	—
D3	0.10	0.17	0.17	0.15	0.15	0.15
C40	0.06	0.07	0.08	0.10	0.11	0.11
440C	0.10	0.13	0.14	0.15	0.15	0.15
PTFE + 65% (31% by vol) Molybdenum Powder (0.5-5.0 μ)						
M	0.07	0.19	0.27	0.32	0.32	0.33
D2	0.08	0.12	0.15	0.20	0.23	0.25
D3	0.08	0.10	0.10	0.12	0.15	0.22
C40	0.03	0.09	0.09	0.06	0.06	0.07
440C	0.06	0.07	0.07	0.09	0.12	0.15
PTFCE + 56% PTFE (fused at 500 F)						
M	0.08	0.19	0.17	0.15	0.14	0.13
D2	0.16	0.19	0.18	0.15	0.13	0.13
D3	0.20	0.20	0.16	0.13	0.12	0.11
C40	0.04	0.10	0.11	0.13	0.14	0.13
440C	0.17	0.18	0.15	0.14	0.13	0.13
Carbon + Graphite + Silver						
M	0.24	0.29	0.33	0.36	0.36	0.34
D2	0.16	0.23	0.25	0.30	0.34	0.34
D3	0.20	0.27	0.28	0.29	0.30	0.30
C40	0.22	0.25	0.26	0.27	0.27	0.27
440C	0.20	0.24	0.24	0.25	0.25	0.26

[a] ¼-in. bearings, 2200-gm load, 77 F.
[b] M — Chromium-vanadium alloy machinery steel with small amounts of nickel and molybdenum, Rc 24. D2 — Air hardened, high chromium tool steel, Rc 55. D3 — Oil hardened, high chromium tool steel, Rc 60. C40 — 40 cobalt — 20 chromium — 15 nickel — 7 molybdenum — 2 manganese alloy, Rc 58.

RUNNING AGAINST 420 STAINLESS STEEL[a]

Material	Coefficient of Friction at . . .		
	3 Rpm (0.2 sfm)	15 Rpm (1.0 sfm)	300 Rpm (20 sfm)
Polytetrafluoroethylene (PTFE)	0.12	0.18	0.26
PTFE + 13% Glass Fiber (0.05μ avg dia)	0.22	0.23	0.25
PTFE + Glass Fiber + Pigment	0.20	0.21	0.26-0.32
PTFE + Glass Fiber + Molybdenum disulfide (MoS_2)	0.11	0.13	0.18
PTFE + Graphite	—	—	0.28
PTFE + Copper Powder	0.13	0.16	0.22
PTFE + 73% (40% by vol) Molybdenum Powder	0.13	0.15	0.20
PTFE + 70% (34% by vol) Mo + 6% Chromium Tetrahydrate	0.30	0.31	0.33
PTFE + MoS_2	0.13	0.18	0.28
PTFE + 90% (50% by vol) Tungsten Powder	0.18	0.20	0.22
PTFE + 28% (18% by vol) Titanium Dioxide (TiO_2)	0.23	0.23	0.27
PTFE + 18% TiO_2 + 4% Polymethylsiloxane	0.15	0.19	0.26
PTFE + 18% TiO_2 + 11% Chlorinated Biphenyl	0.16	0.18	0.23
PTFE + 80% (52% by vol) Tin (fused at 700 F, 10,000 psi)	0.15	0.17	0.20
PTFE + 70% (33% by vol) Silver Precipitated Flowers	0.27	0.26	0.23
Polytrifluorochloroethylene (PTFCE)	0.25-0.27	0.26-0.28	0.29-0.45
PTFCE + 56% PTFE (fused at 500 F)	0.22	0.22	0.26
PTFCE + 51% PTFE + 10% Glass Fiber (fused at 500 F, 13,000 psi)	0.26	0.26	0.26
PTFCE + 14% (27% by vol) PTFE + 64% (28% by vol) Mo	0.16	0.19	0.23
PTFCE + MoS_2	0.36	0.36	0.40
PTFCE + Graphite	0.16-0.25	0.18-0.26	0.24-0.29
PTFCE + 51% PTFE + 13% Chromium Tetrahydrate	0.20	0.22	0.25
Nylon, Molded	—	—	0.28-0.35
Nylon, Sintered and Machined	0.22	0.20	0.28-0.32
Nylon, Resintered after Machining	0.28	0.26	0.32-0.33
Carbon + Graphite + Silver	0.15	0.16	0.20-0.28
Electrographitic Carbon + Silver	0.28	0.28	0.27
Carbon + Graphite + Babbitt	0.21	0.22	0.23
Electrographitic Carbon + Babbitt	0.27	0.27	0.26
Silver Amalgam	0.13	0.13	0.12
Polished 420 Stainless Steel with MIL-G-7421 Grease	0.08	0.06	0.06
Polished 420 with MIL-O-11734 Oil	0.18	0.16	0.03
Polished 420 with Watch Oil	0.12	0.06	0.04
Anodized 6061 Aluminum with Watch Oil	0.13	0.06	0.05
Polished Sapphire (clean)	0.18	0.20	0.36
Polished Sapphire with Watch Oil	0.12	0.06	0.05
Polished Sapphire with Oil Wiped Off	0.13	0.14	0.21

[a] ¼-in. hardened shafts, room temperature, 643-gm load.

ever, it possesses a higher friction coefficient than a number of the other materials for small, oil-free bearings. Because of its relatively large variation in water content and change in size with temperature and humidity, the material cannot be recommended for precision bearings.

High density polyethylene—The coefficient of friction of this material is somewhat greater than that of PTFE, especially at low temperatures. Its rate of wear at 150 rpm, however, is less than that of the other unfilled plastics described above.

Plastics with fillers

PTFCE containing 10 to 60% PTFE as a filler is one of the most promising oil-free bearing materials developed. This material possesses some of the hardness of PTFCE and the frictional characteristics of PTFE, and it has much greater wear resistance than either of these plastics alone. Unfortunately, the fact that its frictional characteristics are similar to those of PTFE detracts from its usefulness at subzero temperatures. PTFCE containing graphite and molybdenum disulfide also exhibits a lower friction coefficient and greater wear resistance than

PTFCE alone, but these dry lubricant additives are not as effective as the PTFE filler.

PTFE bearings containing molybdenum metal powder (0.5 to 5 microns) as a filler have shown considerable promise. This mixture possesses good friction characteristics and exceptional wear resistance under certain conditions.

Preparations of PTFE containing glass fiber and pigment also have good wear and friction properties when used as oil-free bearings with a 0.25-in. bore. The relatively large size of some of the glass fibers and the large pockets of plastic in the mixture preclude its use for small bearings where the bore may be only a few mils in diameter. Additions of graphite, copper powder or molybdenum disulfide to PTFE also reduce wear in 0.25-in. bearings but, here again, formation of pockets in the plastic prevents use of the material in smaller sized bearings.

Impregnated bronze

Microscopic examination of porous bronze reveals that some of the pores and sections of solid bronze are much larger than the diameter of balance staff journals used in watches. For this reason the material is not suitable for small diameter parts. Also, because of comparatively poor friction and wear properties, porous bronze impregnated with either PTFE or molybdenum disulfide cannot be recommended.

Impregnated carbon

In general, the metal-impregnated carbon materials have good friction and wear characteristics. They also have a low coefficient of thermal expansion, and in some applications their good electrical conductance may be useful. Because of lack of homogeneity and relative coarseness of structure, these materials cannot be recommended for very small bearings (less than 1/16-in. bore).

Other materials

No material has been found as satisfactory as diamond for thrust bearings operating under high load conditions such as occur at the upper endstone of balance shafts in chronometers. Also, no material has been found as satisfactory as sapphire for use as pallet stones in timepieces. Sapphire appears to be suitable for use as unlubricated endstones under relatively light loads, especially in timepieces normally operating in an upright

Wear Rates of Bearing Materials

THRUST BEARING MATERIALS[a]

Bearing	Time Run, days	1000-Gm Load		1240-Gm Load		Avg Wear Rate, in./yr.
		Depth of Wear, in.	Pressure, psi	Depth of Wear, in.	Pressure, psi	
PTFE	20	0.011	266	0.010	363	0.110
	40	0.016	187	0.015	247	0.091
	60	0.020	180	0.020	223	0.082
PTFCE	20	0.009	323	0.0075	478	0.119
	40	0.013	228	0.011	330	0.068
	60	0.016	187	0.014	263	0.055
PTFE + 65% (31% by vol) Molybdenum Powder (0.5-5.0 μ)	20	0.0015	1875	0.0015	2326	0.018
	40	0.002	1418	0.002	1758	0.009
	60	0.002	1418	0.002	1758	0.000
PTFCE + 56% PTFE (fused at 500 F)	20	0.002	1418	0.002	1758	0.009
	40	0.002	1418	0.002	1758	0
	60	0.002	1418	0.002	1758	0
PTFE + Glass Fiber + Other Fillers	20	0.0015	1875	0.002	1758	0.009
	40	0.002	1418	0.002	1758	0.005
	60	0.002	1418	0.0025	1393	0.005
Carbon + Graphite + Silver	20	0.002	1418	0.0015	2326	0.018
	40	0.0035	818	0.0015	2326	0.014
	60	0.004	715	0.0015	2326	0.005
Polished Sapphire[b]	20	0.005	574	—	—	0.036
	40	0.007	412	—	—	0.036
	60	0.0095	311	—	—	0.046
Polished Diamond	20	—	—	0	139,300	0
	40	—	—	0	139,300	0
	60	—	—	0	139,300	0
PTFE + Green Pigment Enamel (fused on brass)	4	0.031	180	0.027	233	2.65
PTFCE + 20% Graphite Coating (fused on brass)	10	0.010	292	0.016	232	0.475

[a]Against hardened 440C stainless steel shaft with ⅛-in. end radius; shaft oscillates at 1 cps with 1.5 radian amplitude.
[b]Wear occurred on end of steel pin instead of on sapphire endstone.

JOURNAL BEARING MATERIALS[a]

Material	Shaft Material	Estimated Time to Produce 0.005-in. Radial Wear, hr				Rating[b] at 150 Rpm
		15 Rpm	150 Rpm	700 Rpm	1800 Rpm	
Polytetrafluoroethylene (PTFE)	303	1400	25	—	—	5
PTFE + 13% Glass Fiber (0.05μ avg dia)	303	60,800	7020	2430	962	3
PTFE + Glass Fiber + Pigment	303	95,400	12,700	—	—	2
PTFE + Glass Fiber + Molybdenum Disulfide (MoS_2)	303	58,100	3710	1340	—	3
PTFE + 18% Titanium Dioxide (TiO_2) + 4% Polymethylsiloxane	303	19,100	119	—	—	4
PTFE + MoS_2	303	30,500	480	—	—	4
PTFE + 73% (40% by vol) Molybdenum Powder	303	100,000+	100,000+	—	—	1
PTFE + 63% (29% by vol) Mo Powder	303	—	26,800	—	94	2
	440	—	1660	—	1510	3
	D3[c]	—	3750	—	1240	3
	C40[d]	—	100,000+	—	21	1
PTFE + 70% (34% by vol) Mo + 6% Chromium Tetrahydrate	303	100,000+	1630	—	—	3
PTFE + 36% Silicon Powder	303	4450	1660	166	—	3
PTFE + 25% Dental Silicate	303	13,000	16,600	1400	—	2
	D3	—	—	—	2	—
PTFE + 67% (33% by vol) Copper Powder	303	21,500	203	99	—	4
PTFE + 80% (52% by vol) Tin (fused at 700 F, 10,000 psi)	303	113	35	—	—	5
PTFE + 28% (18% by vol) TiO_2	303	18,900	2070	—	—	3
PTFE + 18% TiO_2 + 11% Chlorinated Biphenyl	303	5790	236	—	—	4
PTFE + Graphite	303	45,700	12,200	—	—	2
PTFE + Copper Powder	303	2230	910	—	—	4
PTFE + 90% (50% by vol) Tungsten Powder	303	8000	1280	—	—	3
PTFE + Green Pigment Enamel (fused on brass)	303	—	5220	—	166	3
PTFE + Clear Coating (fused on brass)	303	—	630	—	3	4
Polytrifluorochloroethylene (PTFCE)	303	1340	116	—	—	4
PTFCE + 10% PTFE (fused at 500 F)	440C	—	870	—	130	4
	303	—	2220	—	140	3
	C40	—	1220	—	140	3
PTFCE + 56% PTFE (fused at 500 F)	303	11,400	8700	11,400	1220	3
	440C	—	1880	—	247	3
	D3	—	1830	—	415	3
	C40	—	3810	—	507	3
PTFCE + 51% PTFE + 10% Glass Fiber (fused at 500 F, 13,000 psi)	303	26,100	14,000	2150	—	2
PTFCE + 14% (27% by vol) PTFE + 64% (28% by vol) Molybdenum	303	63,100	11,300	286	—	2
PTFCE + Mo S_2	303	10,600	2120	48	—	3
PTFCE + 51% PTFE + 13% Chromium Tetrahydrate	303	31,800	11,900	21	—	2
PTFCE + Graphite	303	2050	182	—	—	4
PTFCE + 20% Graphite Coating (fused on brass)	303	—	11,600	—	513	2
Nylon, Molded	303	1440	103	—	—	4
Nylon, Sintered and Machined	303	1160	99	—	—	5
Nylon, Sintered after Machining	303	1570	—	—	—	—
High Density Polyethylene	303	—	360	—	27	4
Carbon + Graphite + Silver	303	14,600	13,300	334	—	2
Electrographitic Carbon + Silver	303	19,400	3230	—	—	3
Carbon + Graphite + Babbitt	303	41,500	5810	—	—	3
Electrographitic Carbon + Babbitt	303	5740	313	—	—	4
Sintered Porous Bronze + Molybdenum Disulfide	303	—	52	—	—	5
Bearing Bronze: 83 Copper—8 Tin—8 Lead	303	—	50	—	—	5
Tungsten + MoS_2 + Plastics Coating (on brass)	303	—	0.9	—	—	5

[a] ¼-in. shafts, room temperature, 2000-gm load.
[b] 1:100,000+ hr., excellent; 2:10,001 to 100,000 hr., very good; 3:1,001 to 10,000 hr., good; 4:101 to 1000 hr., fair; 5:0 to 100 hr., poor.
[c] D3 — Oil hardened, high chromium tool steel, Rc 60.
[d] C40—40 cobalt—20 chromium—15 nickel—7 molybdenum—2% manganese alloy, Rc 58.

position.

Despite its exceptionally low friction at room temperatures, silver amalgam has proved very brittle and hole edges have chipped badly during boring and reaming operations. An amalgam of dental alloy filings has been found less brittle, but it undergoes an increase in its friction coefficient and becomes scuffed shortly after operation is started.

Stretch forming *titanium alloy part in a 500-ton Sheridan press.*

Titanium Alloy Suited for Stretch Formed Parts

Preliminary tests indicate 6 aluminum–4% vanadium alloy can be formed with standard tools and techniques.

by Eric J. Carr, *Manufacturing Engineer, Pilotless Aircraft Div., Boeing Airplane Co.*

■ Stretch forming of titanium-aluminum-vanadium alloy sheet (Ti 6A1-4V) can be done satisfactorily at room temperature using conventional tools and methods. Edge preparation, surface condition and thickness variation offer no greater problems than are encountered with aluminum. However, control of heat treated condition of the alloy and jaw grip are important in obtaining satisfactory results.

Stretch forming is used extensively in the production of double-contoured aluminum and magnesium skins for today's aircraft. Normal stretching operations are performed at room temperature on aluminum alloys and at about 350 F on magnesium.

Tougher alloys will be necessary for future aircraft, and Ti 6A1-4V gives excellent promise for this use. It retains a favorable strength-weight ratio to 1000 F, is heat treatable to 180,000 psi ultimate strength, and is readily weldable.

The measure of formability of a material is the spread between yield and ultimate strengths. Ti 6Al-4V has a relatively small range at a high value (120,000 psi tensile yield strength to 130,000 psi tensile strength, annealed) which indicates difficulty in forming. Preliminary testing has shown, however, that although high forming pressures are required, the material is readily formed within this range.

Forming tests

In the Boeing tests, as suggested above, stretch forming was accomplished with tools and parts at room temperature, using standard methods, tools and lubricants. All parts tested were successfully formed, although springback was not always removed before failure. All failures were in the excess metal or at the jaws.

A 30 by 60-in., double-contoured *Kirksite* block was used in the investigation. The parts were 0.050 in. thick, 12 in. wide and 50 in. long, allowing approximately 12 in. of excess. Parts were tested in three heat treated conditions:

	Yield Strength, 1000 psi	Tensile Strength, 1000 psi
Mill Ann.	120	130
Sol. Heat Treated	105	140
Aged Full Hard	150	180

The preliminary tests indicate that:

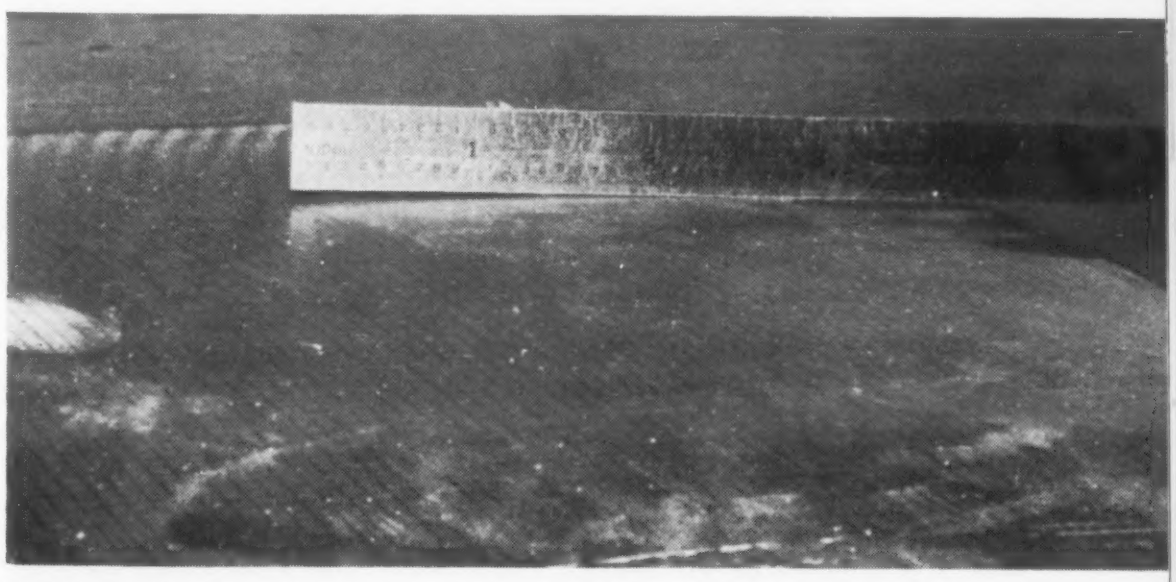
1. Graphite cup grease gives uniformly satisfactory results as a lubricant.

2. Gripping the part is more difficult than with steel or aluminum. Titanium shims or clean steel jaws give the best grip. A heavy (10,000 lb) jaw pressure is necessary, and shims used adjacent to the part should be thinner (up to 0.005 in. thinner) than the material.

3. Edge preparation of the sheets is not as critical as previous information has indicated. Several sheets with sheared edges and two having severe edge notches were successfully stretched with no failure at the notches.

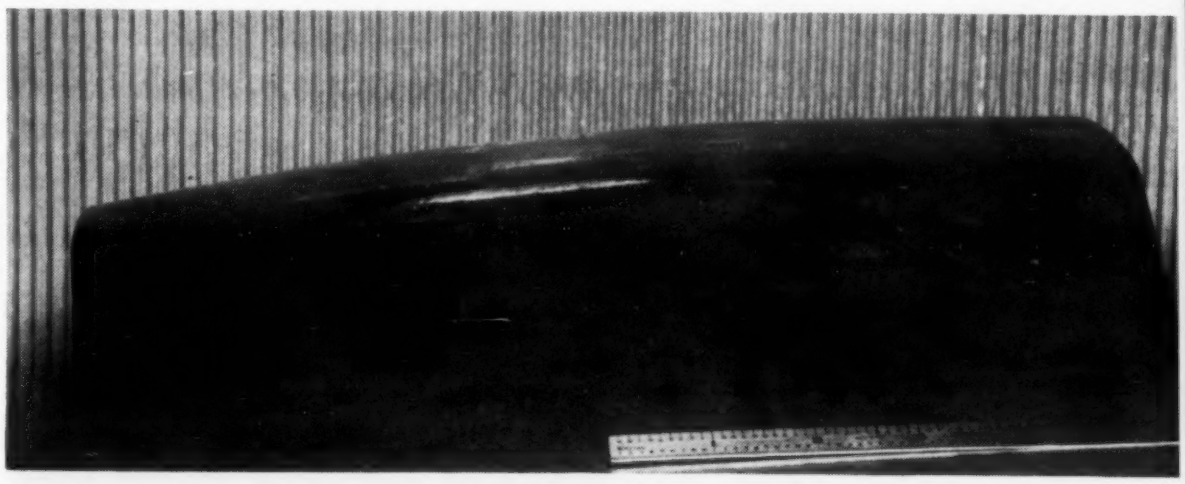
4. Mill annealed and solution heat treated parts are readily formed. Very little strain hardening occurred in either condition and ductile failures were typical, with local elongations as high as 18% in 1 in. Parts heat treated flat, as received from the mill, showed much less distortion than those heat treated after forming. The aging cycle produced very little distortion in unrestrained parts.

5. Springback is not easy to remove in full hard parts. An attempt was made to set formed parts after aging to the full hard state. These parts had edge curl ½ to 1½ in. wide. They pulled down to the block, but broke at the jaw as additional pressure was applied. Springback was not visibly reduced.

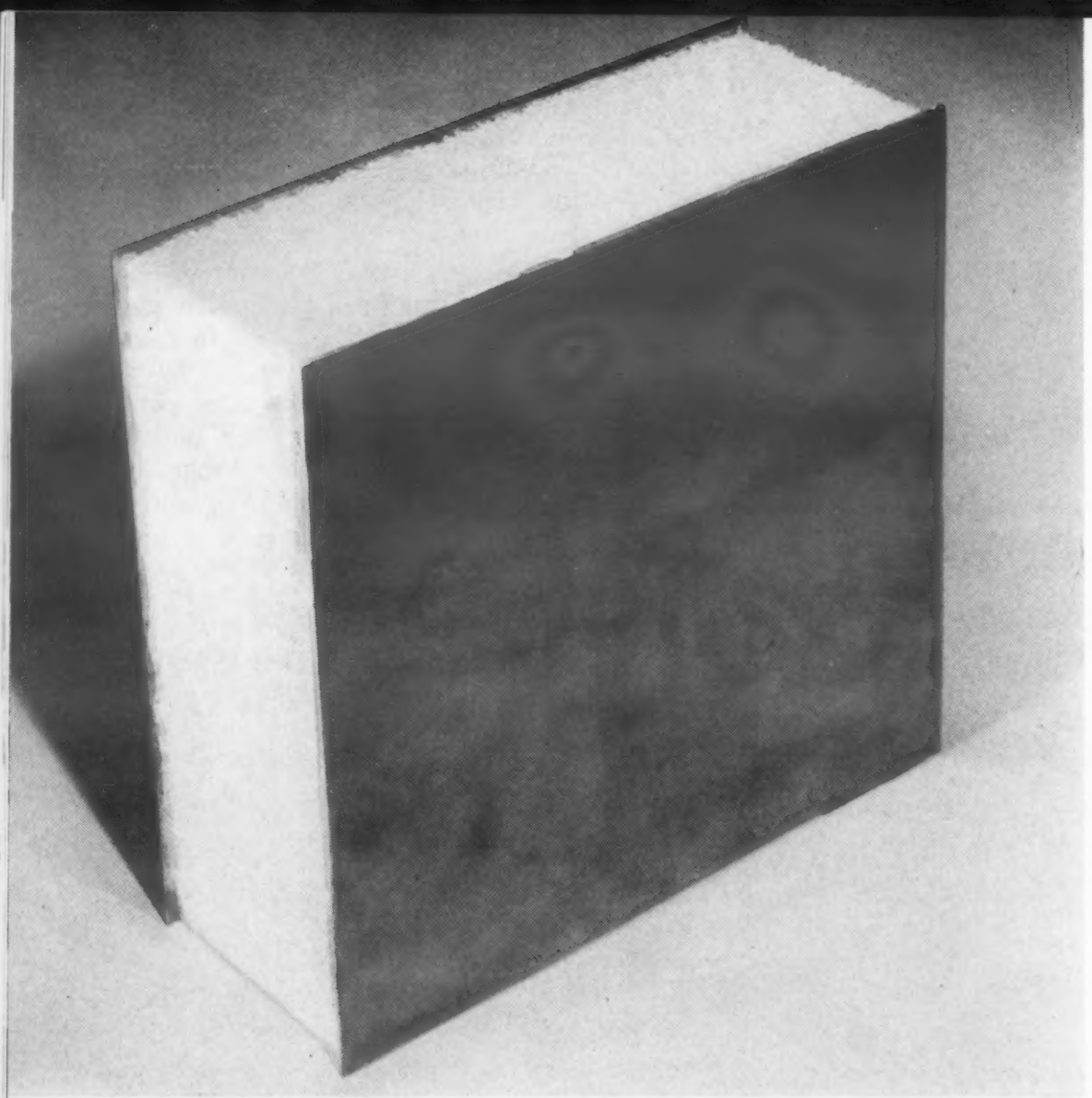


Springback, *shown here by transverse contour of part, varies from about ½ to 1½ in. on each edge.*

Edge condition *of the sheet is not critical in forming mild contoured parts. Note bad sheared condition.*



Contour *across center of stretch formed titanium alloy sheet.*



Sandwich structure *of the new foam is not only easy to make but also has unusually good stress distribution under load. Sandwich shown here has stainless steel facings.*

Polystyrene Beads + Thermosetting Resin =

Self-Expanding Thermoplastic Foam

Unlike currently available thermoplastic foams, this new material can be foamed in place without external heat or gas. It looks promising for sandwich structures and other uses.

by D. L. Graham, *Dow Chemical Co.*

■ A new plastics foam system, now under development, expands without the use of external heat to form a lightweight, structural foam. The system combines expandable polystyrene beads and an exothermic type thermosetting resin. When the two are mixed, and a curing agent and modifier added, the heat produced by the cure of the resin expands the beads to form the foam. As the beads expand they force most of the resin out to form a hard, chemical resistant surface on the part. The remainder of the resin acts as a binder and reinforcement between the individual expanded beads.

The new foaming method will work with several polymer systems. The two main requirements for success are: 1) the thermosetting resin must not chemically attack the gas-containing thermoplastic granules, and 2) the heat of reaction produced during the cure must be sufficient to soften and expand the granules. Because of the suitability of epoxy systems in such foams, the discussion in this article concerns polystyrene bead-epoxy combinations.

Characteristics

Unicellular foams produced by such systems have the following characteristics: 1) good adhesion to metals, glass, wood and several types of plastics, 2) good structural strength, 3) low water absorption, 4) low thermal conductivity, 5) no mold shrinkage, 6) good chemical resistance, and 7) wide density range.

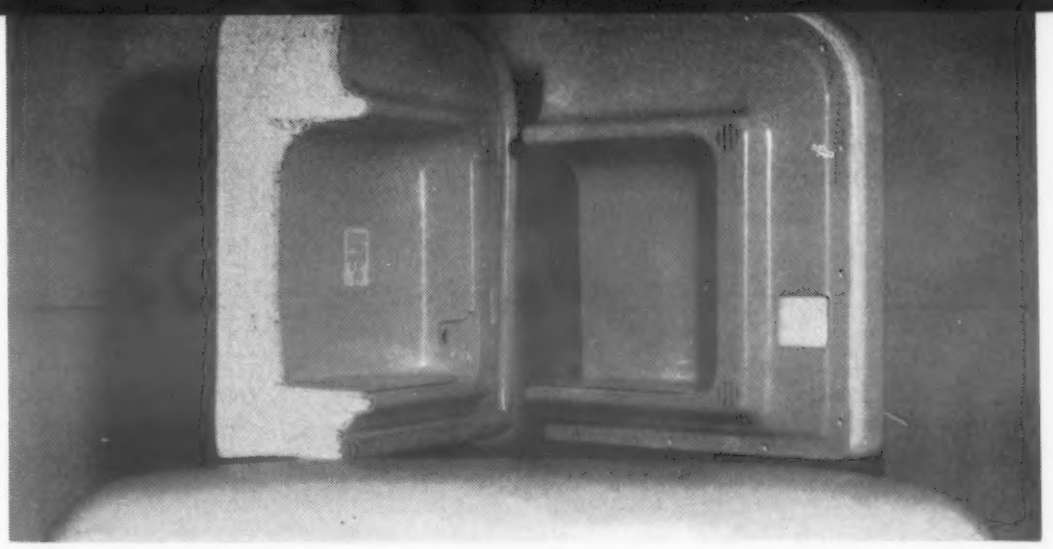
The accompanying table compares the property range of these foams with those of two other types of polystyrene foams. Fig 1 and 2 show how compressive strength and heat distortion temperature vary with bulk density.

Water resistance of the foams is excellent due to both the hard epoxy surface and the non-interconnecting nature of the cells. As in other polystyrene foams, thermal conductivity is low—on the order of 0.24 Btu/hr/sq ft/°F/in.

Densities range from approximately 5 to 20 lb per cu ft. To date, 1.4-mm dia beads have been

Availability

The foam materials described in this article are in the early stages of development and are in very limited supply. According to Dow, the methods, composition and products described are the subject of pending application for patents in the United States and principal foreign countries.



Low temperature insulation *is expected to be a major application for the foam. These developmental parts have molded polystyrene facings.*

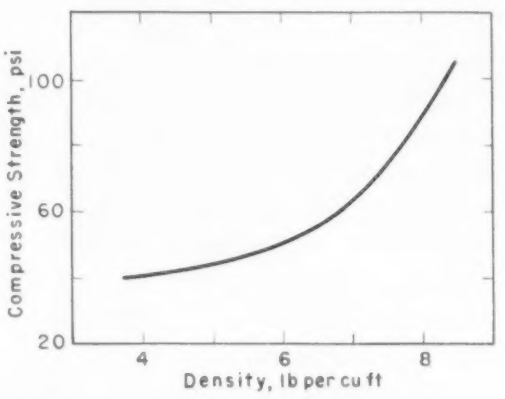


Fig 1*—Compressive strength, measured at 2.5% deformation, varies with density.*

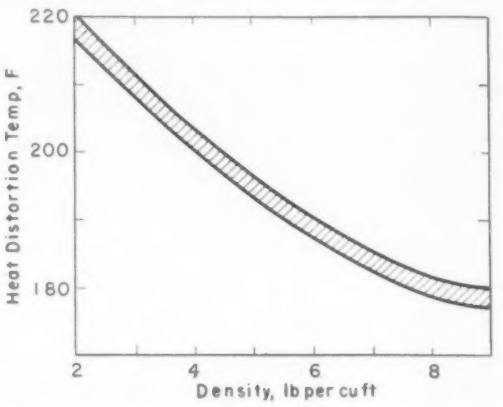


Fig 2*—Heat distortion temperature also varies with density.*

used to produce minimum densities of 6 to 8 lb per cu ft, whereas beads of 2.8 mm dia produce densities as low as 5.0 lb per cu ft. Density of a given molding is determined by 1) mass of the charge to the mold, 2) temperature of the resin, 3) temperature of the mold, 4) type of polystyrene bead used, 5) bead-resin ratio, 6) geometric shape of the mold, and 7) surface area-volume ratio.

Because of the resin-rich surface and the fact that fewer expanded beads are present near the surface, there is a density gradient throughout the structure of the foam. The gradient of a typical molded foam is shown in Fig 3. This gradient provides unusual strength characteristics which are particularly advantageous when the foam is used as a core material in sandwich structures. Because of the gradient, shear moduli increase from the center of the foam to the surface, providing a more balanced stress distribution under load. Though this increase in moduli is not linear, it is definitely an improvement over the typical sandwich which has a core of uniform density.

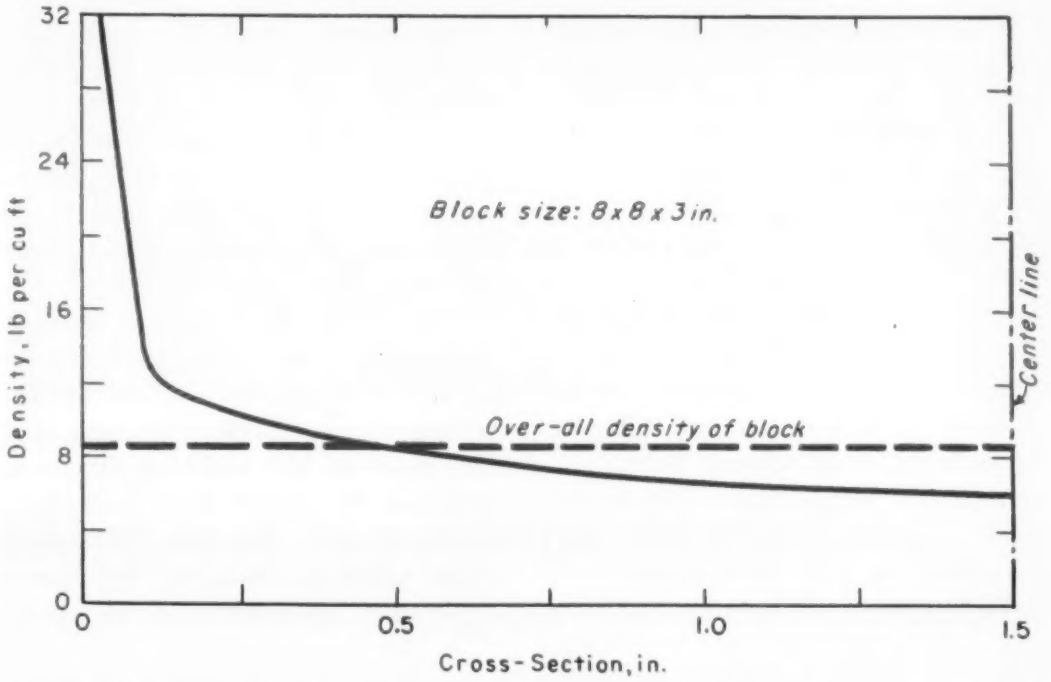


Fig 3*—Density gradient of typical sample measured from the outer surface to the centerline.*

Potential uses

Though the foams are still under development, they look promising for a variety of applications. Since they are structural foams, they should not be considered as a replacement for nonstructural void fillers. Properties of polystyrene-epoxy foams suggest applications such as sandwich structures, low temperature insulation, buoyant structures, and chemical resistant structures.

Sandwich structures—In addition to the good strength properties of the foams, the fact that expansion requires no external heat source is clearly advantageous in fabricating sandwich structures. Also, the epoxy resin provides excellent adherence to a variety of facing materials. Rigid materials such as stainless steel, aluminum, galvanized iron, glass, wood and high impact plastics sheet have been used successfully in combination with the foam.

Panels with glass-reinforced facings can be produced by an in-

teresting one-step operation. Dry glass cloth is placed in either or both surfaces of the mold. During the foaming process the resin is driven to the mold surface and saturates the cloth. Such panels are lightweight, are good thermal insulators, are protected on both sides by a reinforced structural skin, and have the unusual strength characteristics resulting from the density gradient of the core material. Applications for such sandwich structures include truck bodies, boats, furniture and aircraft.

Low temperature insulation—The unicellular construction, structural strength and low thermal conductivity of the foam also make it a promising material for refrigeration applications such as doors, cabinets, freezer lids and evaporator doors. Several prototypes of refrigeration parts have been made to demonstrate the material's adaptability to this use. A refrigerator door has been produced by expanding the foam between molded high impact polystyrene sheets. The outer and inner door liners, held by retaining molds during the molding operation, were formed prior to foaming. Doors have been formed successfully with molded–in lock mechanisms, latches, hinges, gaskets and fixtures. Again, the epoxy resin driven to the surface provides the adhesion to bond the inserts firmly in place. Thus, complete refrigerator doors can be molded in one operation without an external heat source. Other potential low temperature insulation uses include transportation, air conditioning and packaging.

Other uses—Buoyancy applications include boats, boat buoys, floats, pontoons, life preservers, water sports equipment, and flotation chambers in marine construction. Many other applications, such as reinforcement of sheet metal parts, encapsulation of electrical components, anticorrosive structures, and shock absorption applications in automobiles, are being considered.

Molding considerations

To mold a part, expandable polystyrene beads, thermosetting resin, curing agent and modifier are blended thoroughly and charged to the mold. The mold should be temperature-controlled and designed to withstand foaming pressures that are on the order of 10 to 50 psi, depending on density. Because of the adhesive nature of epoxies, molds used repeatedly must be provided with coatings of polytetrafluoroethylene, silicone, or other commercially available mold release agents.

Good foaming efficiency requires control of: 1) temperature of the reactants, 2) mass of the reaction mixture, 3) geometric shape of the mold, 4) mold temperature, and 5) thoroughness of mixing. These are the factors that determine completeness of mold filling, general moldability, voids, density, bonding to surface skins, speed of foaming and over-all cure time.

The time required to produce expansion of the polystyrene beads is dependent on the initial temperature of the reactants and the mass of the reaction mixture, and can be varied from less than 1 min to about 15 min. For maximum speed of foaming, the epoxy resin can be preheated to about 195 F. Preheating also lowers the viscosity of the resin, simplifying handling and mixing.

For optimum expansion, molds should be insulated or heated to reduce the loss of exothermic heat. Coring provides an efficient method of heating and cooling the molds for optimum moldability and shortest over-all cycle time.

When foaming between thin, flexible facing materials, it is well to back the facings with retaining molds to prevent distortion; facings of complex shape should be held against retaining molds securely. Use of retaining molds is particularly important in foaming against thermoplastic skins, since they would be likely to distort from the combination of temperatures and pressures produced by the reaction.

Formulation

The typical polystyrene bead-epoxy foam discussed in this article is Dow Experimental Plastic Q-4124.1. It is composed of four components in the following proportion (expressed as parts by weight):

Epoxy resin (Experimental Plastic Q-4115.2)	100
Expandable polystyrene beads (Experimental Plastic Q-865.2)	120
Curing agent (Dow ET-82)	20
Modifier (Dow ET-83)	10

The resin-bead ratio may be varied from 1:1 to 1:2 to obtain a range of densities and physical properties in the finished molding. A resin-bead ratio of less than 1:1 generally will not permit generation of sufficient exotherm to expand the beads. Generally the best foaming occurs when a 1:1.2 resin-bead ratio is used. Expandable beads measuring 1.4 and 2.8 mm dia may be used, either individually or in combination, to obtain various densities and physical properties. In general the larger diameter beads provide lower densities than the smaller beads.

COMPARISON OF PROPERTIES OF POLYSTYRENE FOAMS

Property	Beads and Resin (Exp. Plastic Q-4124.1)	Molded Beads	Pre-Expanded
Density, lb/cu ft	5–20	1.0–10.0	1.5–4.5
Compressive Strength, psi	45–150	8–250	16–140
Thermal Conductivity, Btu/hr/sq ft/°F/ in.	0.24	0.22–0.27	0.25–0.28
Water Absorption, lb/sq ft surface area	<0.01	<0.02	<0.20
Heat Distortion, Temp F	180–195	180	175

Source: Franson, G. R. and Kennedy, N. R., "Polystyrene — Versatile Foaming Material", presented at 13th National Technical Conference, Society of Plastics Engineers, Jan. '57.

Adapted from a paper presented at the 13th National Technical Conference, Society of Plastics Engineers, Jan '57.

M & M
MANUAL

General Electric Co.

Varnished cambric tapes *are used to insulate these electrical coils.*

Electrical Insulation Materials

by A. J. Monack, *Dept. of Physics, Newark College of Engineering*

This manual is a survey of the major types of solid insulation materials and their electrical, mechanical and thermal properties. The discussion covers all common forms: films, sheets and slabs, tapes, sleeving and flexible tubing, rigid tubing, rods and moldings. Information is arranged in a systematic pattern to aid the engineer in selecting the optimum insulation for a specific application.

MATERIALS & METHODS MANUAL NO. 137—APRIL 1957

TABLE 1—INITIAL SELECTOR CHART

Temperature Range \ Insulation Form	Films	Sheets and Slabs	Tapes	Sleeving and Flexible Tubing
Below 500 F	Polytetrafluoroethylene (H) Polytrichlorofluoroethylene (M) Polyamide (M) Polyester (M) Cellulose triacetate (M) Cellophane (M) Polyvinyl chloride (L) Polyvinyl chloride-acetate (L) Vinylidene chloride (L) Cellulose acetate (L) Cellulose acetate butyrate (L) Rubber (L) Polyethylene (L) Ethyl cellulose (L) Polystyrene (L)	Polytetrafluoroethylene (H) Pasted mica, silicone bonded (H) Glass-silicone laminate (H) Glass-polytetrafluoroethylene laminate (H) Polytrifluorochloroethylene (M) Polyamide (M) Vulcanized fibre (M) Wood (L to M) Pasted mica, organic bonded (L to M) Plastics laminates (L to M)[b] Cellulosic (L) Polystyrene (L) Methacrylate (L)	Polytetrafluoroethylene (H) Polytrichlorofluoroethylene (M) Polyamide (M) Cellophane (M) Polyester (M) Paper (L) Woven acetate fiber (L) Cellulose acetate (L) Ethyl cellulose (L) Rubber (L) Woven cotton (L) Polystyrene (L) Polyvinyl chloride (L) Polyvinyl chloride-acetate (L) Polyethylene (L)	Polytetrafluoroethylene (H) Polytrichlorofluoroethylene (M) Silicone rubber (M) Polyamide (M) Woven polyester fiber (M) Braided cotton (L) Braided rayon (L) Braided silk (L) Braided linen (L) Woven acetate fiber (L) Polyvinyl chloride (L) Natural rubber (L) Synthetic rubber (L) Polyethylene (L)
500 to 1000 F	Ribbon glass (M)	Ceramoplastics—glass bonded micas (M to H) Muscovite mica—small sheets (M to H) Pasted muscovite mica, inorganic bonded (M to H)	Ribbon glass (M) Woven glass fiber (L to H) Woven asbestos (L to H)	Woven asbestos (L to H) Woven glass fiber (L to H)
Above 1000 F		Ceramics—small slabs only (H) Glass (L to H) Amber mica—small sheets (M) Pasted amber mica, inorganic bonded (M) Built-up synthetic mica, inorganic bonded (M) Reconstituted mica, inorganic bonded (L to M)	Woven fibrous silica (H)	Woven fibrous silica (H)

[a] Letters L, M and H after each material indicate portion of temperature bracket for which insulation is suitable—lowest, middle or highest. After most of the possible insulations have been eliminated on the basis of their form and maximum temperature, further selection can be made by referring to the mechanical, physical and electrical properties listed in the other charts in this article.

■ The primary function of an electrical insulation is to confine the flow of a current to a desired path. In performing this function the insulation may also serve as a structural element by maintaining spacings or positions. Electrical insulation is also used to protect the surfaces of conductors from adverse environments such as moisture and chemicals, and to fill spaces or voids where corona discharge is liable to occur.

In general, electrical insulations are classified as gases, liquids or solids. Data presented in this manual will be confined to the most widely used, or solid, forms. Chemically, these solid insulations may be organic, inorganic, or combinations thereof. Many of the electrical and physical properties of organic and inorganic insulations overlap; the most striking differences are in resistance to heat and in permanence of size and shape.

In organizing these data it has been assumed that the most convenient method of selecting an insulation material is to consider first the form or shape it must have and the temperature requirements it must meet. Certain electrical, physical or mechanical requirements, of course, may dictate the choice of material; however, the approach used in this article is usually more convenient.

Once the parameters of form and temperature have been established, a considerable number of materials can be ruled out as unsatisfactory. Selection from the remaining materials can then be made on the basis of their electrical, mechanical and thermal properties.

FOR ELECTRICAL INSULATIONS[a]

Rigid Tubing	Rods	Moldings
Polytetrafluoroethylene (H) Glass-silicone laminate (H) Pasted mica (M to H) Polyamide (M) Vulcanized fibre (M) Polytrichlorofluoroethylene (M) Plastics laminates—grades XX, XXX, C, CE, L, LE, G3, G5, G6, G7, N1 (L to M)[c] Methacrylate (L) Polystyrene (L) Polyvinyl chloride (L) Polyvinyl chloride-acetate (L) Cellulose acetate butyrate (L) Pasted mica paper (L)	Polytetrafluoroethylene (H) Glass-polytetrafluoroethylene laminate (H) Polytrichlorofluoroethylene (M) Vulcanized fibre (M) Polyamide (M) Plastics laminates—grades XX, XXX, C, CE, L, LE, G3, G5, G6, G7, N1 (L to M)[c]	Polytetrafluoroethylene (H) Organic cold molded (H) Silicone, glass fiber or mineral filled (H) Diallyl phthalate (H) Polytrichlorofluoroethylene (M) Alkyd, glass fiber or mineral-filled (M) Phenol-formaldehyde (M) Melamine-formaldehyde (M) Polyamide (M) Pasted mica (L to H) Aniline-formaldehyde (L) Urea-formaldehyde (L) Hard rubber (L) Polyethylene (L) Polyvinyl chloride (L) Polyvinyl chloride-acetate (L) Vinylidene chloride (L) Polystyrene (L) Cellulosic (L)
Pasted mica, inorganic bonded (H)	Ceramoplastics—glass bonded micas (M to H)	Ceramoplastics—glass bonded micas (M to H) Inorganic cold molded (M to H) Glasses, low temperature (M to H)
Ceramics (H) Glass (M to H)	Ceramics (H) Glass (L to H)	Steatite (H) Fluxed alumina (H) Cordierite (H) Titanate ceramics (H) Forsterite (H) Zircon porcelain (H) Lithia porcelain (H) Pure oxides (H) Synthetic micas, hot pressed (M) Electrical porcelain (M to H) Glasses (L to H)

[b] All other grades besides those listed above.
[c] Based on NEMA recommendations for industrial laminated thermosetting products. Other special grades are available from laminates manufacturers.

Table 1 has been prepared to aid the designer in this selection process. In this table, the various types of insulation are grouped according to their forms and temperature limits. Detailed data on these insulations can be found by consulting the appropriate properties charts and the following discussion.

Elastomers and Flexible Plastics

These materials (see Table 3) are used chiefly for wire and cable insulation; occasionally they are used for plugs and connectors, and in housings for electrical and electronic components. Fabrics are often used with the wire and cable covering materials to increase their mechanical strength and resistance to cut-through.

Elastomeric insulations are capable of being stretched repeatedly to 150% or more of their normal length with no permanent set or loss of force. The natural elastomeric materials in common use include: natural rubber, guttapercha, balata and paragutta. Synthetic elastomeric materials include: styrene, acrylonitrile, neoprene, butyl, silicone and polysulfide rubbers. Polyvinyl chloride and its copolymers, polyethylene and the polyfluoroethylenes are commonly used flexible plastic insulations.

Waxes

Insulating waxes are used in bulk form as potting compounds or as thin coatings to prevent the formation of continuous films of moisture. In recent years their use has diminished somewhat due to the superiority of a number of organic resins. The epoxies are considerably superior to waxes for potting; and silicone, fluorocarbon and other resins are much more satisfactory for the formation of hydrophobic surfaces. Typical properties of representative types of insulating waxes are listed in Table 2.

Paper

The chief function of paper is that of a separator or as a wrapping for wire insulation. Untreated paper is roughly equivalent to air as an insulator and when completely dry its resistivity is good—about 10^{15} ohm-cm. Untreated paper usually contains 7-12% moisture and, because of its absorption tendencies, it is usually treated, even when it is serving only as a separator. The electrical properties of papers treated with varnish or lacquer essentially match those of the treating materials.

Electrical properties and maximum operating temperatures of a wide range of insulating papers are listed in Table 4. (Properties of papers used in composite insulations are given in Table 6.)

Insulating papers may be divided into inorganic and organic (cellulosic) materials. The inorganics are preferably treated with silicone varnishes or fluorocarbons, but may be treated with epoxy or polyester resins. Organic

TABLE 2—PROPERTIES OF ELASTOMERS AND FLEXIBLE PLASTICS
(See also page 147)

Property / Material	Max A.C. Volt, kv	Dielec Const (60 cps)	Power Factor (60 cps)	Dielectric Strength, v/mil		Vol Res, ohm-cm	Water Perm (7 days), mg/sq in.	Water Abs (24 hr), %	Max Svc Temp, F	Min Svc Temp, F	Brittle Temp, F
				A.C.	D.C.						
Natural Rubber	3[a]	2.6-5	0.008-0.040	600	1500	10^{17}	7	—	167	−40	−72
GR-S Synthetic Rubber	3[a]	2.7-5	0.009-0.040	600	1500	10^{15}	8	—	167	−65	—
Butyl Synthetic Rubber	28	3-5	0.01-0.04	400	1000	10^{16}	5	—	176	−40	−58
Neoprene	0.6	7	0.02	300	—	10^{12}	25-100	—	194	−22	−40
Silicone Rubber	5	3	0.007	260-700	—	10^{14}	—	0.25-1.00	392	−67	−121
Polyvinyl Chloride	0.6	5-6	0.10-0.15	300-800	2000	10^{12}-10^{14}	5	0.3	149-176	−22 to +41	+6 to −67
Polyvinyl Chloride-Acetate	0.6	5-9	0.08-0.15	400-900	—	10^{11}-10^{13}	—	0.1	149-176	—	—
Polyethylene	15	2.3	0.004	400-1200	—	10^{13}	1	Slight	176	−76	−94
Polytetrafluoroethylene	5	2.0-2.2	0.0005	450-900	—	10^{16}	—	Nil	392	−67	−103
Polytrifluorochloroethylene	5	2.3	0.015	500-900	—	10^{18}	—	Nil	302	−65	—
Gutta-percha	0.6	2.56-4.13[b]	0.0009-0.0300[b]	200-500	—	10^{15}	—	—	140	14	−9 to −33
Polysulfide Rubber	—	7-9.5[b]	0.001-0.005[b]	250-350	—	10^{11}-10^{12}	—	—	275	−65	—

a 28 kv for ozone resisting grade.
b 1000 cps.

TABLE 3—PROPERTIES OF WAXES
(See also page 147)

Type	Dissipation Factor		Dielectric Constant		Volume Resistivity, ohm-cm	Surface Resistivity, ohm/square		Melting Point, F
	60 cps	10^6 cps	60 cps	10^6 cps		50% R.H.	90% R.H.	
Beeswax	—	0.01-0.03	2.8-3.1	2.5-2.9	10^{14}-10^{15}	6×10^{14}	5×10^{14}	113-147
Paraffin	0.0002-0.0090	0.0002-0.0090	2.1-2.5	2.1-2.5	10^{14}-10^{16}	9×10^{15}	6×10^{15}	97
Cerese Wax	0.0009-0.0060	0.0004-0.0030	2.3-2.6	2.3-2.6	10^{18}	10^{17}	10^{17}	135
Cetylacetamide	0.025	0.002-0.005	2.6	2.4-2.5	—	—	—	282
Chlorinated Naphthalene	0.002-0.100	0.0001-0.005	3.1-5.6	2.9-5.4	10^{13}-10^{14}	6×10^{15}	5×10^{11}	95-201
Hydroxystearin	14.2	0.027-0.340	0.12	3.1-3.2	—	—	—	189
Polybutene	0.0002	0.001	2.3	2.3	—	—	—	—

papers are treated with conventional (oleoresinous) or thermosetting varnishes and include:

Kraft paper, usually consisting of a tan sulfate paper which is easily impregnated with varnish. It is commonly used for cable and wire insulation, for wrapping coil layers, and as a backing for composites. It is also used as a base for laminated plastics sheets and tubes.

Rag paper posesses good abrasion resistance and consequently is useful for slot insulation. It is also good for spacers and washers. Very thin (0.0005 in.) condenser papers may be either all rag or rag plus pulp.

Fish paper is a special electrical grade of vulcanized fibre and is excellent for slot and cell liners.

Rope (Manila) paper is made of Manila hemp or old rope. Because of its long fibers it is the strongest of the papers and is used in cables, in composites, and in slot, cell and core insulation.

Japanese (Jap) paper is made from mulberry wood pulp. In 1-mil thickness it is used as a backing for mica flake.

Pressboard or fuller board is made from rag, or rag plus pulp, and is readily impregnated with oil. The rag board is easily formed and bent, whereas the pulp board is somewhat stiffer. These materials are chiefly used for transformer insulation; they are also useful for spacers, collars, shields, etc.

Fabrics

Untreated fabrics are used in the form of cords, sleevings, tapes and threads as components in wire coverings and as wrappings in oil filled transformers. Fabrics in the form of cloths, tapes, ribbons and sleevings are used extensively as carriers for impregnating insulation materials; typical impregnants are oleoresinous varnish, silicone varnish, synthetic rubber and vinyl, isocyanate and polytetrafluoroethylene impregnants. Properties of the various treated and untreated fabric insulations are listed in Table 5.

Fabrics perform two other important functions in insulation. In the form of cloth they are used as base materials in plastic laminates (see Table 11). In the form of fibers, filaments and chopped fabrics, they act as reinforcements

TABLE 4—PROPERTIES OF PAPERS
(See also page 147)

Type of Paper and Treatment	Thickness, mils	Tensile Strength, lb/in. width	Dielectric Strength, v/mil	Insulation Class	Max Operating Temp, F	Dielectric Constant (60 cps	Power Factor (60 cps)
ORGANIC PAPERS							
Fish—Untreated	5	—	450	A	220	—	—
Rag—Untreated	7-20	—	300	A	220	—	—
Pressboard (rag and paper)—Untreated	31-125	—	150-200	A	220	—	—
Pressboard (yellow)—Untreated	10-125	—	200-500	A	220	—	—
Rag—Varnish	6.5-27	350-1600	300-460	A	220	2.0	—
Fish—Varnish	4-134	12-1800	150-300	A	220	2.0	—
Pressboard—Varnish	7-500	—	150-400	A	220	2.0	—
Kraft—Varnish	0.4-15	250-260	160-1100	A	220	2.0	—
Rope—Varnish	0.9-30	10-70	—	A	220	2.0	—
Japanese—Varnish	—	—	—	A	220	2.0	—
INORGANIC PAPERS							
Asbestos—Untreated	2-10	0.2-1.2	280-340	C	725	3.4	0.28
Mica—Untreated	1.5-4	0.2-0.7	500-700	C	900	1.2-1.6	0.0008-0.0015
Glass Fiber—Untreated	2-7	0.3-1.0	—	C	1100	1.07	0.0002
Ceramic—Untreated	5-80	0.1-1.0	—	C	2000	1.08	0.0002
Glass Flake—Alkyd	10	—	100	B	220	2.45	1.99
Glass Flake—Phenolic	9	—	120	B	220	1.93	1.26
Glass Flake—Silicone	9	—	105	H	500	1.91	0.96
Asbestos—Vinyl Acetate	3-15	8-35	290-370	B	340	—	—
Mica—Silicone	1.5-30	10	400-800	H	500	2·2.2.4	0.002-0.003
Mica—Epoxy	3-30	—	800	B	265	—	—
Glass Fiber—Silicone	—	0.6-6.4	—	H	500	—	—
Glass Fiber—Teflon	1.5-6.5	1.2-2.5	180-250	H	400	—	0.05-0.10
Ceramic—Silicone	12	4-6	—	H	500	—	—
Asbestos—Silicone	3-9	6-13	290-330	H	500	—	—

in plastic moldings (see Table 10).

Fabrics for electrical insulation are made from three types of fibers: natural organic, inorganic and synthetic organic.

Natural organic fibers employed for insulation fabrics are cotton, flax and silk. Because of its high cost silk has been replaced almost entirely by synthetic fibers.

Inorganic fibers are of two types: natural, such as asbestos, and manufactured such as glass.

Asbestos insulation is usually made in the form of roving, lap, yarn and cloth. It is often blended with cotton or other fibers to increase its strength and flexibility; these advantages, however, are gained at the expense of maximum service temperature. Insulation with a 75-80% asbestos content (Commercial Grade) has a service temperature of 400 F as compared to 900 F for 99-100% asbestos (AAAA Grade).

Glass fiber may be made from a number of glass compositions, including vitreous silica. Woven into cloth, treated and untreated glass fiber is used in a variety of applications where resistance to moisture and high temperatures is important.

Synthetic organic fibers and filaments that have proved useful for fabric insulation include rayon, nylon and cellulose acetate. Also used occasionally are acrylics such as Orlon or Acrilan, vinyls such as Saran and Vinyon, and polyesters such as Dacron.

TABLE 5—PROPERTIES OF FABRICS
(See also page 148)

Type of Fabric and Treatment	Dielectric Strength, v/mil	Thickness, mils	Breaking Strength, lb/in. width	Max Operating Temperature, F
Cotton—Untreated	50–100	3.5–25	20–40	195–220
Cotton—Varnish	400–1500	4.5–25	40–60	220
Rayon—Varnish	500–1200	2.2–22	25	220
Asbestos—Untreated	50–100	26–50	32–70	255–570
Asbestos—Varnish	400–1200	10–60	—	265
Asbestos—Silicone Varnish	700–1500	10–62	—	480
Linen—Varnish	250–500	8–10	—	220
Silk—Varnish	1000–1900	2–8	20	220
Glass—Untreated	50–100	1.5–25	70–450	535–570+
Glass—Varnish	500–1200	3–30	70–550	265
Glass—Silicone Varnish	1000–1500	3–30	70–450	480
Glass—Silicone Rubber	400–1200	4–32	40–500	480
Glass—Isocyanate	360–1300	3–23	—	300
Glass—Teflon	1200–1400	3–14	—	750
Fibrous Silica—Untreated	50–100	140–150	—	3630

Minnesota Mining and Mfg. Co.

Yellow flatback paper *tape is used in this rotor to hold disk and insulate core from coil windings.*

Composite Insulations

Composite insulations possess a combination of properties not present in a single material. Typical of the composites commonly used are mica splittings, which are backed with or sandwiched between paper or fabric and held together by an oleoresinous varnish, shellac or similar material. Similarly, mica paper is strengthened by backings of glass cloth or polyester film on one or both sides, with an organic or silicone varnish as a binder. Properties of a number of important types of composites are listed in Table 6.

Electrical Tapes

In general, electrical tapes are used to insulate, to hold, or to serve as spacers. They are commonly employed for wrapping coils or conductors, for insulating splices, and for holding and bending insulating materials.

As can be seen from Table 7, electrical tapes are made from nearly all available plastics film materials (Table 9), as well as paper (Table 4), cloth (Table 5), composites (Table 6), and laminated and reinforced combinations (Table 8). Rubber tapes are also used extensively in insulation for wrapping and splices (their properties are essentially those given for elastomeric insulations in Table 3).

Glass insulation tapes are available in the form of flexible ribbon in thicknesses of 0.001 to 0.030 in., and in widths of ⅛ to 14 in. Within certain limitations, the thinner ribbons can be twisted,

Basic Electrical Terms: What They Mean

Insulator—Commonly defined as a material with such low conductivity that it restrains or entirely prevents the flow of current. For practical purposes solids are divided into three classifications: conductors, with resistivities from 10^{-6} to 10^{9} ohm-cm; poor conductors (semiconductors) with resistivities from 10^{9} to 10^{6} ohm-cm; and good insulators, with resistivities from 10^{6} to10^{20} ohm-cm.

Dielectric constant—The property that represents the electrostatic energy stored in a material per unit volume per unit potential gradient. At a given frequency it is the ratio of the capacitance of a capacitor in which the material is the dielectric to the capacitance of the same capacitor with a vacuum as the dielectric. For most purposes, air (instead of a vacuum) may be taken as the comparison dielectric.

Phase angle—The angular difference in phase between the sinusoidal voltage applied to the dielectric and the component of the resulting current. A perfect insulator would have a phase angle of 90 deg.

Loss angle—The difference between the phase angle and 90 deg (hence, the complement of the phase angle). A perfect insulator would have a loss angle of 0 deg.

Dissipation factor—The cotangent of the phase angle, or the tangent of the loss angle, for a given material. It is the reciprocal of Q, the quality factor, and is equal to the ratio of resistance to reactance. It is also the ratio of the energy dissipated to the energy stored per cycle.

Power factor—The cosine of the phase angle or the sine of the loss angle for a given material. It is the ratio of resistance to impedance. When the tangent of the loss angle is less than 0.1, the power factor differs from the dissipation factor by less than 0.0005.

Loss factor—Product of the dissipation factor and dielectric constant. It is a measure of actual loss in the insulation, since the dissipation factor is the fraction of energy lost during a cycle and the dielectric constant is proportional to the energy stored in the dielectric.

Dielectric strength—The maximum potential gradient that an insulator can withstand without rupture. It is commonly expressed in volts per mil. The relation between dielectric strength and thickness is not linear.

Volume resistivity—Ratio of d.c. potential gradient (parallel to the current in the insulation) to the current density. Commonly designated as microhm-centimeters.

Surface resistivity—Ratio of d.c. potential gradient (parallel to the current along the surface) to the current per unit width of surface. Commonly designated by ohms per square where the size of the square is immaterial.

Arc resistance—Total elapsed time until failure occurs when an arc is passed between two electrodes in contact with an insulation surface. ASTM standard test D-495 uses an arc of high voltage and low current and time to failure is measured in seconds. The insulation is said to "track" when a conducting path, usually the result of carbonization under the action of the arc, forms between the electrodes.

AIEE insulation classification—

Class	Material	Max Temp, F
O	Organic, not impregnated	195
A	Organic, impregnated	220
B	Inorganic, organic binder	265
H	Inorganic, silicone binder	355
C	Completely inorganic	355+

rolled and wrapped. Applications are limited somewhat by the inherent brittleness of the material; however, combination with a plastic can help to overcome this disadvantage.

Electrical tapes may be used without adhesive, or they may be coated with a pressure sensitive adhesive on one or both sides (for further data on electrical tapes see "Pressure Sensitive Tapes," M&M, Mar '56, p 136). Some of the pressure sensitive tapes available are: crepe and flatback paper; cotton, glass and acetate cloth; acetate and polyester film; acetate fiber; and Teflon.

Laminated tapes are made of two or more materials bonded together. Typical examples are acetate film laminated to rope paper, and acetate film laminated to acetate cloth. The acetate laminates have high strength, dimensional stability and resistance to water vapor.

Plastics Films, Sheets

Plastics insulating films and sheets are used primarily as wrappings for conductors. The materials used in these films and sheets are in nearly every case identical to the materials used in plastics insulation moldings. The difference is one of form.

Available film materials fall into the usual categories of cellulosics, vinyls, polyethylenes, styrenes, polyamides and polyesters. Rubber hydrochloride is also used because of its impermeability to moisture. Important properties of these materials are summarized in Table 9.

Plastics Moldings

Plastics for molded insulations are generally of the same type as used for other forms of insulation. The thermosetting plastics used in filled molded insulations, for example, are not different from those used in insulation laminates.

The important physical and electrical properties of the various types of molded plastics insula-

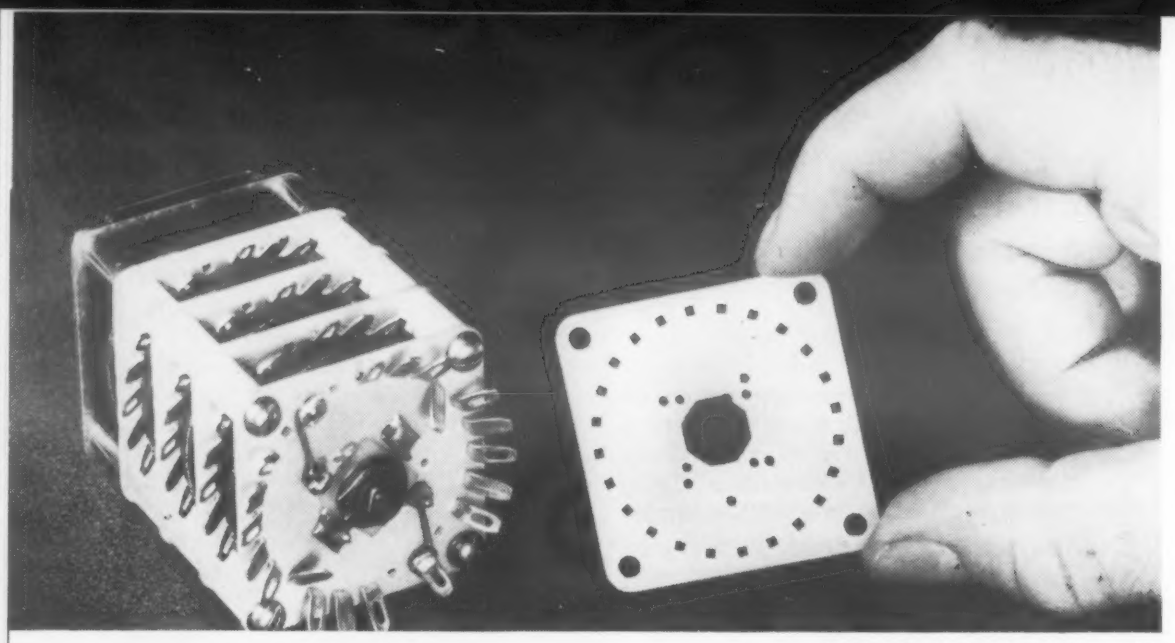
TABLE 6—PROPERTIES OF COMPOSITES
(See also page 150)

Binder	Material	Thickness, mils	Dielectric Strength, v/mil	Insulation Class	Max Operating Temperature, F
Conventional Varnish	Rag Paper (5 mils)—Varnished Cloth (7 mils)	—	750	A	220
	Rag Paper (10 mils)—Varnished Cloth (7 mils)	—	700	A	220
	Rag Paper (15 mils)—Varnished Cloth (10 mils)	—	450	A	220
	Fish Paper (5 mils)—Varnished Cloth (5 mils)	—	800	A	220
	Fish Paper (10 mils)—Varnished Cloth (7 mils)	—	750	A	220
	Fish Paper (15 mils)—Varnished Cloth (7 mils)	—	500	A	220
	Jap Paper—Mica Splittings—Jap Paper	3-6	300-500	A	220
	Rope Paper—Mica Splittings—Rope Paper	3-6	300-750	A	220
	Jap Paper—Mica Splittings—Fish Paper	10-12	300-500	A	220
	Jap Paper—Mica Splittings—Cotton Cloth	5.5-7.5	300-500	A	220
	Jap Paper—Mica Splittings—Rayon Cloth	5	300-500	A	220
	Jap Paper—Mica Splittings—Glass Cloth	5.5-8.0	300-500	A	220
Organic Varnish or Resin	Mica Splittings—Cellophane	5-15	—	A	220
	Mica Splittings—Glass Cloth	4-20	900-1000	B	265
	Glass Cloth—Mica Splittings—Glass Cloth	6-25	1000-1200	B	265
	Glass Cloth—Mica Paper—Glass Cloth	8-20	550-1000	B	265
	Polyester Film—Mica Paper—Polyester Film	5-20	700-1000	B	265
	Polyester Film—Mica Splittings—Polyester Film	4-20	1000-2000	B	265
Silicone Varnish	Mica Splittings—Glass Cloth	8-15	800-1000	H	500
	Glass Cloth—Mica Splittings—Glass Cloth	9.5-20 0	400-1300	H	500
	Polyester Film—Mica Splittings—Polyester Film	4-20	1000-2000	H	500
	Glass Cloth—Mica Paper	5-20	800	H	500
	Glass Cloth—Mica Paper—Glass Cloth	10-20	750	H	050

TABLE 7—PROPERTIES OF UNREINFORCED TAPES
(See also page 150)

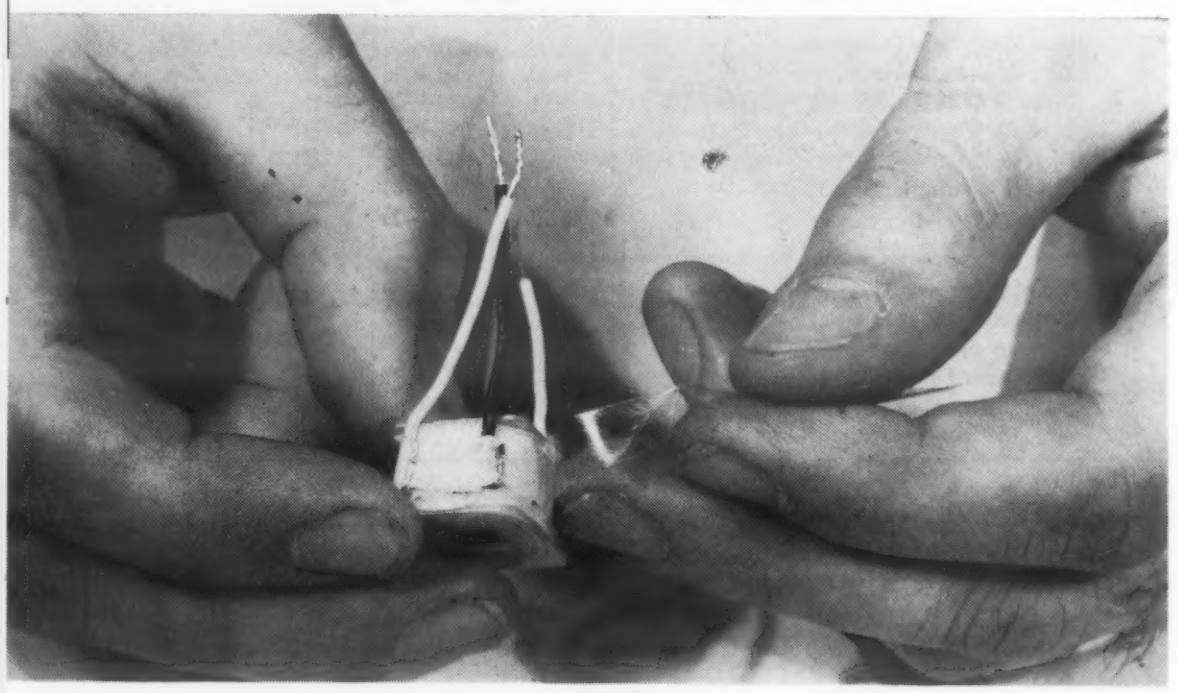
Type of Tape	Thickness, mils	Dielectric Strength, v/mil	Tensile Strength, lb/in. width	Tear Resistance	Insulation Class
Crepe Paper	10	125-200	15-30	Low	A
Flatback Paper	7	125-200	25-30	Fair	A
Cotton Cloth	11	150-250	40-90	Very good	A or O
Acetate Cloth	7-9	200-300	40	Fair	A or O
Glass Cloth (rubber adhesive)	6-8	200-500	140-200	Very good	B
Glass Cloth (silicone adhesive)	6-8	200-500	140-200	Very good	H
Acetate Film	2.0-3.5	1400-1600	15-30	Fair	A
Polyester Film	0.2-3	2000-7000	5-60	Excellent	A or B
Acetate-Rope Fiber	6-10	500-800	30-40	Fair	A
Acetate-Acetate Cloth	10	550-700	55-70	Fair	A or O
Ribbon Glass	1-3	3000[a]	—	—	C
Polytetrafluoroethylene	0.5-13	1000-4000	1-30	Excellent	B and H
Polytrifluorochlorothylene	2-10	2000-5000	10-50	Excellent	B
Polystyrene	0.4-10	1000-3000	5-120	Good	A or O
Vinyl Chloride	6-20	700-1500	20-60	Very good	A or O
Vinylidene Chloride	0.5-10	1000-1800	5-100	Very good	A or O
Ethyl Cellulose	3-10	800-3000	30-100	Good	A or O
Polyethylene	0.5-10	1000-5000	1-35	Excellent	A or O
Irradiated Polyethylene	2-10	1000-4000	5-25	—	A
Polyamide	1-10	800-1500	10-100	Good	A or O
Cellophane	1-4	—	10-30	Good	B
Cellulose Triacetate	1-10	—	10-150	Fair	A
Vinyl Chloride-Acetate	1-10	1000-1500	5-45	Very good	A or O

[a] Thickness of 1 mil.



National Vulcanized Fibre Co.

Glass-silicone laminate *with high resistance to heat and moisture forms plates in miniature rotary switch.*



Minnesota Mining and Mfg. Co.

Polyester backed insulating tape, *in thickness of only 3 mils, is designed for use in fine wire coils, transformers and other miniature components.*

tion are given in Table 10. For purposes of classification these materials can be arranged as follows:

Thermosetting plastics — Those plastics which generally soften only once under heat and do not soften on subsequent heating. This group of insulating materials includes phenolics, amines (ureas and melamines), anilines, polyesters (alkyds and allyls), silicones and organic cold molded materials.

Thermoplastics — Those materials that usually can be softened repeatedly by heating and made rigid again by cooling. This group includes cellulosics, acrylics (methyl methacrylate), styrenes (polystyrene, modified polystyrene and styrene copolymers), fluorocarbons (polytetrafluoroethylene and polytrifluorochloroethylene), vinyls (polyvinyl chloride, polyvinyl chloride-acetate and vinylidene chloride) and polyamides (nylon).

Filler materials used in molded insulators include short fibers, chopped fabrics, and granular or flake fillers such as wood flour, mica and diatomaceous earth.

Plastics Laminates

Plastics laminates consist of a reinforcing material impregnated with a thermosetting resin. The material is laminated in multiple layers, then cured with heat or pressure to form dense, hard sheets, tubing or rods with good

TABLE 8—PROPERTIES OF REINFORCED TAPES
(See also page 150)

Type of Tape	Tensile Strength, lb/in. width	Dielectric Strength, v/mil[a]
Cellulose Acetate-Rayon	200	1400
Cellulose Acetate-Glass	325–500	1400
Polyester-Rayon	200	2000
Polyester-Nylon	80–90	2000
Vinyl-Glass	500	1600
Paper-Glass	240	100–200
Polyethylene-Glass	135	1200
Vinylidene Chloride-Glass	65	1200

[a] Average values for thickness of 3 mils.

mechanical properties. Although not common, an insulation laminate may contain two or more types of base material and two or more resins.

The base materials used are cellulose paper, cotton fabric and web, glass fabric and mat, asbestos paper and fabric, nylon, and occasionally Orlon. Wood veneers and insulating boards are sometimes impregnated or coated with various resins, also. The most common binders for laminated plastics are phenolics, melamines, epoxies, diallyl phthalates, polyesters, silicones and fluorocarbons. Significant properties of these laminates are given in Table 11. (Considerable supplementary data on electrical and mechanical properties of insulation laminates are contained in "Selecting Plastics Laminates for Industrial Use," M&M, Feb '57, pp 130-138).

Insulation laminates are easily machined and possess good strength and dimensional stability. Sheet sizes vary from 36 x 36 to 49 x 108 in. Tubing is produced in sizes ranging from 3/32 in. i.d. up to 72 in. o.d., in wall thicknesses from 0.0075 to 2 in. Round, square, rectangular, oval and irregular shapes are available. Molded rods are available in diameters from 3/32 to 4 in.

Vulcanized fibre is a dense material of partially regenerated cellulose made by treating paper with zinc chloride to obtain a gelled substance; the zinc chloride

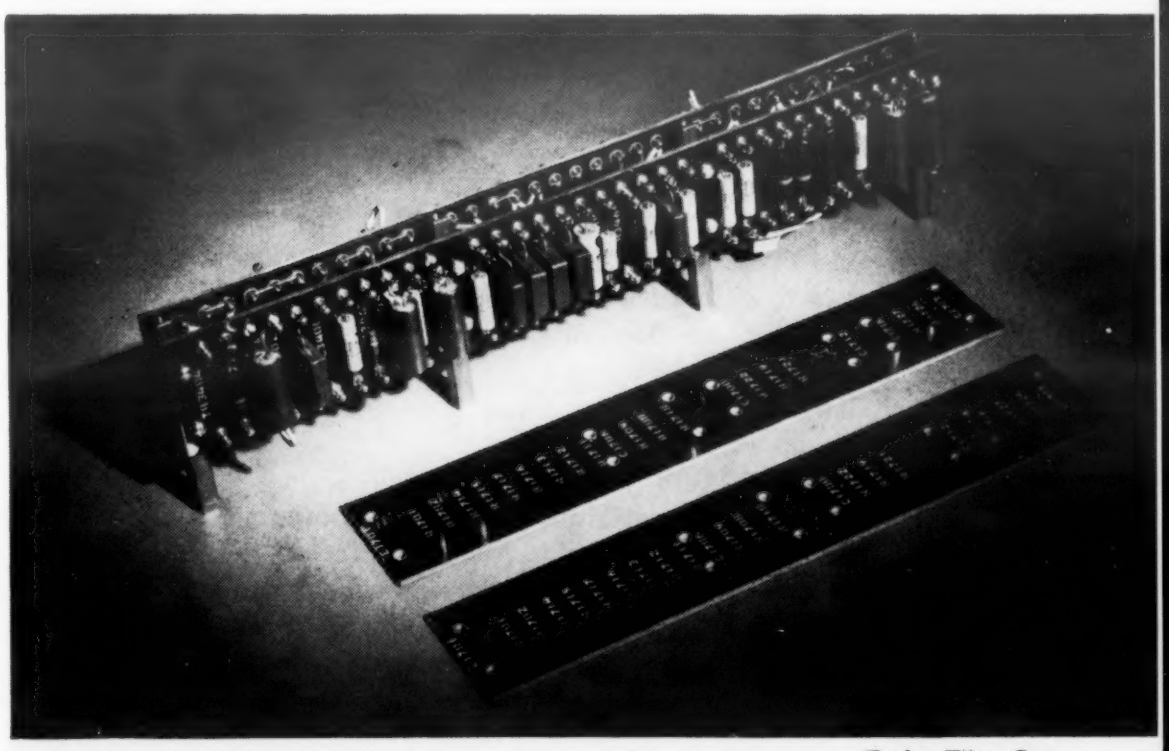
TABLE 9—PROPERTIES AND FORMS OF PLASTICS FILMS AND SHEETS
(See also page 151)

Type of Plastic	Forms	Thickness, mils	Width, in.	Tensile Strength, 1000 psi	Tear Strength, lb/in. width	Elongation, %	Max Operating Temperature, F	Brittle Temperature, F	Dielectric Strength, v/mil
Polyvinyl Chloride	Sheets, rolls, tapes	1-10	54-84	1.5-5.5	110-500	150-500	150-200	-50	1200-1500
Polyvinyl Chloride-Acetate	Sheets, rolls, tapes, tubes	1-10	84	2.0-4.5	—	150-500	150-200	—	1000-1500
Vinylidene Chloride	Rolls	0.5-10	54	1.8-15	80-465	20-140	150-200	-25 to -50	1000-1800
Cellophane	Sheets, rolls, ribbon	0.9-1.7	45-56	4.5-18	—	15-45	300	—	—
Cellulose Acetate	Sheets, rolls, tubes	0.5-10	40-60	5.5-15	—	25-45	150-220	—	700-1200
Cellulose Triacetate	Sheets, rolls	1-10	40	9-16	—	10-40	300-400	—	—
Ethyl Cellulose	Sheets, rolls, tubes	3-10	28-29	7-11	—	30-40	200-250	—	800-3000
Polytetrafluoroethylene	Sheets, tapes, tubes	0.5-13	12	1.5-3.5	—	100-300	500	-130	1000-4000
Polytrifluorochloroethylene	Sheets, rolls, tapes, tubes	2-10	20	6.0-6.5	—	90-200	300	-80	2000-5000
Polystyrene	Sheets, rolls	0.4-10	40-43	7-12	275-500	3-10	175-200	—	1000-3000
Polyamide	Rolls	1-10	18	9	—	Orients	180-380	-60	800-1500
Polyester (polyethylene terephthalate)	Sheets, rolls, tapes	0.2-7.5	54	15-30	50-1750	35-110	300	-80	1000-7000
Polyethylene	Sheets, rolls, tapes, tubes	0.5-25	108	1.0-3.5	65-575	200-800	200	-70	1000-5000
Rubber Hydrochloride	Sheets, rolls, tapes	0.4-2.5	60	3.5-5.0	—	200-800	180-200	-20	—
Vinyl-Nitrile Rubber	Sheets, rolls, tapes, tubes	1-3	11.5-41.5	2.5-4.0	—	250-500	200	-32	—
Cellulose Acetate Butyrate	Sheets, rolls	1-10	40	4-10	—	40-100	120-180	—	800-1500

is removed by leaching, and the resulting product is dried and finished by calendering. Though vulcanized fibre is not actually a plastics laminate, some of its properties (see Table 11) and many of its uses are similar. Sheets up to 52 x 84 in. are available in some grades; thicknesses vary from 0.004 to 2 in. Tubing is produced in diameters from ⅛ to 16 in., in wall thicknesses from 0.020 to ½ in. Rod sizes vary from 3/32 to 2 in. dia.

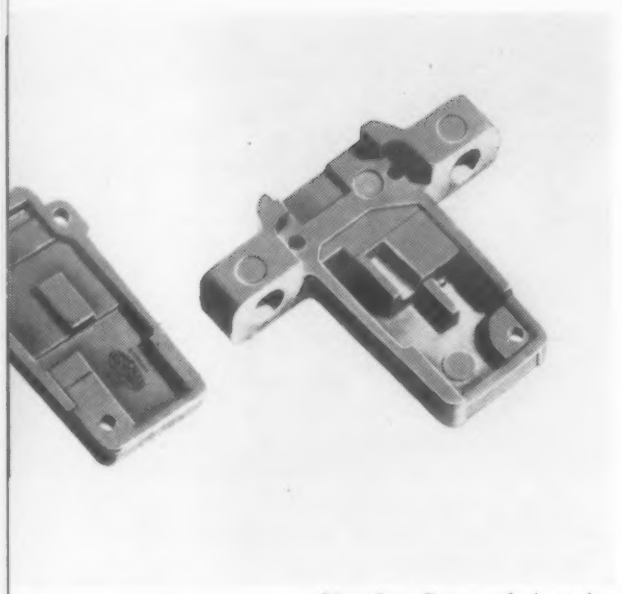
Pasted or Built-Up Mica

Because of the scarcity and high cost of sheet mica, mica is usually used in the built-up or paste form made by bonding flakes together with natural or synthetic resins or with inorganic



Taylor Fibre Co.

Glass-epoxy laminate *resistor board is used in flight control assembly for Martin's Matador missile.*



Mycalex Corp. of America

Glass-bonded mica, *selected for superior dimensional stability, forms case and cover of recording head unit for computer.*

binders. Insulation using mica paper instead of mica flakes has also been developed.

The natural micas in use are muscovite or phlogopite (amber). It is expected that synthetic fluorphlogopite, bonded with inorganic binders for resistance to high temperatures, will become important in future applications.

Shellac is still used extensively as a binder; however, a superior insulation is obtained with polyester or alkyd resin binders of the glyptal type. Epoxy resin binders are also available. Silicone resin binders are generally used where high temperature resistance combined with good electrical properties is required.

Pasted mica is generally classified as follows (see Table 12 for electrical properties):

Molding plate—This material is made of about 75 to 82% mica and 18 to 25% binder—shellac or epoxy for Class B insulation and silicone for Class H. Sheet sizes run as large as 36 in. square, in thicknesses from 0.004 to 0.063 in. The sheets are only partially cured and curing is completed when the insulation is molded. Typical molded insulations include: commutator end rings, troughs, slots, spools, coil forms and tubes.

Segment plate—This material is generally made of 85 to 90% mica flakes or mica paper and 10 to 15% binder—shellac or epoxy for Class B insulation and silicone for Class H. The low binder content combined with a full cure helps to prevent slippage of the mica flakes. Standard sheets are 18 x 36 in. (12 x 12 in. for the silicone type), in thicknesses from 0.010 to 0.063 in. Sheets as thin as 0.004 in. are also available. Chief applications for the segment plate insulation are: commutator segments, flat insulating parts, barriers, washers and disks.

Heater plate—The organic type (Class B) of heater plate insula-

TABLE 10—PROPERTIES

Type of Plastic	Mechanical Properties					
	Ten Str, 10^3 psi	Compr Str, 10^3 psi	Flex Str, 10^3 psi	Mod of Elas, 10^5 psi	Izod Impact Str, ft lb/in.	Rockwell Hardness
Ethyl Cellulose	2-8	10-35	4-12	1-3	2-8	R 50-115
Cellulose Acetate	2-9	13-36	2-16	0.9-4	0.4-5	R 35-125
Cellulose Acetate Butyrate	3-7	7-22	2-10	0.7-2	0.8-6	R 30-115
Methyl Methacrylate	7-9	12-18	13-17	4.5	0.4-0.5	M 85-105
Polystyrene	5-9	11-16	8-16	4-6	0.25-0.5	M 65-90
Modified Polystyrene	3-12	5-16	5-17	1.8-6	0.25-11	M 65-90
Styrene Copolymers	4-12	5-16	7-17	2-5	0.4-5	M 80-90
Polyethylene	1-6	—	—	0.2-0.6	—	R10
Polytrichlorofluoroethylene	6	32-80	8	2-3	3.5	R110-115
Polytetrafluoroethylene	1.5-3	1.7	—	0.6	3	—
Polyvinyl Chloride (rigid)	5-9	10-13	8-16	5-6	0.4-20	—
Polyvinyl Chloride Acetate	6-9	10-11	9-14	3.5-4	0.4-0.5	—
Vinylidene Chloride	3-5	2-3	4-6	0.5-0.8	0.3-1	M 50- 65
Polyamide	7-11	7-13	8-14	2.5-4	1.0	R110-118
Phenol-Formaldehyde						
Wood Flour Filler	6-9	23-36	8-12	8-12	0.3-0.6	M100-120
Asbestos Filler	4-9	15-35	7-15	10-25	0.3-3.5	M 95-115
Mica Filler	5-7	15-25	8-12	30-50	0.3-0.4	M100-110
Glass Fiber Filler	5-10	17-26	10-60	33	10-50	M 95-100
Fabric and Cord Filler	3-9	15-30	8-15	9-13	0.8-8	M 95-120
Urea-Formaldehyde						
Alpha Cellulose Filler	6-13	25-35	10-16	15	0.2-0.4	M115-120
Melamine-Formaldehyde						
Alpha Cellulose Filler	7-13	25-45	10-16	13	0.2-0.4	M110-125
Cotton Flock Filler	7-9	30-35	13	—	0.4-0.5	—
Asbestos Filler	5-7	30	9-11	16	0.3-0.4	M110
Macerated Fabric Filler	9-11	30-35	12-15	—	0.6-0.8	M120
Glass Fiber Filler	6-10	25-32	15-25	—	8-12	—
Alkyd						
Mineral Filler	3-4	18-25	7-10	15-25	0.30-0.35	—
Glass Fiber Filler	4-10	20-25	5-30	16-20	3-24	M70-120
Aniline-Formaldehyde	8-10	25-35	12-20	5-6	0.3	M115-120
Diallyl Phthalate						
Asbestos Filler	4.5	22.5	8	—	0.5	M99
Glass Fiber Filler	6	25	9	—	0.6	—
Synthetic Fiber Filler	4.5	30	7	—	0.8-1.0	—
Silicone						
Mineral Filler	25-45	15-25	6-8	—	0.25-0.4	M89
Glass Fiber Filler	40-50	9-15	9-15	—	3-15	M45

Electrical Properties							Physical Properties						
Dielec Str (⅛ in.) v/mil	Resistivity (50%, R.H.) ohm-cm	Dielectric Constant		Dissipation Factor		Arc Resistance, sec	Spec Gr	Ther Cond, Btu/sq ft/hr/°f/ft	Coef of Ther Exp, per °F x 10^{-5}	Max Cont Service, Temp, F	Water Abs (24 hr), %	Machinability	Moldability
		60 cps	10^6 cps	60 cps	10^6 cps								
THERMOPLASTICS													
350-500	10^{12}-10^{14}	3.0-4.2	2.8-3.9	0.005-0.020	0.010-0.060	150-200	1.1-1.2	0.10-0.17	18-36	115-185	0.8-1.8	Good	Excellent
250-365	10^{10}-10^{13}	3.5-7.5	3.2-7.0	0.01-0.06	0.01-0.10	50-310	1.24-1.34	0.10-0.19	14-29	140-220	2.0-6.5	Good	Excellent
250-400	10^{10}-10^{12}	3.5-6.4	3.2-6.2	0.01-0.04	0.01-0.04	—	1.15-1.22	0.10-0.19	20-31	140-220	0.9-2.2	Good	Excellent
450-500	10^{15}	3.5-4.5	2.7-3.2	0.04-0.06	0.02-0.03	—	1.18-1.19	0.10-0.15	16	155-190	0.3-0.4	Excellent	Excellent
500-700	10^{17}-10^{19}	2.4-2.7	2.4-2.7	0.0001-0.0003	0.0001-0.0004	60-135	1.04-1.07	0.05-0.08	11-14	150-205	0.03-0.05	Fair	Excellent
300-600	10^{12}-10^{17}	2.4-4.8	2.4-3.8	0.0003-0.02	0.0004-0.02	20-135	0.98-1.11	0.02-0.07	5-38	140-200	0.05-0.55	Good	Good
400-700	10^{14}-10^{15}	2.5-3.4	2.5-3.1	0.006-0.010	0.006-0.010	80-150	1.01-1.10	0.07-0.12	11-18	200	0.2-0.5	Good	Good
400-700	10^{13}	2.2-2.3	2.2-2.3	0.0005	0.0005	135-235	0.92-0.95	0.19	29-32	212-250	0.02	Fair	Excellent
530	10^{18}	2.3	2.5	0.015	0.010	360	2.1	0.03	8-13	390	Nil	Excellent	Excellent
480	10^{16}	2.0	2.0	0.003	0.003	200	2.1-2.2	0.15	18	500	Nil	Excellent	Excellent
700-1000	10^{17}	3.4-3.6	2.9-3.0	0.012-0.020	0.006-0.014	60-80	1.35-1.55	0.07-0.17	9-11	130-160	0.1-0.4	Excellent	Excellent
425	10^{16}	3.2-3.3	3.0-3.1	0.007-0.010	0.018-0.019	60-80	1.33-1.43	0.10	13-34	120-130	0.10	Good	Excellent
350	10^{14}-10^{16}	4.5-6.0	3.0-4.0	0.03-0.45	0.05-0.08	—	1.65-1.72	0.07	34	160-200	0.1	Good	Excellent
375-475	10^{14}	4.1-4.6	3.4-3 5	0.014-0.040	0.03-0.04	130-140	1.09-1.14	0.13-0.14	18-27	270-300	0.4-1.5	Excellent	Excellent
THERMOSETTING PLASTICS													
200-425	10^{9}-10^{13}	5.0-9.0	4.0-7.0	0.05-0.30	0.03-0.07	Tracks	1.32-1.45	0.10-0.17	5-8	300-350	0.3-1.0	Fair	Excellent
100-350	10^{10}-10^{12}	10-75	5.0-7.0	0.25-0.50	0.10-0.50	Tracks	1.52-2.00	0.19-0.39	3-4	350-400	0.1-0.5	Poor	Fair
300-460	10^{12}-10^{14}	4.7-7.5	4.2-5.2	0.01-0.07	0.005-0.040	Tracks	1.75-1.92	0.24-0.34	4-5	250-300	0.01-0.10	Poor	Fair
140-370	10^{13}	7.1	4.6-6.6	0.03	0.02	60	1.75-1.95	—	3	350-450	0.1-1.2	Poor	Good
200-400	10^{11}-10^{12}	6.5-15.0	4.5-7.0	0.08-0.45	0.03-0.09	Tracks	1.36-1.43	0.10-0.17	2-7	250	0.05-2.00	Fair	Fair
300-400	10^{12}-10^{13}	7.0-9.5	6.4-6.9	0.035-0.040	0.028-0.032	100-150	1.47-1.52	0.17-0.24	5	170	0.4-0.8	Fair	Excellent
300-400	10^{12}-10^{14}	7.9-9.5	7.2-8.2	0.030-0.080	0.027-0.045	110-180	1.47-1.52	0.17-0.24	7	210	0.1-0.6	Fair	Excellent
300-330	—	—	—	—	—	110-150	1.50-1.55	—	—	250	0.2-0.3	Good	Good
350-400	10^{11}	6.4-10.2	6.1-6.7	0.07-0.17	0.041-0.050	120-140	1.70-2.00	0.31-0.41	4-8	250-400	0.10-0.15	Fair	Good
250-350	10^{9}-10^{10}	7.6-8.6	6.5-6.9	0.07-0.11	0.036	115-125	1.5	0.24	5	250	0.3-0.6	Good	Good
250-300	10^{12}	—	—	—	—	180	1.9-2.0	0.28	3	300-400	0.3-0.6	Good	Good
400	10^{14}	5.9-7.5	4.6-5.5	0.02-0.06	0.015-0.040	175-200	1.80-2.25	—	6	300-350	0.1-0.8	Fair	Excellent
150-400	10^{12}-10^{14}	5.2-6.0	4.0-4.5	0.023-0.024	0.015-0.020	100-180	1.70-2.0	0.19-0.29	2-5	300	0.1-0.2	Fair	Excellent
600-650	10^{16}-10^{17}	3.7-3.8	3.5-3.6	0.002	0.006-0.008	—	1.22-1.25	0.63	9-11	180-190	0.01-0.08	Good	Fair
380	10^{9}	—	4.5	—	0.06	138	1.65	—	—	450	0.15	Good	Excellent
350	10^{9}	—	4.0	—	0.009	125	1.59	—	—	430	0.10	Good	Excellent
360	10^{9}	—	3.4	—	0.01	115	1.24	—	—	430	0.08	Good	Excellent
400	10^{7}-10^{9}	4.0-5.0	3.7-5.0	0.003-0.013	0.003-0.006	250-420	1.65-2.00	0.09-0.10	9-11	480	0.2-0.5	Fair	Fair
200	10^{7}-10^{13}	4.0-5.0	3.6-4.6	0.005-0.007	0.004-0.006	220-350	1.68-2.00	0.09-0.10	14	480	0.1	Fair	Fair

tion is composed of 80 to 93 mica and 3 to 20% binder. The inorganic type (Class C) is made up of 88 mica and 12% binder; this type is used up to 1000 F and, if made with phlogopite mica, will withstand 1600 F. Chief applications of heater plate are in heating appliances such as flatirons, hair driers and waffle irons; in strip and space heaters; and other parts where high heat resistance is required, such as terminal insulation, switch support insulation and washers. Standard sheets range up to 18 x 36 in., in thicknesses from 0.004 to 0.063 in.

Flexible plate—This cold-forming type of flexible mica insulation may contain up to 35% of a binder which remains permanently plastic at room temperature. It meets Class B insulation requirements with an organic binder and Class H requirements with a silicone binder. The material is available in 36 x 36 in.

TABLE 11—PROPERTIES
(See also

Type of Laminate	Mechanical Properties							
	Ten Str, 10^3 psi	Compr Str, 10^3 psi	Flex Str, 10^3 psi	Mod of Elast, 10^5 psi	Izod Impact Str, ft-lb/in. notch	Rockwell Hardness	Machinability	Insul Res (96 hr, 90% R.H.) megohms
Phenol-Formaldehyde								
Paper Base	6-25	20-40	10-25	4-30	0.4-2.2	M70-120	Good	2-35 x 10^4
Cotton Fabric Base	9-16	30-45	15-30	3-15	1-10	M70-120	Good	5-10 x 10^3
Cotton Web Base	15	30-40	18-21	—	2.0-5.5	M100-110	Good	10-200
Nylon Fabric Base	5-10	—	10-22	3.5	2-8	M100	Good	3-100[b] x 10^4
Glass Fabric Base	10-40	40-60	20-40	10-20	3-16	M105-110	Fair	25-500
Asbestos Fabric Base	5-12	18-45	10-35	3-15	2-11	M70-110	Fair	—
Asbestos Paper Base	5-15	35-40	10-35	—	0.8-2.0	M100	Fair	—
Wood Base	15-30	10-20	25-40	35	4-8	M90-105	Good	0.3-335.0
Melamine-Formaldehyde								
Paper Base	10-25	30-50	15-20	—	0.3-1.5	M110-125	Fair	—
Cotton Fabric Base	9-13	30-45	15-20	10-20	1-2	M110-120	Good	—
Asbestos Paper or Fabric	6-12	25-50	17-25	—	0.8-4.0	M110-115	Fair	—
Glass Fabric Base	25-50	30-85	28-55	30-40	5-15	M105-130	Fair	—
Glass Mat Base	16	60	20-25	15	5	—	Fair	—
Diallyl Phthalate								
Glass Fabric Base	20-30	45	40-50	—	4-7	M120	Fair	—
Cotton Fabric Base	8-11	40	12-17	—	0.8-1.2	—	Good	—
Polyester								
Glass Fabric Base	40-50	30-60	50-60	10-30	20-35	M100-110	Fair	—
Glass Mat Base	15-25	30-50	20-35	10-20	10-25	M90-110	Good	5-50 x 10^3
Paper Base	6-15	20-25	12-25	8-12	—	—	Excellent	—
Silicone								
Glass Fabric Base	10-25	35-45	10-45	35-45	5-22	M100	Fair	1-3 x 10^5
Asbestos Fabric	—	40-50	12-16	40-50	6-9	—	Good	—
Polytetrafluoroethylene								
Glass Fabric Base	8-15	20	10-13	—	5-6	M60	Good	5-5000 x 10^3
Ceramic Fiber Base	1.5- 4	—	—	—	1.0-2.5	—	Fair to Good	1 x 10^7
Epoxy-Glass	30-50	50-90	45-80	25-35	6-16	M105-120	Good	1-6 x 10^5
Vulcanized Fibre	6-12	20-30	12-20	8-12	1-8	R50-100	Good	—
Lignin	5- 8	25-30	9-15	—	0.5-1.5	M90	Good	—

[a] Short time test
[b] ¼-in. thickness

sheets in thicknesses from 0.003 to 0.031 in., and is commonly used for armature slot liners, field coils and generator and transformer insulation.

Tubing—This form of mica insulation is made with alkyd, polyester or epoxy binders for Class B insulation, silicone binder for Class H, and inorganic binders for Class C. Tubes are available in round, square and rectangular shapes and are used for coil forms, transformer cores, stud insulators, grid rheostats and bushings. Sizes range from 3/16 to 4 in. i.d., 12 to 36 in. length and 1/64 to ¼ in. wall thickness.

TABLE 12—PROPERTIES OF PASTED MICA
(See also page 154)

Type	Dielectric Strength, v/mil	
	Short Time	Step-by-Step
Molding Plate	400–1300	250–1100
Segment Plate	600–1300	400–1100
Heater Plate	600–1200	400–1000
Flexible Plate	350–1000	200–800
Tubes	300–500	200–400

Ceramics

As indicated in Table 13, the number of ceramic materials available for electrical insulation is large. In general, these materials can be categorized as follows:

Porcelain—Conventional porcelain insulators are made from clay, quartz and feldspar. Parts are usually made by dry pressing, wet processing, casting or extruding, and fired above 2000 F. Dimensional tolerances are poor and machining after firing is difficult. Special porcelains containing high percentages of mullite, zircon, wollastonite, etc., are available.

Steatite—Steatite insulators are made from talc (hydrous magne-

OF PLASTICS LAMINATES
page 152)

Electrical Properties							Physical Properties				
Vol Res, ohm-cm	Dielec Str (step-by-step, ⅛ in.), v/mil	Dielectric Constant		Dissipation Factor		Arc Resistance, sec	Spec Gr	Ther Cond, Btu/sq ft/hr/°F/ft	Coef of Ther Exp, per °F x 10^{-5}	Max Cont Svc Temp, F	Water Abs (24 hr), %
		60 cps	10^6 cps	60 cps	10^6 cps						
10^{10}-10^{13}	250-800	4.5-7.5	3.6-6.0	0.02-0.10	0.02-0.08	Tracks	1.30-1.40	0.04	3-5	225-250	0.3-9.0
10^{10}-10^{12}	150-450	5.0-10.0	5.0-5.7	0.04-0.20	0.05-0.10	Tracks	1.30-1.36	0.05-0.06	3-6	225-250	1.0-2.0
—	150	—	7.0	—	0.10	Tracks	1.30-1.37	—	2-3	225	1.5
10^{14}	300-425	3.7-4.2	3.5-3.9	0.01-0.02	0.015-0.040	5-40	1.15-1.20	—	7	165	0.20-0.35
—	250-700	—	3.7-6.0	0.01-0.02	0.01-0.03	Tracks	1.4-1.8	0.03-0.04	3-5	290	0.3-2.5
—	50-125	—	5.5-7.0	—	0.10-0.15	Tracks	1.6-1.8	0.11	3-5	275	0.3-2.5
—	120	—	5.2	—	0.12	Tracks	1.65-1.85	—	2-3	275	0.4-2.0
—	—	—	5	0.20	0.05	Tracks	1.3	—	—	150-200	2.5-11.0
—	200-450	—	6.4-8.5	—	0.035-0.050	—	1.40-1.55	—	—	200-250	1.0-2.0
—	100-250	7.0-8.3	6.2-10.0	0.040	0.03-0.10	120-145	1.35-1.50	—	1-3	200-250	1.0-2.0
—	50-125	—	8.0-9.5	—	0.10-0.22	—	1.75-1.85	—	—	225-275	1.0-5.0
—	150-350	—	6.9-9.0	—	0.010-0.025	175-190	1.8-2.0	—	1-2	300	1.0-2.5
—	300	—	6.5	—	0.040-0.080	180	1.80	—	—	300	1.5-3.0
—	500	4.3	4.1	0.013	0.015	150	1.65	—	—	300	0.12
—	300	5.1	4.8	0.015	0.018	130	1.38	—	—	—	0.60
—	—	—	—	—	—	80-120	1.5-2.1	—	—	300-400	0.3-0.9
10^{12}	200-450	4.0-4.7	4.0-4.7	0.005-0.025	0.007-0.020	80-120	1.5-1.8	—	—	300	0.3-1.0
10^{13}	400-600	3.0-4.2	3.0-4.2	0.10	0.03	25-75	1.2-1.5	—	6	220-250	1.5
—	150-250	3.7-3.4	3.7-4.3	0.0006-0.0050	0.0012-0.0050	150-250	1.6-1.9	0.02	1-2	400-500	0.2-0.7
—	50-100	—	—	—	—	—	1.75	—	—	500	1.0-1.5
10^{12}	250-300	2.7	2.7	0.0005	0.0006	160	2.2	0.02-0.05	—	480	0.02
10^{13}	—	2.5-2.7	2.4-2.5	0.002-0.003	0.001-0.003	190	1.9-2.2	—	7	500	0.5-2.0
—	300-600	4.2-6.5	4.5-5.3	0.003-0.015	0.015-0.025	15-130	1.7-1.9	—	—	300-360	0.05-0.25
—	150-250[a]	4.7	—	—	0.03-0.08	140	1.0-1.5	0.07-0.12	4	225	18-65
10^{12}	105[b]	6	—	0.11	—	135	1.35-1.45	—	—	150	2.5

sium silicate). They are shaped by the same methods used for porcelain. As with porcelains, tolerances are somewhat poor and machining of fired parts is difficult. A type of magnesium silicate known as forsterite is used for applications where parts must be sealed to metals, or where extremely low dielectric losses are required.

Pure oxides—These very refractory materials are more difficult to shape and fire than the other ceramic materials and possess comparatively high porosity. The oxides most commonly used (alone or in combination) are alumina, beryllia, zirconia, magnesia and thoria. Also, compressed (not sintered) magnesium oxide is sometimes used as an insulator in items such as tubular resistance heating elements.

Fluxed oxide bodies—The best known insulators in this category are the high alumina bodies which contain up to 98% alumina. The materials are abrasive, but possess excellent mechanical and electrical properties. Among many other applications, they have proved extremely valuable for aviation ignition systems.

Cordierite—Cordierite is a magnesium-aluminum-silicate and is characterized by excellent thermal endurance. The material is available in either porous, low porosity or vitrified form.

Lithia ceramics—Insulating materials in the lithia-alumina-silica system are especially noted for their low coefficient of thermal expansion. Coefficients vary from low positive to low negative values over a wide temperature range. For this reason, the materials are capable of withstanding repeated quenchings from 2000 F into water at room temperature.

Titania, and titanate ceramics—These materials are used principally where a high dielectric constant (up to 10,000 for some types) is required. They also possess a low dissipation factor.

Phosphate-bonded talc or mica—Talc or synthetic fluor-phogopite have been mixed with phosphoric acid to produce promising new ceramic insulations. The materials are formed by pressing and heating, and they are machinable. They are also capable of withstanding high temperatures. Electrical properties have not yet been fully evaluated but they appear to be good.

Glasses—Electrical glasses are available in a wide range of properties and materials—from low temperature glasses to vitreous silica. Glass shapes are largely produced by manipulating the glass while it is still viscous, although powdered glass may be compressed to shape and then sintered.

Ceramoplastics and Cold Molded Materials

Ceramoplastics, represented almost entirely by glass bonded micas, are unusual in that they are entirely inorganic yet they are molded in the same way (except for the higher temperatures) as organic plastics. Ceramoplastics can replace organic plastics insulations in those applications where the electrical, mechanical or thermal requirements are too severe for the organics or where dimensional stability or resistance to nuclear radiation is required.

The materials can be molded into complex shapes with extreme precision. Distortion and warpage are eliminated since, unlike conventional ceramics, ceramoplastics require no heat treatment after forming. Also, there is no cold flow after molding.

Ceramoplastics utilize special low temperature glasses as a binder. These glasses permit operation of the insulators at temperatures of 660 to 900 F, depending upon the type of glass and the percentage of mica in the filler. Filler materials consist of natural or synthetic mica in powdered form; titanates, quartz, glass fibers, alumina, etc. are added when special properties are required.

Since molding temperatures are comparatively low (about 1000 to 1500 F) it is possible to mold metal inserts directly into the insulators. This cannot be done with

TABLE 13—PROPERTIES (See also

Property \ Type	Steatite	Fluxed Alumina	Corderite	Titanate	Glasses		Forsterite
					Hard	Soft	
MECHANICAL PROPERTIES							
Tensile Strength, 1000 psi	6-10	20-25	2.5-4.0	4-10	6-10	5-9	8-10
Compressive Strength, 1000 psi	65-90	80-250	20-45	40-120	60-175	50-175	60-100
Flexural Strength, 1000 psi	16-24	20-45	8-12	10-42	11-16	10-15	18-20
Modulus of Elasticity, 10^5 psi	130-150	150-50	20-50	100-150	70-130	76-98	130-150
Charpy Impact Strength (½-in. rod), ft-lb	0.3-0.4	0.4	0.2-0.3	0.3-0.5	0.1-0.3	0.1-0.3	0.3-0.4
Knoop Hardness	1400	2000	1500	1800	250-900	250-900	1400
Water Absorption, %	0-1	Nil	0-15	Nil	Nil	Nil	Nil
Machinability	Poor	Poor	Poor	Poor	Poor	Poor	Poor
PHYSICAL AND THERMAL PROPERTIES							
Specific Gravity	2.5-2.7	3.2-3.6	2.1-2.4	4.0-8.9	2.2-2.7	2.4-4.3	2.7-2.9
Density, lb/cu in.	0.090-0.098	0.115-0.130	0.076-0.087	0.144-0.320	0.079-0.097	0.087-0.155	0.097-0.105
Ther Cond, Btu/sq ft/hr/°F/ft	0.85-1.45	1.69-12.10	0.73-0.97	1.94-2.90	0.36-0.73	0.36-0.73	1.21-2.42
Specific Heat, Btu/lb/°F	0.19-0.21	—	—	—	0.16-0.21	0.16-0.21	—
Coef of Ther Exp, per °F x 10^{-5}	1.55-1.89	0.99-1.44	0.36-0.54	1.26-1.80	0.14-0.90	1.17-2.16	1.98
Max Continuous Service Temp, F	1800-2000	2000-2700	2300	1800	800-1800	700-900	1800-2000
Thermal Shock Resistance	Moderate	Good	Good	Poor	Good to excellent	Poor to moderate	Poor
ELECTRICAL PROPERTIES							
Dielectric Strength (step-by-step, ¼ in.), v/mil	200-350	250-400	40-125	50-300	300-400	200-300	200-300
Volume Resistivity, ohm-cm	10^{13}-10^{15}	10^{14}-10^{15}	10^{12}-10^{14}	10^{8}-10^{15}	10^{15}-10^{17}	10^{12}-10^{17}	10^{13}-10^{15}
Dielectric Constant							
60 cps	5.9-6.5	8.4-8.5	—	14-9000	3.8-14.6	6.4-9.2	6.3
10^6 cps	5.2-6.3	8.3-8.4	4.5-5.4	14-8000	3.7-14.5	6.6-9.1	6.2
Dissipation Factor							
60 cps	0.0013-0.0150	0.0013-0.0015	—	0.0006-0.0360	0.0006-0.0008	0.0012-0.0800	0.0014
10^6 cps	0.0008-0.0035	0.0007-0.0010	0.004-0.012	0.0002-0.0105	0.0006-0.0050	0.0005-0.0100	0.0003
Arc Resistance, sec	500+	500+	High	High	High	Medium to high	High

[a] Thickness of 9 mils.

conventional ceramics because of their high firing temperatures.

Compression molded ceramoplastics with a high mica content can be machined. Nearly all machining operations except punching can be performed within a tolerance of 0.001 in. or better. Slabs and rods can be purchased as stock items.

Cold molded materials have a base or filler that is usually asbestos, asbestos-silica or clay-asbestos. Bituminous or phenolic binders are used chiefly for organic insulations; these are cured at about 450 F. Binders for inorganic or refractory cold molded insulations may consist of portland cement, calcium hydrate or phosphoric acid.

Cold molded insulations are chiefly used for such applications as connector plugs, switch bases, sockets, outlet covers and fuse housings. Because of their high water absorption, the materials must often be impregnated.

Engineering properties of ceramoplastics and cold molded insulation materials are listed in Table 14.

Other Materials

Despite the inroads made by the newer organic and inorganic materials, a number of the older materials are still being used as electrical insulators.

Wood—Paraffinned or unwaxed maple wood wedges for motor slots are available in about 20 shapes and in more than 400 sizes. In addition to low initial cost, wood wedges are said to offer reduced assembly time and fewer breakdowns due to loose windings. Wood panels, usually of plywood, are also used to some extent for mounting instruments.

Paraffin-impregnated wood has a volume resistivity of 10^{10} to 10^{13} ohm-cm. Dielectric constant for untreated woods ranges from 1.4 to 2.9 and higher at 60 cps; dissipation factor ranges from 0.004 to 0.058.

Slate — Electrical slate, once widely used for panels and bases, has been largely supplanted by plastics, ceramics and ceramoplastics. The dielectric constant for this material varies from 12.4 to 19.0 at 1 mc and it may exceed 60 at 60 cps. The dissipation fac-

OF CERAMICS
page 156)

Porcelain										
High Voltage	Low Voltage	Zircon	Lithia Porcelain	Alumina (sintered)	Beryllia (sintered)	Zirconia (sintered)	Muscovite Mica	Vitreous Silica (transparent)	Synthetic Mica	Wollastonite
10-15	6	3-8	1.5-3.5	15	10	12	5-10	—	—	—
25-100	25-50	80-150	60	225	100	200	30	150	—	80
9-15	3.5-6.0	20-35	8	48	20	27	—	10	—	20
70-140	70-100	200-300	120	470	430	260	200-300	97-104	—	—
0.2-0.3	0.2-0.3	0.4-0.5	0.25	—	—	—	—	—	—	—
1100	1100	1800	1400	2000	2000	1100	90	600	50-300	1400
0-0.05	0.5-2.0	Nil	0.1	10	0-1	8	Low	Nil	Low	0.03
Poor	Poor	Poor	Poor	Poor	Poor	Poor	Fair	Poor	Fair	Poor
2.3-2.5	2.2-2.4	3.1-3.7	2.3	3.6	2.9	5.4	2.6-3.2	2.2	2.5-3.5	2.8
0.083-0.090	0.079-0.086	0.112-0.133	0.084	0.131	0.105	0.194	0.094-0.115	0.079	0.126	0.098
0.48-1.21	0.97-1.21	1.33-3.63	1.33	13.07	101 64	—	0.36	0.18	—	—
0.25	0.25	—	—	0.20	0.24	0.12	0.20	0.18	—	—
0.90-1.26	0.90-1.26	0.63-0.99	0.153	0.90-1.44	1.08	0.99	1.8	0.097	1.44-2.70	1.10
1800	1600	1800-2200	1800	3000	3500	3500	1000	2000	1300-1500	1500
Moderate	Moderate	Good	Excellent	Good	Excellent	Moderate	—	Excellent	—	Moderate
250-400	40-100	250-350	200-300	250	—	—	1000-2000[a]	250	—	265
10^{12}-10^{14}	10^{12}-10^{14}	10^{13}-10^{15}	—	10^{16}	10^{16}	—	10^{13}-10^{17}	10^{19}	10^{10}-10^{15}	—
6.5	5.5	9.1	—	—	—	—	5.4-8.7	3.8	—	—
5.4-7.0	5.0-7.0	7.1-9.0	5.6	9.6	5.8	—	5.4-8.7	3.8	5.9-7.8	6.2
0.0008-0.0009	0.015	0.036	—	—	—	—	0.0025	0.0007	—	—
0.0006-0.0100	0.010-0.020	0.0008-0.0014	0.005	0.0006	—	—	0.0001-0.0004	0.0001	0.0003-0.0010	0.0005
500+	500+	High	High	500+	500+	500+	High	500+	High	High

Corning Glass Works

Glass *is used as an insulator in a variety of electrical parts because of its excellent dielectric properties.*

tor is high—0.45 to 0.63 at 1 mc—and volume resistivity is about 10^8 ohm-cm.

Marble—This material is used to a minor extent for electrical insulation. Its volume resistivity is 10^9 to 10^{11} ohm-cm.

Amber—Amber is occasionally used for insulation. Significant electrical properties are: a dielectric constant of 2.70 at 60 cps and 2.65 at 10^6 cps; a dissipation factor of 0.001 at 60 cps and 0.006 at 10^6 cps; and a resistivity of 10^{16} ohm-cm.

Synthetic sapphire — Synthetic sapphires are single crystals available in the form of rods, balls, tubing and special shapes. The materials are used in equipment such as klystrons, magnetrons and traveling wave guides.

At 300 mc, parallel to the c-axis, the dielectric constant is 10.6 and the dissipation factor is less than 0.0001. Perpendicular to the c-axis the dielectric constant is 8.6 and the dissipation factor is also less than 0.0001.

At 100,000 mc, with the field perpendicular to the c-axis, the dielectric constant is 11.0 and the dissipation factor is 0.0002. Dielectric strength is high, and volume resistivity is 10^{11} ohm-cm at 930 F.

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M. W. Kellogg Co.
Mica Insulator Co.
Mycalex Corp. of America

TABLE 14—PROPERTIES OF CERAMOPLASTICS AND COLD MOLDED MATERIALS
(See also page 159)

Property \ Material	Ceramoplastics (glass bonded micas)				Cold Molded Materials	
	Compression Types		Transfer Types		Organic	Refractory
	Insulation	Capacitor	Insulation	Capacitor		
PHYSICAL AND MECHANICAL PROPERTIES						
Specific Gravity	3.0	3.25	2.6-3.8	3.5-3.8	1.9-2.2	1.6-2.2
Density, lb/cu in.	0.11	0.115	0.075-0.136	0.125-0.136	0.068-0.077	0.058-0.073
Tensile Strength, 1000 psi	6-7	6	5-6	5	1.4-3.0	1.5-2.0
Compressive Strength, 1000 psi	35-42	35-42	20-25	20-25	6-15	12-18
Flexural Strength, 1000 psi	15-18	12-15	10-15	10-15	3.7-10.0	2.0-7.5
Modulus of Elasticity, 10^5 psi	90-120	90-120	70-80	70-80	—	—
Izod Impact Strength, ft-lb/in. notch	1.8	—	0.7	—	0.15	0.15
Rockwell Hardness	M110-120	—	M115-130	—	M75-95	M80-90
Water Absorption, %	Nil	Nil	Nil	Nil	1.0-5.5	3-15
Machinability	Fair to good	Fair to good	Poor	Poor	Poor	Good
Moldability	Fair	Fair	Good	Good	Poor	Good
THERMAL PROPERTIES						
Ther Cond, Btu/sq ft/hr/°F/ft	0.29	—	0.23-0.31	—	—	—
Specific Heat, Btu/lb/°F	0.16	—	0.13-0.24	—	—	—
Coef of Ther Exp, per °F x 10^{-5}	1.8	1.8	1.8-2.0	1.8-2.0	—	—
Max Continuous Service Temp, F	600-1000	600-700	500-800	500-600	500	900-1300
Heat Distortion Temp (264 psi), F	850	800	700	650	400+	400+
Thermal Shock Resistance	Moderate	Moderate	Moderate	Moderate	Moderate	Moderate
ELECTRICAL PROPERTIES						
Dielectric Strength (step-by-step, ¼ in.), v/mil	400-600	270-400	400-500	300-400	50-150	50-80
Volume Resistivity, ohm-cm	10^{14}-10^{15}	10^{14}	10^{14}-10^{17}	10^{14}	10^{12}	10^8-10^{10}
Dielectric Constant, 60 cps	7.5-7.6	—	7.0-9.5	—	17-28	—
Dielectric Constant 10^6 cps	7.4-7.9	10-25	6.9-9.2	10-40	6	—
Dissipation Factor, 60 cps	0.0035-0.0070	—	0.007-0.050	—	0.13-0.30	0.07
Dissipation Factor, 10^6 cps	0.0015-0.0020	0.0020-0.0040	0.0015-0.0120	0.0025-0.0035	—	—
Arc Resistance, sec	300	300	250	250	75-200	100-600

FILE FACTS

Metal and Alloy Powders—A DIRECTORY*

Metal Powders

Production Method (or particle shape)	Mesh Size (approx)	Purity, %	Supplier
ALUMINUM			
(Roughly Spherical)	−5 and finer	99+ and 99.6+	A1
(Granulated roughly spherical)	0.25 in. dia.	99.0+ and 99.75+	A1
Atomization	5 microns avg to 25 microns avg	99.5+	A1
Mechanical stirring	−8 to +140	Grade I—95 to 97.5; II—92 to 95; III—90 to 92; IV—85 to 90	Ap
(Granular particles)	−8, −12+120, −120+200, −325	99	Be
——	——	99.3 to 99.99	M
——	−20, −30, −40, −100, −200	98 to 99	MD
Atomization	−24, −40, −100, −200	99.3	Mu
Atomization	−40, −100	——	R
Mechanical comminution	Various sizes	99	Rea
ANTIMONY			
——	——	99.5 to 99.9[a]	M
——	−100, −200, −325	99	MD
ARSENIC			
Resublimed under nitrogen	——	——	M
BERYLLIUM			
Mechanical Comminution	−200	98.5 min	BB
——	Various sizes	——	M
BISMUTH			
——	−100	99+	Be
——	−100, −200, −325	99	MD
CADMIUM			
——	−100	99+	Be
——	−150, −300	49.50 min	Ha
——	Various sizes	——	M
——	−100, −200, −325	99	MD
CHROMIUM			
——	−100	98	Be
——	−50	97 min	FM
Electrolytic	−100, −150, −250	Various grades: 99 to 99.75	Ha
Atomization	−28, −60, −100	99 min	Ha
——	Various sizes	——	M
Exothermic	−20 to −200	98.5 min	Mu
——	−50	98	SC
Electrolytic	−20, −100, −200, −325	99.8 min	UC
——	Various sizes	97.25 min	UC
COBALT			
——	−300	98 to 99	Be
——	1 to 3 microns	99.7 min	Ha
——	Various sizes	——	M
Hydrogen reduction	−100, −200, −300 or finer	97.5 min	Mu
COLUMBIUM			
——	20 to 80; −400	99.5 min	K
——	Various sizes	——	M
Hydride method	−325	99.3	MH
——	1 to 5 microns	99+	Mu
——	−80, −230, −325	99.7	SC
COPPER			
Electrolytic	Various sizes	99 to 99.5	AM
——	−150	99+	Be
Gaseous production	−40, −100, −200, −325	99.0 min	Gl
Atomization	Various sizes, 40% −325 to 95% −325	99.25 min	Gr

Metal Powders—continued

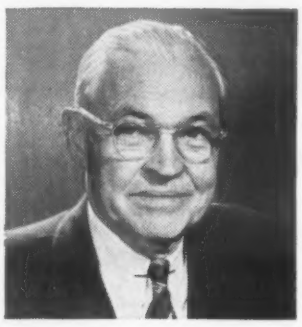
Production Method (or particle shape)	Mesh Size (approx)	Purity, %	Supplier
COPPER (cont.)			
——	Various sizes	——	M
——	−40, −150, −200	97.5 to 99	MD
(Dendritic)	−100	99.40 to 99.80	MM
Atomization	——	99.60	MM
(Spherical)	−100, −100+200	99+	NJ
Atomization (irregular or spherical)	Various sizes	99 min	PML
GOLD			
——	To specs	To specs	ES
——	——	——	M
IRON			
Carbonyl reduction	10 to 20 microns avg	99.5 to 99.9	An
Hydrogen reduction (sponge)	−30, −80	98.5 min (tentative)	AWS
——	−100+325	96 to 98	B
——	−100+325	96 to 98	Be
Sponge method	From −40 mesh up	97.5+	E
——	−30	94 min	EM
——	−80	98.5 min	EM
Electrolytic	−100, −200	99.0 min.	EM
Reduction (sponge method)	−40, −80, −100, −250, −325, 16 microns	98+	H
Magnetite	−40, −60, −100, −200	97.5+	H
Hydrogen reduction	−80, −200, −325	98.5 min.	Ha
Pulverization	−200, −100+325	93	Ha
Electrolytic (dense, oblong particles)	−65	99.3	HVA, J
Electrolytic (spongy particles)	−100	99.3	HVA, J
——	Various sizes	——	M
Carbonyl annealed	−325 (10 to 20 microns)	——	Ma
Reduction	−80, −100, −325	98+	Ma
Magnetite	−40	97.6 to 97.9	Ma
(Spherical)	−100	95.0 min	MP
(Spherical)	−100	95.5 min	MP
Reduced oxide	−100	98.50	Pl
Reduced oxide	−100	98.35	Pl
Electrolytic	−100	99.0 min	Pl
Hydrogen reduction	−100	96.6 min	Py
Electrolytic	−100	——	Py
Hydrogen reduction	−325	——	Py
Sponge method	−100	——	Fe
LEAD			
——	−100	99+	Be
Atomization	−40, −100, −200, −325	99.5 min	Gl
——	Various sizes	——	M
——	−100	99.5	MD
Atomization	——	99 min	PML
Atomization	−200	99.90+	NL
MAGNESIUM			
——	−100	93 to 95	Ha
Mechanical comminution	Various sizes	96 to 98	Rea
Mechanical comminution	Various sizes	——	U
MANGANESE			
——	−100	99.00	Ha
——	Various sizes	——	M
——	−100, −200, −325	99	MD
Alumino-thermic	−8, −100, −325	96 min	Mu
Electrolytic	−100	99.00 min	Pl
——	Various sizes	95.5 min	UC
Electrolytic	Various sizes	99.9 min	UC

For more information, Circle No. 598

(continued on p 165)

RB&W FASTENER BRIEFS

RUSSELL, BURDSALL & WARD BOLT AND NUT COMPANY



Technical-ities

By John S. Davey

Factor of Safety— make it a reality

You can't calculate that with a bolt having yield strength of 4 times the working load you're automatically getting a *safety factor* of 4. Far from it. Only when the bolt is *tightened* to four times working load do you get it.

That's because rigidly fastened members can be externally loaded to the full value of residual tension in bolts without any separation or extra bolt stress.

Suppose you need a bolt for a 5000 lb. working load. For a X4 safety factor, you use a bolt of 20,000 lb. capacity, and tighten it to 20,000 lb. tension. If you tighten to only 10,000 lbs., any external load larger than this causes loosening, and progressive bolt failure from fatigue. So your safety factor is really only 2.

PRODUCTION MAN FOLLOW-THROUGH IMPORTANT

Factor of safety, then, is not established on the drawing board. It can only be put into the product by the shop man with wrench. In short, a bolt is no better than the supervision of its tightening.

A NOTE ON FLEXIBLE JOINTS

This case is different. You tighten such a joint just to working load. So use a bolt capable of this *plus* any added stress *multiplied* by your safety factor.

How to simplify bolt and nut usage

DESPITE their now unified dimensions, "standard" fasteners number thousands upon thousands of different types and sizes. More and more companies are beginning to realize that *usage* simplification offers advantages.

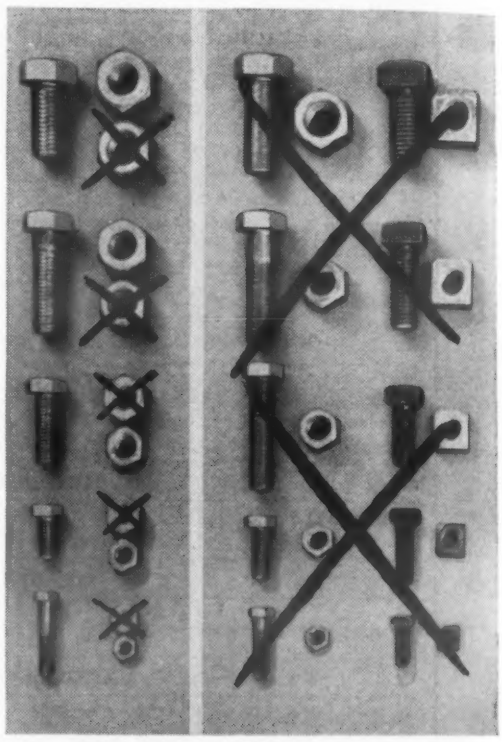
EXAMPLES

A well known electrical manufacturing company finds it no handicap to eliminate all 1/16" bolt sizes above 3/8", thereby simplifying production and purchasing.

One engineering firm eliminated 1700 different fastener items from inventory by determining that the jobs could be done as well by other sizes or types.

SOME SUGGESTIONS

To guide your thinking, RB&W points up the following ways to simplify: (1) Forget thread fits for all but specialized needs – standard "tolerance fits" have thoroughly proved themselves. (2) Why adhere to double thread standard when coarse threads prove stronger and assemble faster? (3) Stick with hex head bolts – they do better jobs than square. (4) It can save money to change diameter or length, rather than to add another item to stock. (5) Two standard physical grades meet most load range requirements – do you really need special alloys? (6) Heavy nuts really belong with larger size bolts – use finished nuts with the smaller sizes.



Here is a graphic display of possible simplification. From a typical array of fasteners, it shows what may be superfluous for meeting the requirements of proper fastening in a great many instances.

RB&W would be happy to enlarge on these facts, and help you simplify fastener selection to get proper joint strength and cut assembly time and inventory. Write Russell, Burdsall & Ward Bolt and Nut Company, Port Chester, N.Y.

Plants at: Port Chester, N. Y.; Coraopolis, Pa.; Rock Falls, Ill.; Los Angeles, Calif. Additional sales offices at: Ardmore (Phila.), Pa.; Pittsburgh; Detroit; Chicago; Dallas; San Francisco.

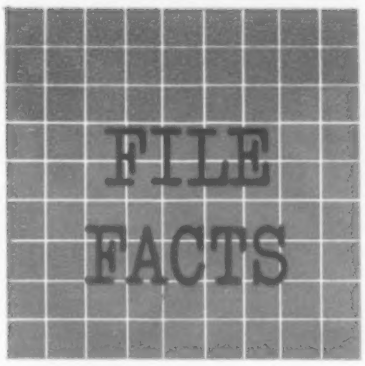
High strength bolts save costly crane

At one company's plant, a large, heavy-duty crane had deteriorated due to rivets loosening. Replacing with new rivets was no permanent answer, but RB&W high tensile bolts were.

Used with hardened washers, these RB&W bolts clamp members together so tightly, no slipping into bearing takes place, holes are reinforced against fatigue, and connections become vibration-proof.

Assembling heavy duty equipment with RB&W high strength bolts in the first place can avoid such problems and create more satisfaction with the product.

For more information, turn to Reader Service Card, Circle No. 374



Metal Powders—continued

Production Method (or particle shape)	Mesh Size (approx)	Purity, %	Supplier
MOLYBDENUM			
Hydrogen reduction	−200 (95% −325)	99.9	AEM
—	−100	99	Be
Hydrogen reduction	−80, −200	99.9	C
Hydrogen reduction	−30, −200	99.9	Fa
Hydrogen reduction	−200	99.75 min	Ha
—	−80	99.0 min	Ha
—	Various sizes	—	M
Hydrogen reduction	−80, −200	99.80 min	Mu
Hydrogen reduction	Up to 325	99.8+	NAP
Hydrogen reduction	−325 (1 to 5 microns)	99.80 min	S
—	−325 (1 to 5 microns)	99.50 min	S
—	−230	99.4	SC
—	−100	82 to 88	UC
NICKEL			
(Spherical)	−80, −150	99+	Be
(Irregular)	−200	99+	Be
—	−50	99.65	FM
(Spherical)	−100, −200, −325	99 min	Ha
—	Various sizes	—	M
—	−100, −150, −200, −325	99.25	MD
Electrolytic	−100	98.80 min	Pl
Hydrogen precipitation, (botryoidal particle shape)	Various sizes	99.5 min	SG
Hydrogen precipitation, (low density particles)	50 to 100% −325	99.5 min	SG
PALLADIUM			
—	To specs	To specs	ES
PLATINUM			
—	To specs	To specs	ES
—	−200	—	Ha
—	Various sizes	—	M
RARE METALS			
—	—	—	M
RHENIUM			
Hydrogen reduction (of $KReO_4$)	Various sizes	98.5	UT
Hydrogen reduction (of NH_4ReO_4)	Various sizes	Spectroscopically pure	UT
RHODIUM			
—	Various sizes	—	M
RUTHENIUM			
—	Various sizes	—	M
SELENIUM			
—	Various sizes	99.5 min	AM
—	−200	99+	Be
—	Various sizes	—	M
SILICON			
—	−100	97 min	Ha
—	Various sizes	—	M
—	Various sizes	96.5 to 98	UC
—	−30+80, −150+325, −325	99.7 to 99.9	UC
SILVER			
Electrolytic	Various sizes	—	AM
—	To specs	To specs	ES
—	−150, −250	999 fine	Ha
Galvanic precipitation	−60, −150, various sizes	999.0 fine	HH

Metal Powders—continued

Production Method (or particle shape)	Mesh Size (approx)	Purity, %	Supplier
SILVER (cont.)			
Chemical reduction	1 to 10 microns	99.76	HH
Atomization	−80	999.00 fine	HH
—	—	99.5 and 99.999	M
—	−100	99	MD
Atomization	—	99.9 min	PML
TANTALUM			
Electrolytic reduction	−80	—	Fa
—	−20	98.5 min	K
—	20 to 80	99.6	K
—	−325	99.5 min	K
—	−80, −200, −400	99.80	Ha
—	Various sizes	—	M
Hydride method	−200, −325	99.5	MH
—	−50, −325	99.5	SC
TELLURIUM			
—	—	—	M
THORIUM			
—	200 to 300 and finer	98.5 min	AEM
TIN			
Atomization	Various sizes	99.5+	AM
Atomization	−100	—	Be
Atomization	−40, −100, −200, −325	99.5 min	Gl
Atomization	Various sizes from 40% −325 to 95% −325	99.90 min	Gr
—	−100, −200	99.5 min	Ha
—	Various sizes	—	M
—	−50, −100, −200, −325	99.5	MD
Atomization	−100	99.85	NL
TITANIUM			
—	−100, −200, −325	99 min	Ha
—	Various sizes	—	M
—	−100, −200, −325	99.5	MD
Hydride method	−325	99+	Mu
—	−80	99.2	T
(Sponge-like shape)	−60 to −325	99+	UI
TUNGSTEN			
—	90% under 3 microns, peak at 2 microns	99.9+	AEM
—	−65	98.9 min	Be
Hydrogen reduction	−325 (various particle sizes available)	99.9	C
Hydrogen reduction	−200	99.9	Fa
—	−80	99 min	Ha
Hydrogen reduction	−325 or 1 to 5 microns	99.90 min	Ha
—	Various sizes	—	M
Hydrogen reduction	2 microns	99.6 min	Mu
—	−80	99 min	Mu
Hydrogen reduction	Up to 400	99.8+	NAP
Hydrogen reduction	−325 (5 size distributions in 1 to 5 micron range)	99.95	S
—	−65	99 min	UC
URANIUM (Presently available only with AEC approval)			
(Equiaxed regular shape)	Various sizes: −12 to −325	99.3 typical	SCN
VANADIUM			
—	—	—	M

(continued on p 167)

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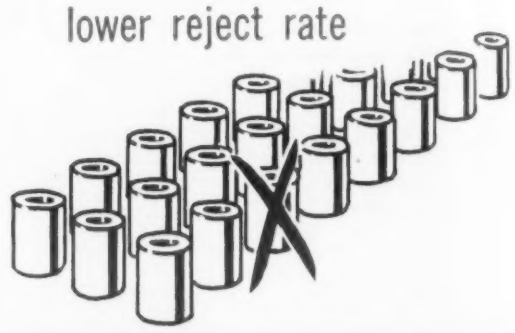

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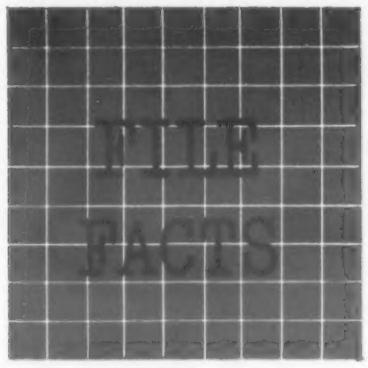


Metal Powders—continued

Production Method (or particle shape)	Mesh size (approx)	Purity, %	Supplier
ZINC			
——	−35, −150	98.80 min	Ha
——	——	——	M
——	−200	98	MD
——	Various sizes: −20 to −200	98.80 min	NJ
Atomization	——	99.5 min	PML
ZIRCONIUM			
——	−150	94 and 99	FM
——	−250	99.50 min	Ha
——	——	——	M
Hydride method	−60, −325	95 to 98	MH

Alloy Powders

Production Method (or particle shape)	Mesh size (approx)	Composition and Purity, %	Supplier
ALUMINUM ALLOYS			
Mechanical comminution	Various sizes	50 Mg −50 Al	Rea
BABBITT			
Atomization	−40, −100, −200, −325	99.5 min	Gl
BRASS			
Special process	−40, −100, −200, −325	99.5 min	Gl
(Spherical)	−28, −60, −100	50 to 90 Cu (some with 0.2 to 0.3 P)	Ha
——	−100	Various Cu-Zn compositions with several % Al or Pb	Ha
——	−100	85-5-5-5 (ASTM spec)	MD
——	−100	80-10-10 (ASTM spec)	MD
(Irregular)	−60, −100	Various compositions: 50 to 90 Cu; small % P, Pb, Al or Fe	NJ
Atomization (Irregular)	——	Various compositions: 60 to 90 Cu, small % P or Pb	PML
BRONZE			
Atomization	Various sizes	To specs	AM
Special process	−40, −100, −200, −325	99.5 min	Gl
Atomization	Various sizes, from 40% to 95%−325	To specs	Gr
Atomization	Various sizes, from 40% to 95%−325	Leaded (purity to specs)	Gr
——	−30+60	90 Cu −10 Sn	Ha
——	−60+100, −100+325	90 Cu	Ha
——	−100	90 Cu −10 Sn	MD
——	−100	Various compositions: 90 to 93 Cu, 5 to 10 Sn, 1.5 Zn added to ore grade	NJ
Atomization (spherical or irregular)	——	Various compositions: 50 to 90 Cu	PML
CHROMIUM ALLOYS			
(Irregular)	−20, −50, −100, −325 and micron size	Various compositions	AMP
——	−100	20 Cr −80 Ni	Ha
——	——	Cr-Co; various compositions	Ha
Hydride method	−100	Cr-Co (30-70, 40-60, 70-30)	MH
Hydride method	−100, −150	Cr-Ni (80-20, 65-20, 50-50, 40-60, 20-80)	MH
——	−60	70 Cr −30 Mo (99 purity)	SC
——	−60	Cr-W; 60 Cr (98.5 purity)	SC
COBALT ALLOYS			
(Irregular)	−20, −50, −100, −325 and micron size	——	AMP

Alloy Powders—continued

Production Method (or particle shape)	Mesh size (approx)	Composition and Purity, %	Supplier
COPPER ALLOYS (See also Brass, Bronze, Nickel Silver)			
Atomization	Various sizes	Various Cu-Pb compositions, with up to 10 Sn and up to 4 Zn	AM
Special process	−30, −40, −60, −80	Cu-Sn (99.5 min)	Gl
Atomization	Various sizes; from 40 to 95% −325	Cu-Sn-Pb to specs	Gr
——	−100	Phosphorous copper (8.5 P)	Ha
——	−60, −100, −200	Beryllium copper (2, 3 or 4 Be)	Ha
——	——	Copper-coated iron (8 Cu-Fe)	Ha
——	−100	Cupro-nickel (ASTM specs)	MD
——	Various sizes: −10 to −150	Cu-Sn various compositions with 2.5 to 10.5 Sn	MD
——	−100	Phosphorous copper ASTM spec	MD
Atomization	——	Cu-Pb; various compositions	PML
IRON ALLOYS			
——	−20, −50, −100, −325 and micron size	——	AMP
——	Various sizes	Ni-Fe, Cr-Fe, Co-Fe and others	Ha
(Spherical)	−80	8 Cu, 3 Ni, bal Fe (96.0 min metallic)	MH
Atomization	——	Various compositions made to order	PML
Atomization (irregular)	−50, −100, −150, −200, −325	Si-Fe, Ni-Fe	V
MOLYBDENUM-CHROMIUM ALLOYS			
——	−60	70 Mo −30 Cr (99 purity)	SC
NICKEL ALLOYS			
(Irregular)	−20, −50, −100, −325 and micron size	Various compositions	AMP
Atomization	−50, −100, −150, −200, −325	80 Ni −20 Cr	V
NICKEL SILVER			
——	−200	64 Cu −18 Zn −18 Ni	Ha
——	−100	ASTM specs	MD
Atomization	−100	64 Cu −18 Zn −18 Ni and with 1.5 Pb	NJ
Atomization	−100	70 Cu −20 Zn −10 Ni	NJ
(Irregular)	−100	64 Cu −18 Zn −18 Ni, and with 1.5 Pb	NJ
(Irregular)	−100	70 Cu −20 Zn −10 Ni	NJ
Atomization	——	Various compositions made to order	PML
SILVER ALLOYS			
(Irregular)	−20, −50, −100, −325 and micron size	——	AMP
STEELS			
——	−150, −200	98.5 to 99 Fe	Be
Atomization	−40, −80, −325	98 Fe min	RS
		Stainless Steels	
Atomization (irregular)	−40+100, −40, −100, −200	——	H
(Irregular)	−100	Types 302, 302B, 316, 318 Si, 431	Ha
Atomization (irregular)	−50, −100, −150, −200, −325	Types 304, 316, 318, 347, 410, 431	V

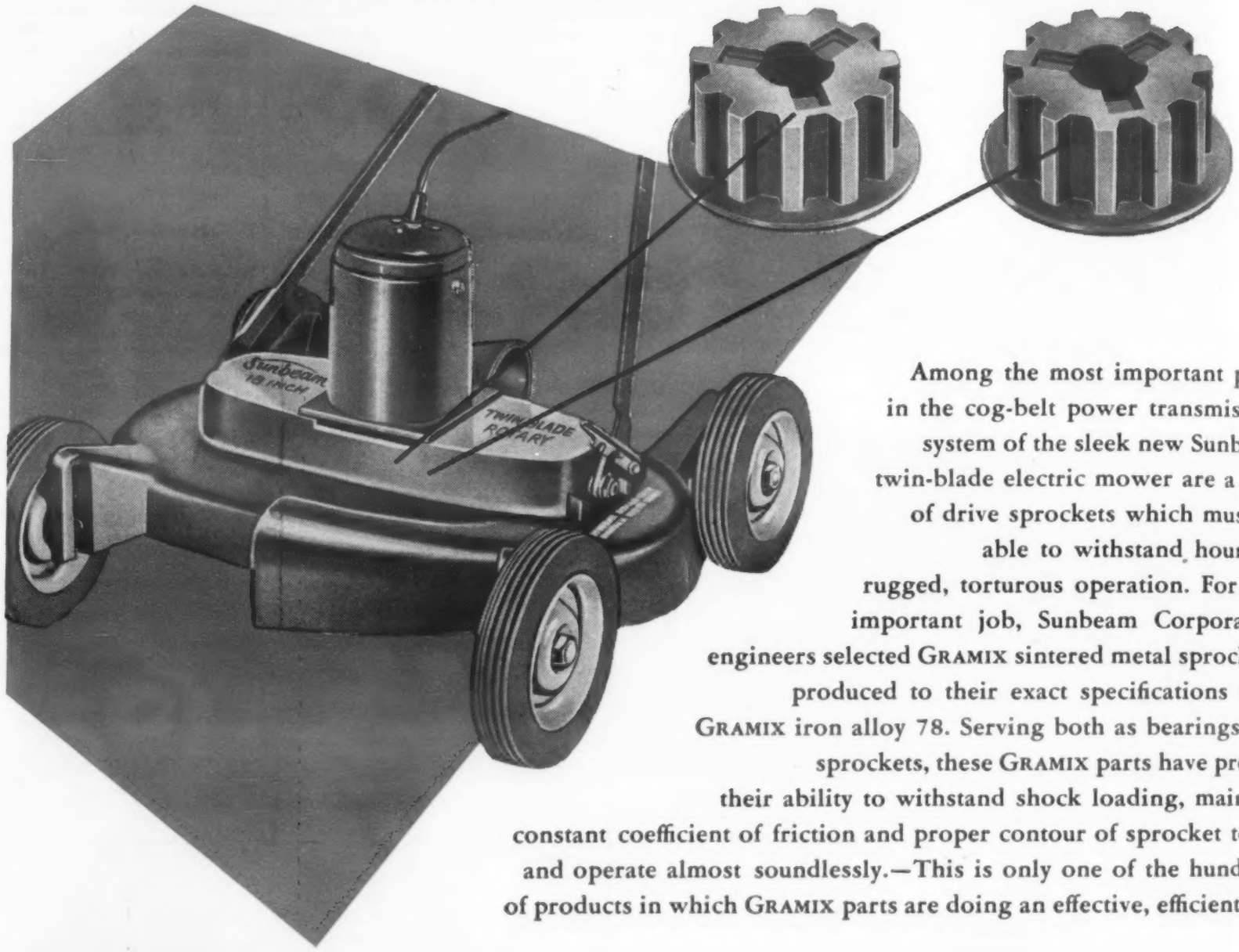
(continued on p 169)

for their new electrical mower

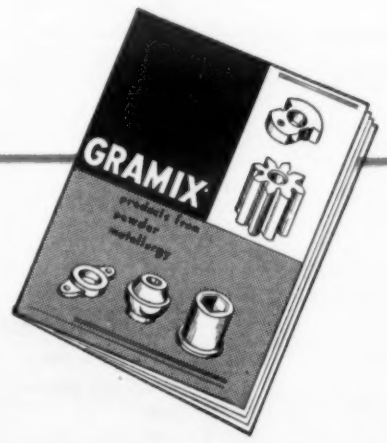
Sunbeam engineers specify long wearing

GRAMIX® iron sprockets

(PRODUCT OF POWDER METALLURGY)



Among the most important parts in the cog-belt power transmission system of the sleek new Sunbeam twin-blade electric mower are a pair of drive sprockets which must be able to withstand hours of rugged, torturous operation. For this important job, Sunbeam Corporation engineers selected GRAMIX sintered metal sprockets, produced to their exact specifications with GRAMIX iron alloy 78. Serving both as bearings and sprockets, these GRAMIX parts have proved their ability to withstand shock loading, maintain constant coefficient of friction and proper contour of sprocket teeth, and operate almost soundlessly.—This is only one of the hundreds of products in which GRAMIX parts are doing an effective, efficient job.



Write for this book. Being die-pressed to shape, then sintered, GRAMIX parts usually cost less than machined pieces . . . yet can be produced to tolerances as close as .0005 inch. GRAMIX Bulletin No. 21 tells the whole story. Write today for your copy.

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Alloy Powders—continued

Production Method (or particle shape)	Mesh size (approx)	Composition and Purity, %	Supplier
STEELS continued			
		Alloy Steels	
(Irregular)	−20, −50, −100, −325 and micron size	Various types	AMP
—	—	Made to specs	H
—	—	4650, other AISI compositions	Ha
—	—	To specs	Pl
Atomization (irregular)	—	AISI/SAE 4630	V
TIN-LEAD ALLOYS			
Atomization	−100, −150, −325 −100 and finer	Various compositions	AM
—	—	Various compositions	Be
Atomization	−40, −100, −200, −325	99.5 min	Gl
—	Various sizes	50 to 85 Pb, bal Sn	Ha

Alloy Powders—continued

Production Method (or particle shape)	Mesh size (approx)	Composition and Purity, %	Supplier
TIN-LEAD ALLOYS continued			
Atomization	−100	99.5 Sn + Pb	NL
Atomization	—	Various compositions	PML
TITANIUM ALLOYS			
Hydride method	−325	Co-Ti (20-80, 50-50)	MH
Hydride method	−325	Ti-Ni (30-70, 50-50, 70-30)	MH
—	—	Ti-Fe; various compositions	NL
Comminution	−80, −100	Ti-Ni (approx 60 Ni)	NL
ZIRCONIUM ALLOYS			
Hydride method	−325	Zr-Ni (30-70, 50-50, 70-30)	MH
Hydride method	−325	50 Zr −50 Co	MH
SPECIAL ALLOYS			
Various	Various	Made to order	AM,
Atomization	—	Made to order	Ha, V, PML

Suppliers and Their Addresses

Code Letter	
AEM	Associated Engineering and Mfg. Corp. Glen Ridge, N. J.
Al	Aluminum Co. of America 230 Park Ave. New York 17, N. Y.
AM	American Metal Co., Ltd. 61 Broadway New York, N. Y.
AMP	Alloy Metal Powders, Inc. 230-240 Eagle St. Brooklyn 22, N. Y.
An	Antara Chemicals Div. of General Dyestuff Corp. 435 Hudson St. New York 14, N. Y.
Ap	Apex Smelting Co. 2537 W. Taylor St. Chicago 12, Ill.
AWS	Allen Wood Steel Co. Conshohocken, Pa.
B	Paul Blum Co. 315 Larkin St. Buffalo 10, N. Y.
BB	Brush Beryllium Co. 4301 Perkins Ave. Cleveland 3, Ohio
Be	Belmont Smelting and Refining Works 330 Belmont Ave. Brooklyn 1, N. Y.
C	Cleveland Tungsten, Inc. 10200 Meech Ave. Cleveland 5, Ohio
EM	Easton Metal Powder Co. 233 Broadway New York 7, N. Y.
E	Ekstrand & Tholand 420 Lexington Ave. New York 17, N. Y.
ES	Eastern Smelting and Refining Corp. 107 W. Brookline St. Boston 18, Mass.
Fa	Fansteel Metallurgical Corp. North Chicago, Ill.
Fe	Ferrum Ltd. 506 Ste. Madeleine Blvd. Cap de la Madeleine Quebec, Canada
FM	Foote Mineral Co. 18 W. Chelten Ave. Philadelphia 44, Pa.

Code Letter	
Gl	Glidden Co. Hammond, Ind.
Gr	Greenback Industries, Inc. 2527 W. Maple Rd. Birmingham, Mich.
H	Hoeganaes Sponge Iron Corp. Riverton, N. J.
Ha	Charles Hardy Inc. 420 Lexington Ave. New York 17, N. Y.
HH	Handy & Harman 82 Fulton St. New York 38, N. Y.
HVA	Husqvarna Vapenfabriks AB Huskvarna, Sweden
J	A. Johnson & Co., Inc. 21 West St. New York 6, N. Y.
K	Kennametal, Inc. Latrobe, Pa.
M	A. D. Mackay 198 Broadway New York, N. Y.
Ma	Magnetic Powders, Inc. Johnsonburg, Pa.
MD	Metals Disintegrating Co. Elizabeth (B), N. J.
MH	Metal Hydrides, Inc. 12 Congress St. Beverly, Mass.
MM	Malone Metal Powders, Inc. 220 W. 42nd St. New York 36, N. Y.
MP	Metal Powders Ltd. 73 Fifth Ave. Iberville, Quebec
Mu	Murex Ltd. Rainham Essex, England
NAP	North American Philips Co., Inc. Elmet Division Lewiston, Me.
NL	National Lead Co. Metal Div. 111 Broadway New York 6, N. Y.
NJ	New Jersey Zinc Sales Co. 160 Front St. New York 38, N. Y.

Code Letter	
Pl	Plastic Metals Div. National Radiator Co. 342 Madison Ave. New York 17, N. Y.
PML	Powder Metallurgy Ltd. 59-62 High Holborn London WC1, England
Py	Pyron Corp. Box E, LaSalle Station Niagara Falls, N. Y.
R	Reynolds Metals Co. 2500 S. Third St. Louisville 1, Ky.
Rea	Reade Manufacturing Co., Inc. Metal Powder Div. 135 Hoboken Ave. Jersey City 2, N. J.
RS	Republic Steel Corp. Metal Powder Div. Landis Ave. Toledo 5, Ohio
S	Sylvania Electric Products, Inc. Tungsten & Chemical Div. P. O. Box No. 70 Towanda, Pa.
SC	Shieldalloy Corp. West Boulevard Newfield, N. J.
SCN	Sylvania-Corning Nuclear Corp. P. O. Box 59 Bayside, N. Y.
SG	Sherritt Gordon Mines Ltd. Chemical Metallurgical Div. Fort Saskatchewan Alberta, Canada
T	Titanium Metals Corp. of America 233 Broadway New York 7, N. Y.
U	U. S. Magnesium Co. Pleasant Valley, N. Y.
UC	Electro Metallurgical Co. Div. of Union Carbide & Carbon Corp. 30 E. 42nd St. New York 17, N. Y.
UI	United International Research, Inc. 38-15 30th Street Long Island City 1, N. Y.
UT	Dept. of Chemistry University of Tennessee Knoxville, Tenn.
V	Vanadium-Alloys Steel Co. Latrobe, Pa.

[a]Many of the companies listed make special mesh size distributions or special alloy compositions to order.

Compiled by Herbert B. Michaelson, International Business Machines Corp.

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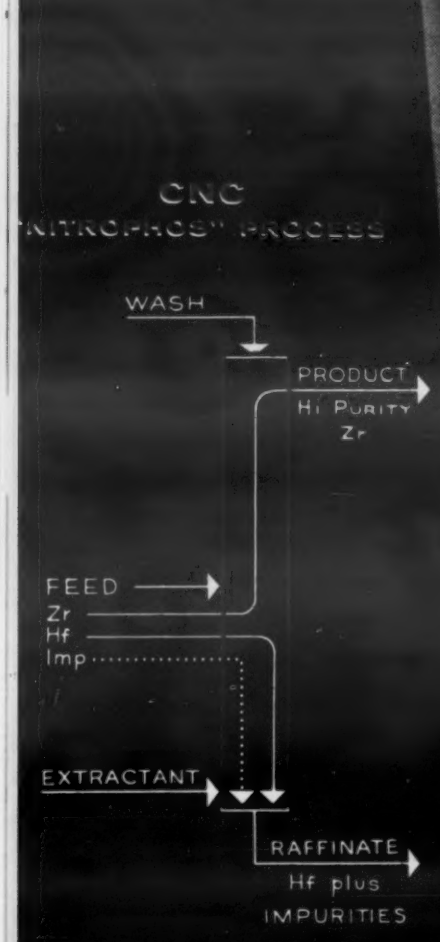

The new Columbia-National Zirconium Plant near Pensacola, Florida is the most modern in the world. The "Nitrophos" process continuously and automatically separates hafnium from zirconium and removes impurities, thus assuring uniform, high quality zirconium sponge.

The Zirconium Age has arrived! Columbia-National Corporation with its new sponge producing facility nearing commercial operation offers you a new source of zirconium at a new low price.

Uniform high quality zirconium is assured by the only fully integrated operation converting zircon sand to sponge at one location under the responsibility of one management. The unique "Nitrophos" extraction process is used to separate and purify zirconium and hafnium in this plant.

Reactor-grade and hafnium-containing commercial-grade zirconium sponge will be produced in sufficient quantities to fill government and industry requirements. Leading metal converters and fabricators are now supplying zirconium mill and finished products.

There is new opportunity in the Zirconium Age. You are urged to investigate its use in atomic reactors and in process equipment where corrosion conditions are severe. Columbia-National is ready to help with melting and application assistance. Write for technical data on fabrication, properties and corrosion resistance. Columbia-National Corporation, 70 Memorial Drive, Cambridge, Mass.

ILLUSTRATION OF TYPICAL REACTOR CORE COURTESY WESTINGHOUSE ELECTRIC CORP.

Columbia-National Corporation

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NEW METALS FOR INDUSTRY

What's new IN MATERIALS

Contents

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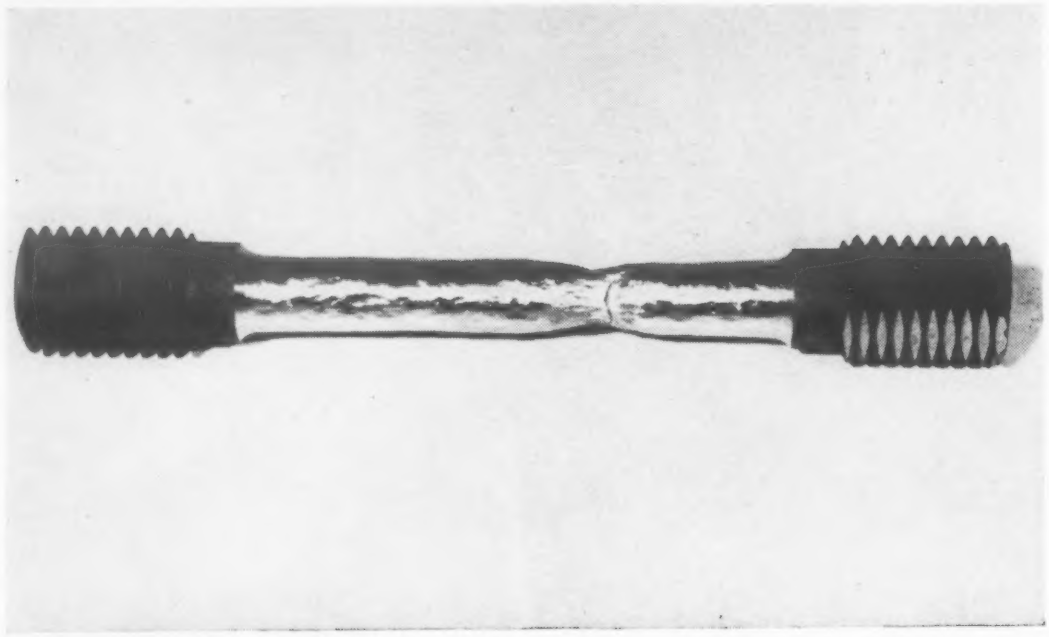


***High ductility** of CD-4MCu corrosion resistant cast alloy is shown by this pulled tensile specimen.*

Relatively low nickel content but . . .

Cast Stainless Alloy Is Stronger, More Resistant Than 18-8

■ A new high strength, cast stainless alloy combines excellent mechanical properties with excellent corrosion resistance. Developed in Ohio State University's Corrosion Research Laboratories as part of the research program of the Alloy Casting Institute, the new material represents substantial progress in the search for high strength, corrosion resistant alloys.

Although many stainless materials have been developed that exhibit high strength and hardness, some of them have inferior corrosion resistance as compared to regular 18-8 stainless. What makes the development of the new alloy (designated CD-4MCu) significant is that it not only possesses better mechanical properties than 18-8 but also has better corrosion resistance. Moreover, as shown in the accompanying table, the new alloy uses relatively little nickel.

According to Dr. M. G. Fontana, chairman of Ohio State University's Metallurgical Engineering Dept., not only is the corrosion rate of the new alloy very low but there is no tendency for the corrosion rate to increase with time. As a result, manufacturers of valves, pumps, fittings, high pressure components, etc., "can be assured that there will be no loss of corrosion resistance over a long period of time."

Part of the testing procedure to determine corrosion resistance of the new alloy, involved bending specimens after exposure to a boiling copper sulfate-sulfuric acid solution. No decrease in angle of bend before cracking was observed after exposure for 72 hr. In other tests, the new alloy showed no corrosion at room temperature in 10% sulfuric acid, 50% sulfuric acid or 0.5% hydrochloric acid; even in 5% hydrochloric acid the corrosion rate was only 60 mils per year.

In addition to better corrosion resistance, the new alloy is reported to have better machinability than 18-8 stainless, good welding and grinding characteristics, and good foundry characteristics (fluidity and feeding).

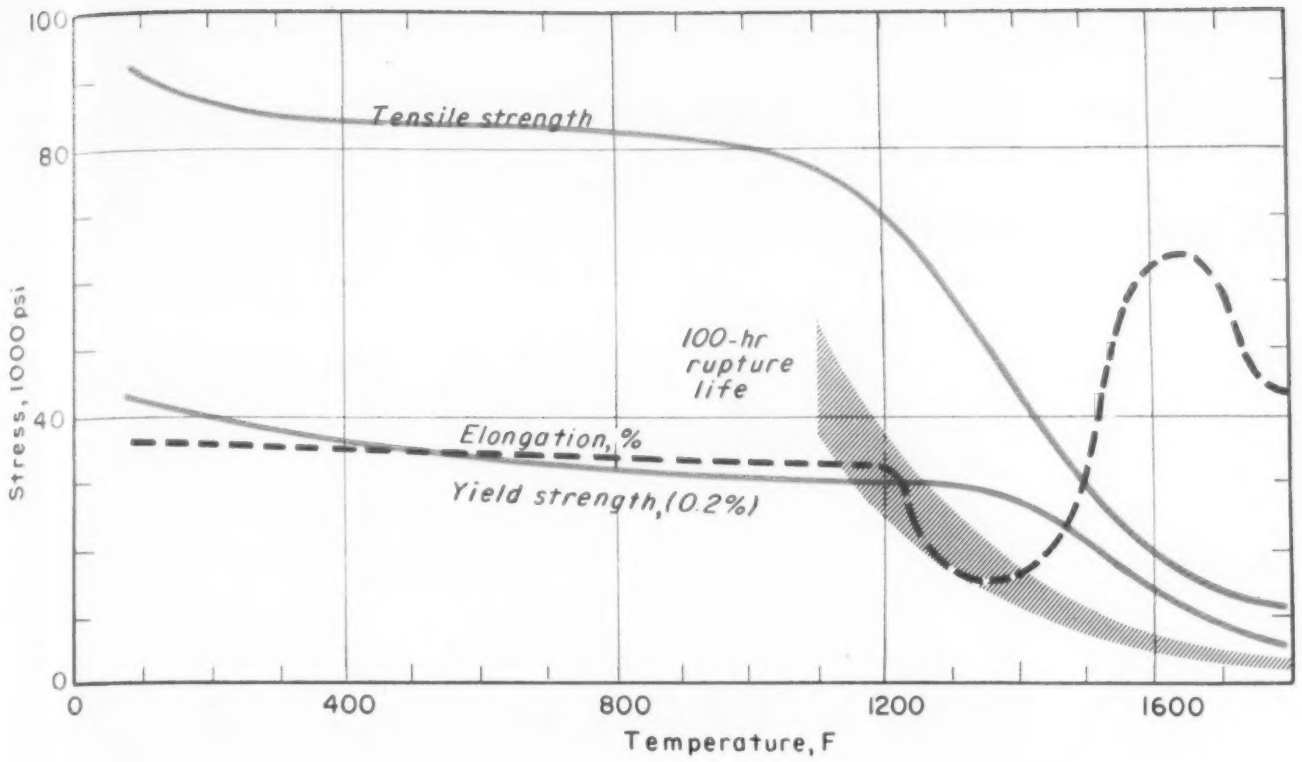
PROPERTIES OF CD-4MCu

Heat Treatment		Tensile Strength, psi	Yield Strength, psi	Elongation, %	Reduction of Area, %	Brinell Hardness	Charpy V Notch, ft-lb	Corrosion Rate, mils/yr[c]
Temp, F	Time, hr							
850	4[a]	141,000	100,000	25	38	302	9.5	6.5
950	3[b]	140,000	120,000	16	—	321	—	6[d]
1950	2 (w.q.)	113,000	81,000	29	48	248	104	6
As cast		121,000	84,000	27	41	262	19	18
2050	1 (w.q.)	103,000	85,000	19	—	250	—	7[d]

[a]Aging treatment preceded by water quenching after 2 hr at 1950 F.
[b]Aging treatment preceded by water quenching after 1 hr at 2050 F.
[c]In boiling 65% nitric acid. Average of five 48-hr periods; two specimens each.
[d]Average of two 48-hr periods; single specimens.

COMPOSITION OF CD-4MCu, %

Chromium	25-27
Nickel	4.75-6.00
Carbon	0.04 max
Molybdenum	1.75-2.25
Copper	2.75-3.25
Silicon	1.0 max
Manganese	1.0 max
Iron	bal



Tensile and rupture *properties of Incoloy T.*

Improved Nickel Alloy Sheet Can Be Used up to 1600 F

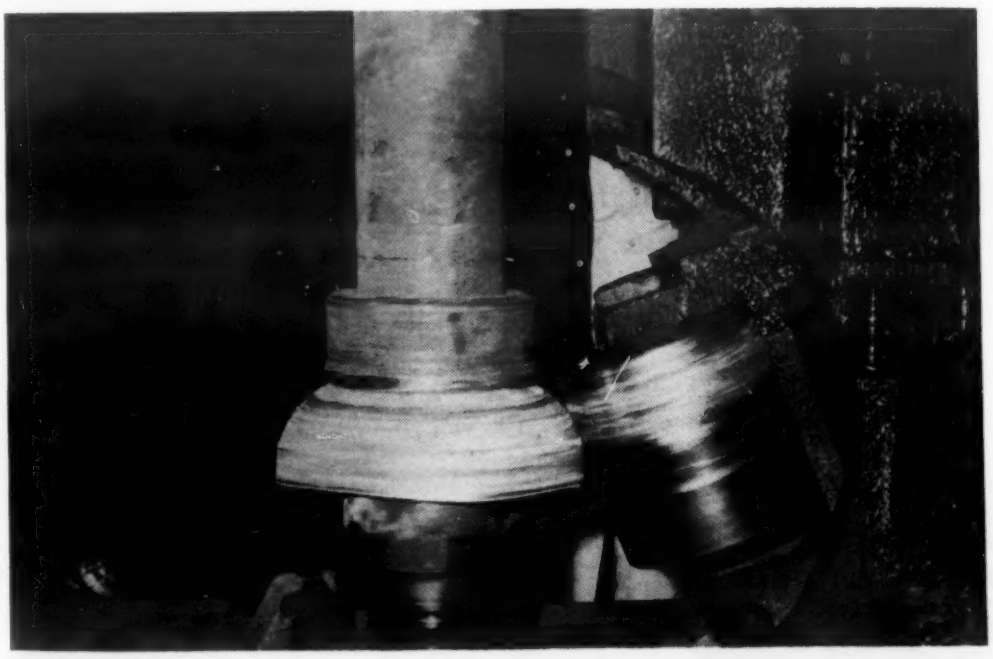
■ A high temperature alloy sheet material, developed by International Nickel Co., Inc., New York, N. Y., is expected to find wide use in highly stressed parts of jet engine combustion systems and in airframes used for hypersonic flight.

The new alloy, called Incoloy T, differs from the conventional Incoloy nickel-chromium-iron alloy in that it contains approximately 1% titanium. As a result of the titanium addition, the alloy exhibits improved tensile and rupture properties and has excellent oxidation resistance up to 1600-1700 F. Cyclic oxidation tests conducted on the alloy at 1600 F for periods from 100 to 1000 hr showed that although the material gains in weight the oxide layer that is formed adheres tightly to the surface.

The alloy sheet is designed to operate at temperatures up to 1600 F. It is generally annealed at 1900 to 1950 F. However, successful annealing has been accomplished by heating 20-30 min at 1800 to 1850 F, followed by rapid cooling in air. For use at temperatures below 1200 F, tensile and rupture strengths can be improved by cold working.

COMPOSITION OF INCOLOY T, %

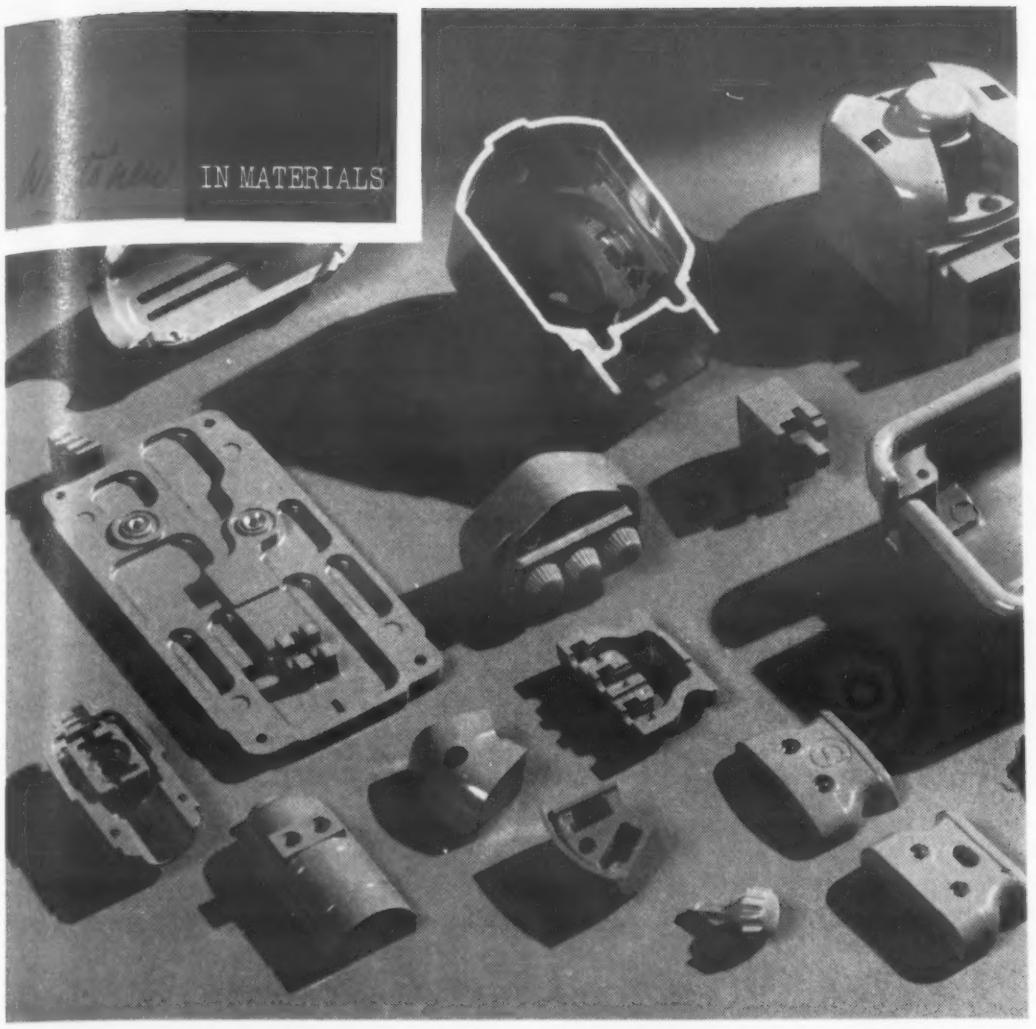
Carbon	0.10 max
Manganese	1.50 max
Silicon	1.00 max
Chromium	19.0-22.0 max
Nickel Cobalt	30.0-34.0
Copper	0.50 max
Sulfur	0.03 max
Titanium	0.75-1.50
Iron	bal



Spinning titanium—For the first time a "head" of solid titanium has been formed without the use of costly dies and stamping equipment, according to Lukens Steel Co.

In a research program conducted jointly by Lukens and Rem-Cru Titanium, Inc., a commercially pure titanium plate was worked on a spinning machine at a minimum of 600 F. (The plate had been previously heated under close temperature control at 1400-1450 F.) An elliptical-shaped head 16-in. in dia and ¼ in. thick was successfully spun on the standard equipment shown at the left.

(more What's New on p 175)



Sewing machine parts *molded of new polyester compound.*

TYPICAL PROPERTIES OF DUREZ POLYESTER MOLDING COMPOUND

PHYSICAL PROPERTIES	
Specific Gravity	1.79
Tensile Strength, psi[b]	5000
Izod Impact Strength, ft-lb/in.[b]	0.28
Flexural Strength, psi[b]	8500
Max Water Absorption, %	0.5
Compressive Strength, psi [b]	22,000
Molding Shrinkage, in./in.[a]	0.008
Heat Distortion (264 psi), F	360
Mod of Elasticity in Tension, 10^6 psi[b]	1.1
Rockwell Hardness[a]	M105
ELECTRICAL PROPERTIES	
Dielectric Strength, v/mil[c]	
Short-Time	400
Step-by-Step	324
Volume Resistivity, ohm-cm[b]	5×10^{14}
Dissipation (power) Factor[b]	
60 cps	0.011
1 kc	0.011
1 mc	0.022
Dielectric Constant[b]	
60 cps	4.6
1 kc	4.6
1 mc	4.4
Arc Resistance, sec	125

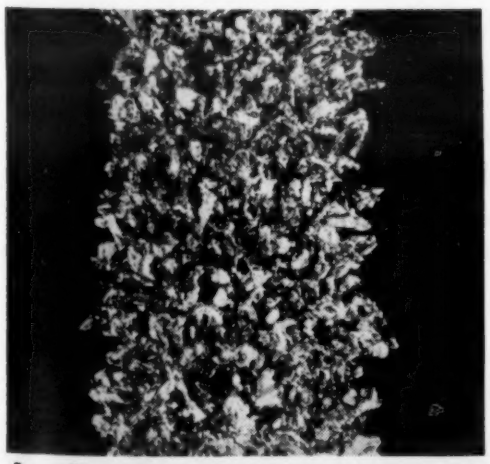
[a]Cond 50% R. H. at 73 F.
[b]Cond 48 hr at 122F, tested at room temp.
[c]Cond 48 hr, 50% R. H. at 73 F.

New Line of Polyesters Available Next Fall

A line of cellulose-filled, light colored polyester molding compounds will be made available next fall by Durez Plastics Div., Hooker Electrochemical Co., Niagara Falls, N. Y. The new polyesters, produced experimentally for about two years, will be made available in both regular and self-extinguishing grades.

The thermosetting molding compounds are readily molded and can be handled in conventional molding equipment. According to the producer, they have good shelf life and preforming characteristics. The new polyesters are similar to phenolic molding compounds in their physical properties, and are said to offer good color stability and heat and moisture resistance. Electrical properties of the polyesters are better than those of the phenolics. The new material, ranging in price from 42 to 77¢ per lb, will be sold in fine granular form.

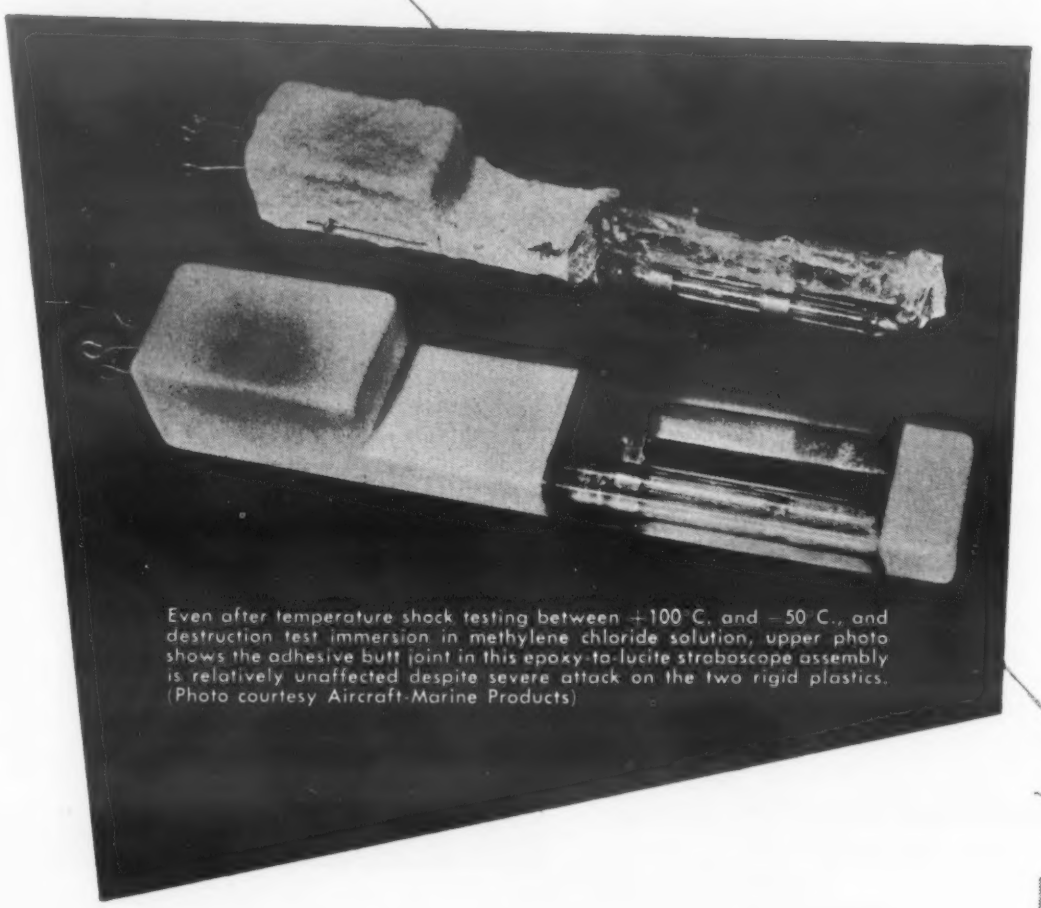
High Purity Metal Improves Chromium Alloys



As deposited *high purity iodide chromium (⅔' size).*

Chromium-base alloys containing a high purity iodide chromium metal have shown the greatest degree of ductility thus far demonstrated for chromium and chromium-base alloys. The iodide chromium, prepared by an improved iodide decomposition process developed at Battelle Memorial Institute, is available in limited quantities from Chilean Nitrate Sales Corp., 120 Broadway, New York 5, N. Y. The company believes a similar material can be commercially produced, and plans for its production are under consideration.

A number of unsuccessful attempts have been made in the past to increase the chromium content of high chromium alloys to obtain better high temperature properties. These attempts were unsuccessful because of the poor fabrication characteristics of the alloys (see photo p 177). However, recent investigations have shown that use of iodide chro-



Even after temperature shock testing between +100° C. and −50° C., and destruction test immersion in methylene chloride solution, upper photo shows the adhesive butt joint in this epoxy-to-lucite straboscope assembly is relatively unaffected despite severe attack on the two rigid plastics. (Photo courtesy Aircraft-Marine Products)

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INDUSTRIAL ADHESIVES

Bondmaster® Adhesives

for plastics and metals

This unusual job was bonded without heat and without pressure, using BONDMASTER M654, a 100% solids, epoxy based adhesive—one of 30 formulations we've developed for joining metals and plastics (rigid, foamed and flexible) to themselves and to each other.

Let us help you with your specialized bonding problems. A free "Adhesives Selector Chart" is yours for the asking.

RUBBER & ASBESTOS CORP.
227 BELLEVILLE AVE., BLOOMFIELD, N.J.

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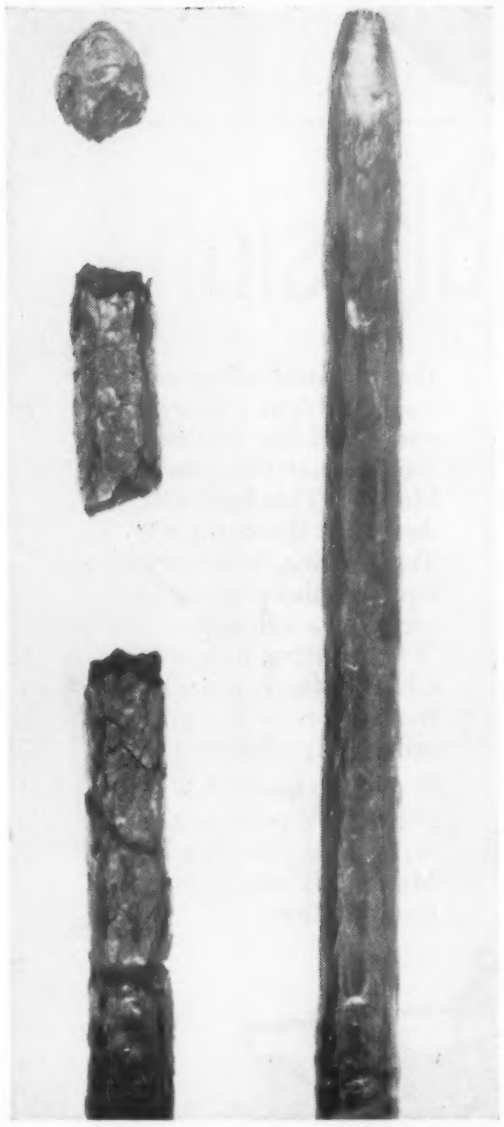
mium means that as much as 5 to 10% more chromium can be added to certain alloys without impairing either fabrication characteristics or room temperature ductility.

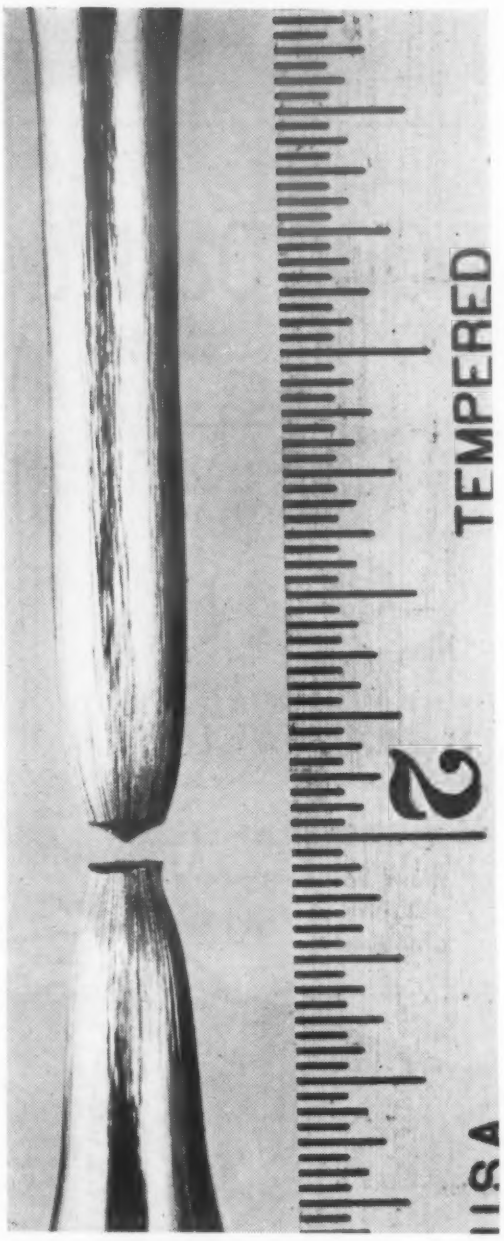
Improved ductility

In room temperature tensile tests, the new wrought chromium-base alloys have shown as much as 44% elongation and 78% reduction in area. The improved ductility is attributed to the iodide chromium and to the fibrous structure of the wrought metal. Modulus of elasticity was also improved to a certain extent in alloys containing iodide chromium. As yet, transverse ductility has not been determined.

Despite these favorable properties, the supplier says, considerable development will be required before iodide chromium alloys can be considered useful structural materials.



***Fabrication characteristics** of iodide chromium (right) are compared with those of hydrogen treated electrolytic chromium (left). Both were sheathed in mild steel and swaged under identical conditions.*

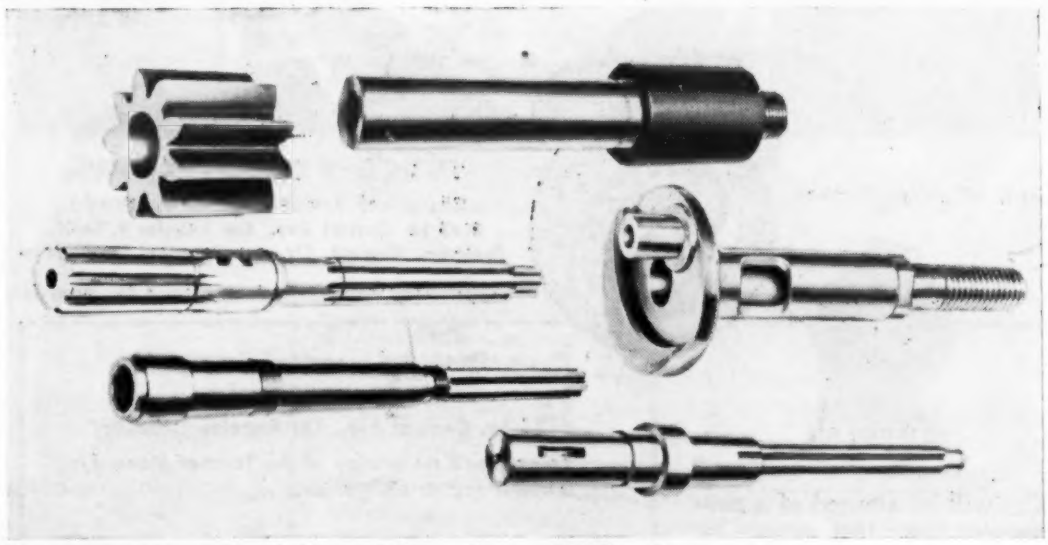


***Fracture characteristics** of ductile iodide chromium metal.*

Here are further details on "e.t.d."

High Strength Steel Bars Need No Heat Treatment

■ Additional information has been made available on the Elevated Temperature Drawing ("e.t.d.") process La Salle Steel Co. uses to make steel bars having excellent physical and mechanical properties without heat treatment. Reported in the Dec '56 issue of MATERIALS & METHODS (p 143), the process is claimed to produce steel bar products in which, for the first time, the dimensional tolerances, surface finish and excellent machinability generally associated with cold finished bars



***Improved bar stock** is used to make parts like these.*

For more information, turn to Reader Service Card, Circle No. 452

What's new IN MATERIALS

have been incorporated into a bar product which also has strength properties normally developed by heat treatment.

The properties depend upon three factors: 1) bar chemistry (0.40-0.48 carbon, 1.35-1.65 manganese, 0.04 phosphorus, 0.24-0.33 sulfur, and 0.15-0.30% silicon); 2) amount of reduction in cross section of the bar as it is drawn through a die; and 3) drawing temperature. As the bar is deformed at elevated temperatures (between 200 F and the lower critical temperature), three metallurgical phenomena take place: 1) the steel bar strain hardens by appropriate slip processes within the crystal structure; 2) it age hardens by precipitation of nitrides along with precipitation of carbon from supersaturated solid solution; and 3) a substructure develops within the grains.

The new material, called "Fatigue Proof," is claimed by the company to be the only material offered commercially with a guaranteed minimum Rockwell C value of 30, tensile strength of 140,000 psi and yield strength of 125,000 psi.

New Silicone Rubbers: Sponge, Low Shrink

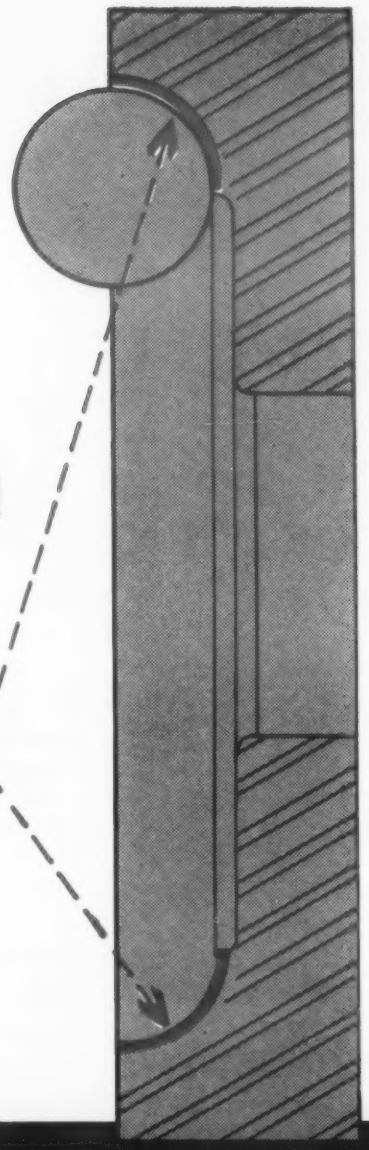
Four new silicone compounds have recently been introduced. One is a sponge rubber and the other three are low shrink compounds in the 50 through 70 durometer range.

1. Sponge rubber

A new 50-durometer silicone sponge rubber has recently been marketed by Garlock Packing Co., Palmyra, N. Y. Designated Style 9383, the material is flexible at temperatures of —100 F and is resistant to temperatures up to 500 F. It resists tearing and abrasion and has good compression set.

The sponge rubber is available

If you have a **heat-treating** job like this



You need an **Induction Heating Machine** like this

New TOCCOtron Machine 50 kw 500,000 cycles

For many years TOCCO has led the Induction Heating Field—manufacturing both motor-generator and vacuum tube oscillator type machines to meet every induction heating requirement. This new 50 KW TOCCOtron unit is a big brother to the 25 KW unit which has been serving the Metal-Working Industry for many years.

Here's What It Does

With a frequency range of 350,000 to 600,000 c.p.s. the TOCCOtron unit is ideal for surface hardening small diameter parts to shallow depths (as the bearing race illustrated above), through hardening or annealing small sections and soldering or brazing small assemblies where the heating effect must be very strictly localized.

The greater capacity of the new 50 KW TOCCOtron *doubles* production rates formerly achieved by TOCCOtron equipment.

A Really Complete Machine

This radio frequency unit is a truly complete induction heating machine. It contains not only all the direct current supply components and the oscillator components, but also all the control components required for either single or two station operation.

Among the standard features of the 50 KW TOCCOtron are:

1. The industrial heavy gauge steel cabinet which completely encloses all high potential circuits preventing radiation interference and personnel hazards.
2. Meters in all sensitive circuits to enable the user to obtain the maximum output and efficiency.
3. 3-phase quadrature filament excitation of rectifiers for maximum life.
4. Externally adjustable grid bias and drive control for ease in setting up new production runs.
5. Externally mounted circuit breaker and disconnect located so that it is easily accessible.
6. Tapped plate transformer allowing variations of plate voltage.

If your operation requires the hardening, annealing or brazing of very small parts in very big quantities the new 50 KW TOCCOtron can do the job better, faster and at lower cost than any other method available.

THE OHIO CRANKSHAFT COMPANY

***Mail Coupon Today*— NEW FREE Bulletin**

The Ohio Crankshaft Co. • Dept: T-4, Cleveland 5, Ohio

Please send catalog G showing TOCCO Induction Heating Equipment from 60 to 600,000 cycles.

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Company_____

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For more information, turn to Reader Service Card, Circle No. 486

PROPERTIES OF LOW SHRINK SILICONE RUBBERS

	L-WK-168	L-WK-170
ORIGINAL PROPERTIES		
Durometer A Hardness	57	77
Tensile Strength, psi	670	870
Elongation, %	135	80
Specific Gravity	1.23	1.41
AIR OVEN[a]		
Durometer A Change, %	0	0
Tensile Strength, Change, %	−1.8	−13
Elongation Change, %	−10	−18
ASTM No. 1 OIL[b]		
Durometer A Change, %	− 6	− 6
Tensile Strength, Change, %	+ 1	− 6
Elongation Change, %	0	− 8
Volume Change, %	+7.8	+ 7
Low Temp Flexibility[c]	OK	OK
Compression Set, %[d]	15	19

[a]Aged 70 hr at 450 F. [c]Aged 5 hr at −65 F.
[b]Aged 70 hr at 300 F. [d]Aged 24 hr at 350 F.

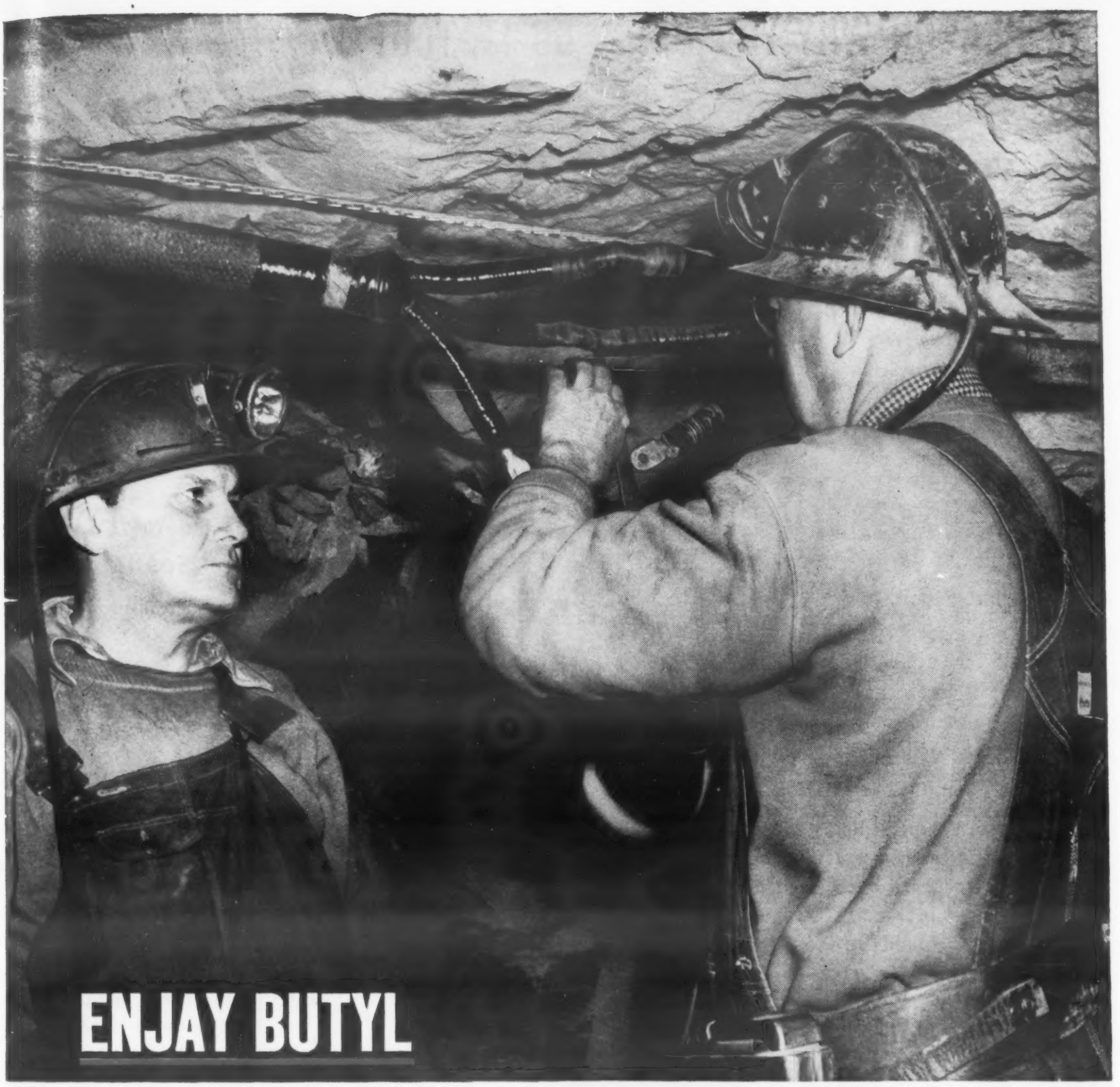
in sheets from 1/16 to ½ in. thick and in extrusions from ¼ to ¾ in. in dia. The material is recommended for aircraft door seals, ports and bomb bays.

2. Low shrink rubbers

Three low shrink silicone compounds in the 50 through 70 durometer range have been introduced by Acushnet Process Co., New Bedford, Mass. They are especially adaptable to o-rings and similar shapes, and their low shrinkage permits the use of tooling originally designed for organic rubbers. Free of toxic additives, the silicone rubbers can be used in the food and drug industries. Physical properties of two of the low shrink compounds are shown in the accompanying table.

Photosensitive Plastic? Needed for 3-D Models

A photosensitive thermoplastic resin to be used in the production of three-dimensional terrain models is now being sought by Horizons, Inc., of Cleveland. Working on a contract from the U.S. Naval Training Device Center, the research organization is trying to find such a material that will be



electrical wonder rubber OFFERS TRIPLE VALUE

Performance! Versatility! Economy! In all three, Enjay Butyl is the world's outstanding rubber value. In laboratory tests, and a wide variety of applications, no other rubber has matched Enjay Butyl's ability to resist ozone and corona, impact and abrasion, moisture and weathering . . . properties that make Enjay Butyl-made products *outstanding* performers.

Underground service cables, transformer housings, high-voltage industrial cables . . . in these, and many other electrical applications, Enjay Butyl outperforms and out-lasts *all other* types of rubber, synthetic *or* natural. *Low-in-cost* and *immediately available*, this truly wonder rubber may well be able to cut costs and improve performance in *your* products. For further information, and for expert technical assistance, contact the Enjay Company.

ENJAY

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ENJAY COMPANY, INC., 15 West 51st Street, New York 19, N. Y.

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ENJAY BUTYL

Enjay Butyl is the greatest rubber value in the world . . . the super-durable rubber with *outstanding* resistance to aging • abrasion • tear • chipping • cracking • ozone and corona • chemicals • gases • heat • cold • sunlight • moisture.

For more information, turn to Reader Service Card, Circle No. 368

What's new IN MATERIALS

thermally stable at temperatures of 300 F.

Contour lines and names of rivers, towns, hills and mountains, and other important terrain features will be transplanted from a negative to the resin through a photographic process. The resin will then be molded to a three-dimensional shape.

Copper-Cored Glass Wire for Sealing

By inserting a solid OFHC (oxygen-free high conductivity) copper core in a seamless sleeve of glass sealing alloy, General Plate Div. of Metals and Controls Corp. has come up with a sealing alloy wire that is claimed to have three times the electrical conductivity of solid alloy wire.

The new material is claimed to increase current carrying capacity with no increase in diameter, i.e., the same diameter wire can be used to meet demands for increased conductivity. If greater current capacity is not required, wire size can be reduced proportionately.

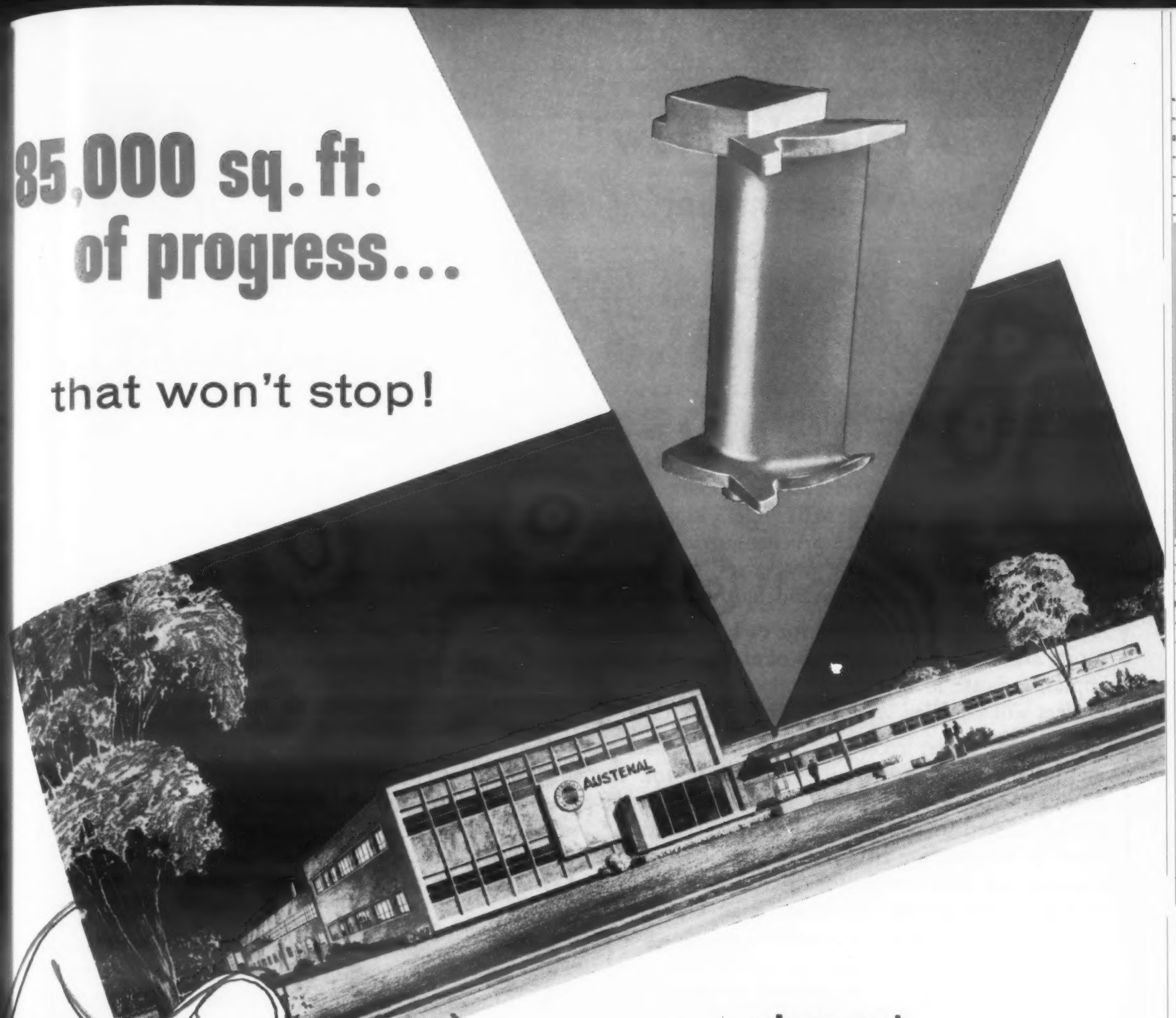
Among the applications listed for the material are glass-to-metal seals for terminals and terminal blocks, and hermetic seal headers for unit terminals, switches, relays, coils, capacitors, rectifiers, transformers and potentiometers. The wire, supplied in coils, is available in diameters from 0.010 to 0.250 in. and in annealed or cold drawn tempers.

Cadmium Plating Bath Produces Bright Parts

A new cadmium plating process called Cadalume is said to increase brightness of the electroplate up to 10%. The life of plating bath brighteners is increased 400% and plating speeds

85,000 sq. ft. of progress...

that won't stop!



Austenal's new **microcast** *plant utilizes the ultimate in investment casting technique and equipment.*

Pioneer and leader in investment casting, Austenal, Inc., is building a new 85,000 square foot plant to augment its present Microcast production facilities.

Austenal's new LaPorte, Indiana plant will allow for greater casting versatility, with the precision and superiority inherent in Microcast parts.

New production line vacuum furnaces, designed especially for Austenal, will make possible the melting of high temperature alloys never before castable.

MICROCAST PRECISION CASTINGS PROCESS

austenal
INC.

microcast division
224 EAST 39th STREET, NEW YORK 16, N. Y.
7001 SOUTH CHICAGO AVE., CHICAGO 37, ILL.

Other Austenal Microcast research and production facilities located at:

DOVER, NEW JERSEY

CHICAGO, ILLINOIS

NEW YORK, NEW YORK

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are increased up to 10% with the new method. Developed by Hanson - Van - Winkle - Munning Co., Church St., Matawan, N. J., the process uses two brighteners: one for making up a new bath, the other for maintenance additions.

The clearness of the new plating bath helps in arranging work in either unlined or lined steel tanks.

Effect of Silicon on Properties of 4340

Transverse ductility is a major design criterion in the selection of steel for use in aircraft where tensile strengths in the range 200,000-300,000 psi are required. Since high-silicon alloys are among those used in aircraft the effects of silicon on transverse properties are of some interest. Accordingly, John Vajda, John T. Hauser and Cyril Wells, of Carnegie Institute of Technology, recently conducted an investigation to determine the effects on transverse properties in the quenched and tempered condition of adding 1% and 1.5% silicon to an AISI 4340 steel.

Earlier investigators had demechanical properties of high strength steels quenched to martensite and subsequently tempered to various tensile strengh levels. This new investigation was designed to determine the properties of high strength steels of such mass and so end quenched that a whole range of structures would be developed during quenching.

Some of the conclusions reached by the investigators and presented at the 38th annual convention of the American Society for Metals, are:

1. The maximum tempering temperature at which silicon increased resistance to softening during tempering seemed to be higher in fully quenched than in slack quenched steels.

2. The ratio of yield strength

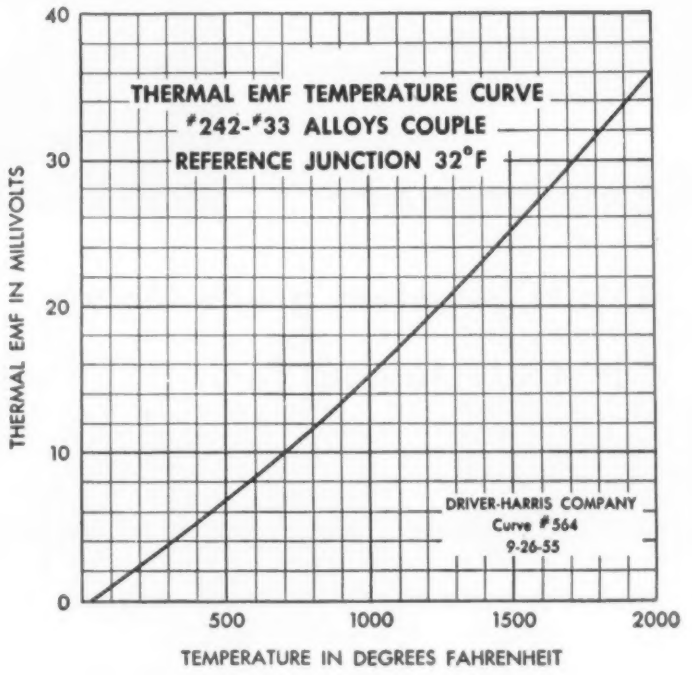
Driver-Harris Announces Major Advance in Pyrometry!

New #242-33 Thermocouple* for Reducing Atmospheres Maintains Calibration Through a Greatly Extended Life

This new Driver-Harris Thermocouple was developed primarily to withstand industrial reducing atmospheres at high temperatures and thereby to end the danger of runaway furnaces and ruined charges.

Unusually high resistance to "green-rot" attack is the outstanding property of the alloys of this thermocouple, whose analysis is:

Positive Leg (No. 242 Alloy)	Negative Leg (No. 33 Alloy)
80/20 Ni-Cr + Cb	3% Si-Ni



Although the thermal-emf response of this thermocouple is lower than the conventional thermocouple now in use, the slope of its temperature-emf curve is virtually parallel in the higher ranges of temperature in which both couples are designed to be used. Thus, the thermal-emf sensitivities are equivalent in the higher temperature ranges.

Tested against the conventional thermocouple in an atmosphere of the following nominal composition: CO...10%; CO_2...5%; CH_4...1%; H_2...16%; O_2...Nil; N_2...Balance (best for accelerating green-rot attack), exposure after 212 hours showed *only +0.13 mv. drift for the D-H thermocouple, and −7.54 mv. for the conventional thermocouple.*

When the thermal-emf of the conventional thermocouple *drops,* as in a reducing atmosphere such as this, the working temperature of the furnace controlled by it *rises.* However, when a #242-33 couple is used under the same conditions the thermal-emf remains substantially constant. This means that a furnace controlled with the new D-H thermocouple *cannot overheat and ruin charges.*

Members of the Heat-Treating and Instrument Manufacturing Industries are urged to investigate this new Driver-Harris Thermocouple without delay so that through their combined efforts all U. S. Industry can benefit. Complete technical data and application information is waiting for your inquiry. Write today to our Thermocouple Division.

*U. S. Patent No. 2,691,690

Driver-Harris COMPANY HARRISON, NEW JERSEY

BRANCHES: Chicago, Detroit, Cleveland, Louisville, Los Angeles, San Francisco In Canada: The B. GREENING WIRE COMPANY, Ltd., Hamilton, Ontario

MAKERS OF THE MOST COMPLETE LINE OF ALLOYS FOR THE ELECTICAL, ELECTRONIC, AND HEAT-TREATING INDUSTRIES

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to tensile strength in end quenched 7- by 7-in. rounds was decreased by silicon additions.

3. Marked improvement of both the yield strength and the yield to tensile ratio occurs as a result of tempering 17 hr at 500 F. It appears to be essentially independent of the transformation of retained austenite and may be associated with the relief of stress during tempering.

4. For a tempering treatment of 17 hr at 500 F, the addition of 1.5% silicon to AISI 4340 steel improves transverse reduction of area and transverse V-notch Charpy impact quality in 7-in. rounds. This treatment also improves transverse ductility and transverse toughness of the slack quenched, but not the fully quenched, material to which 1% silicon has been added. At a tempering temperature of 800 F both properties are impaired by added silicon.

5. Since the effect of silicon on transverse mechanical properties was determined over a very large range of cooling rates, the findings are applicable to large, massive forgings as well as to small forgings.

Intricate Coring for Aluminum Castings

A sheathed tube method of coring aluminum and magnesium castings has been developed by Howard Foundry Co., 1701 N. Kostner Ave., Chicago 39, Ill. The core consists of a preformed metal tube sheathed in a flexible refractory sleeve. Both the tube and the sleeve are removed after molding the casting.

The coring process permits small intricately shaped, unlined passages in sand castings. It is used when it is impossible to mold a passage with a sand core or when sand coring costs are high. Passages for transmitting oils, fuels, coolants and hydraulic

For more information, Circle No. 525 ➤

Here's selective heat treating that can be

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flame hardening

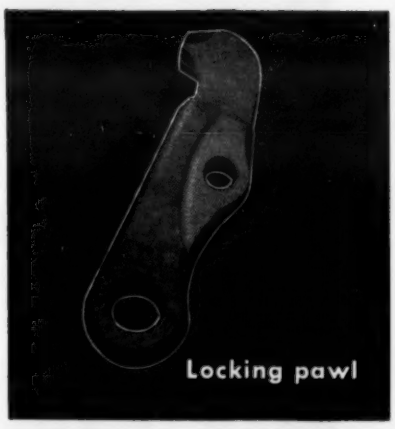
inductron
induction hardening

Transmission pinion pin

Locking pin

Bevel gear

Steering arm ball stud



Locking pawl

Cincinnati does both—selective flame or induction hardening—and the parts shown at right are typical of those that can be hardened by either method. If that's your situation, then talk to Cincinnati . . . headquarters for equipment that gives you the hardness wanted, where it's wanted, using the heat source most economical for you. Use electric power—or acetylene, propane, natural or manufactured gas—whichever is readily available to you or provides lowest cost.

Whether flame or induction, you can be assured of heat-treating machinery that will deliver the hardness you specify, and meet your cost-per-piece requirements, on high production quantities or varied, small-lot runs. It will be excellently engineered, equipped with the finest of components, thoroughly safeguarded, easily maintained.

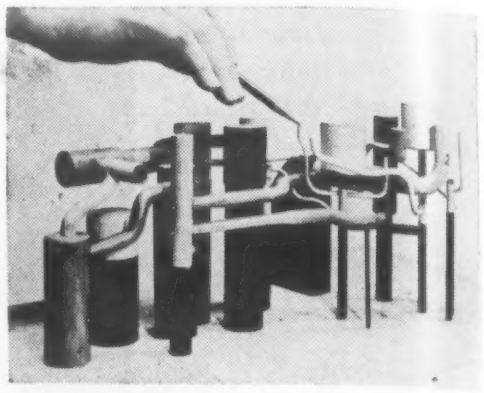
Call in a Process Machinery Division field engineer. He is ideally equipped to evaluate your needs and give you unbiased recommendations as to the most economical equipment for your selective surface hardening work.

CINCINNATI

flamatic and inductron
hardening machines

THE PROCESS MACHINERY DIVISION
THE CINCINNATI MILLING MACHINE CO
CINCINNATI 9, OHIO, U.S.A.

What's new IN MATERIALS



***Passages** for aluminum aircraft fuel control units are shown in this core mock-up.*

fluids do not have to be attached to exteriors of cast components nor do holes have to be drilled.

According to Howard Foundry, rigidity and dimensional stability of the sheathed tube core makes possible the casting of ⅛ in dia passages. The process is also adaptable to large core diameters.

Plastics Tubes, Shapes Made in Large Sizes

Large extruded plastics tubes and shapes—up to 3 in. i.d.—are now available from Anchor Plastics Co., Inc., 36-36 Thirty-Sixth St., Long Island City 6, N. Y. The hollow shapes may be obtained with heavy or thin wall thicknesses; in oval, rectangular and flanged cross sections; and with special surface effects such as ribs, beads and flutes.

Finishing Process Adds Sparkle to Aluminum

A new metal finishing technique which produces a startling glitter on the surface of aluminum sheet was recently announced by Aluminum Co. of America. Called "Spangle Sheet," the unusual effect is achieved by inducing the formation of abnormally large grains in a special aluminum alloy. Individual grains are then made to stand out in relief

APRIL
1957

DOW

Plastiatrics

DOW'S CLINICAL APPROACH TO HEALTHY PLASTICS APPLICATION

PRACTICAL ANSWER TO STATIC DUST COLLECTION

FIGURE 1

FIGURE 2

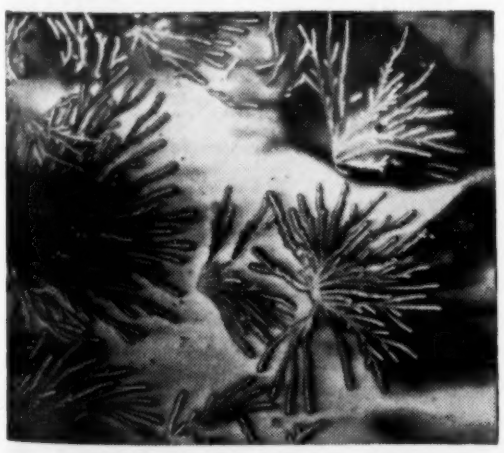


FIGURE 3—*Figures 1, 2 and 3 show typical static dust patterns on nontreated plastic surfaces as reproduced by Dow process using fluorescent pigments and "black light".*

DOW RESEARCH SHOWS HOW TO SPECIFY PROPER TREATMENT TO ASSURE DUST-FREE POLYSTYRENE SURFACES

FIGURE 4—*Here the same "black light" technique shows the absence of static charge on plastic surfaces destaticized by new method.*

AMERICA'S FIRST FAMILY OF POLYSTYRENES

GENERAL PURPOSE

- STYRON® 666
- STYRON 665 (Extrusion)
- STYRON 688 (Easy Flow)
- STYRON 689 (Easy Flow)

HIGH IMPACT

- STYRON 475
- STYRON 429 (Extrusion)
- STYRON 777 (Medium Impact)
- STYRON 440 (Heat Resistant)
- STYRON 480 (Extra High Impact)

HEAT RESISTANT

- STYRON 683
- STYRON 700

Static electricity which attracts and holds dust has long been acknowledged a problem in the manufacture and use of plastic products.

To overcome this behavior, Dow Plastics Technical Service developed new techniques for obtaining, observing and recording dust deposits. With these tools, Dow research explored hygroscopic chemicals that render the surface hydrophyllic or, in other words, that destaticize it.

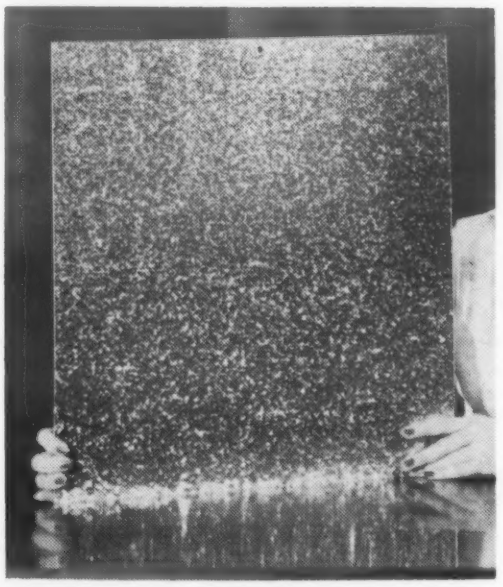
A method was developed and conclusively tested to provide freedom from static for long periods of time. This method includes dipping, spraying or otherwise coating moldings with a dilute detergent solution that reduces electrostatic charges to levels that prevent dust pickup.

FREE BULLETIN

A list of suitable compounds together with further information on this subject are contained in the bulletin, "Static Dust Collection of Plastics". Address: THE DOW CHEMICAL COMPANY, Midland, Michigan—Plastics Sales Department PL1540H.

YOU CAN DEPEND ON DOW

What's new IN MATERIALS



***Mirrorlike facets** catch light and cause sparkling on aluminum surface.*

by an acid etch, which also forms tiny mirrorlike facets on each grain. As the light source, the aluminum sheet or the position of the observer is moved, waves of light sparkle across the surface.

The new material, though not now commercially available, will be supplied by Alcoa in its finished form.

Comparison of Leaded and Nonleaded Steels

The effects of lead on the physical properties and the Charpy impact characteristics of leaded steels have been the topic of much discussion and investigation. Not a great deal has been done, however, on the differences, if any, between the Charpy impact characteristics of leaded and nonleaded steels. A. P. Weaver, of Inland Steel Co., reported on such an investigation at the 38th annual convention of the American Society for Metals. Working with C-1050 and C-1141 steels, Mr. Weaver found that:

1. Charpy impact transition temperatures, in seven out of eight instances, averaged 22 F lower for leaded steels than for the corresponding nonleaded grades.

2. There were no significant

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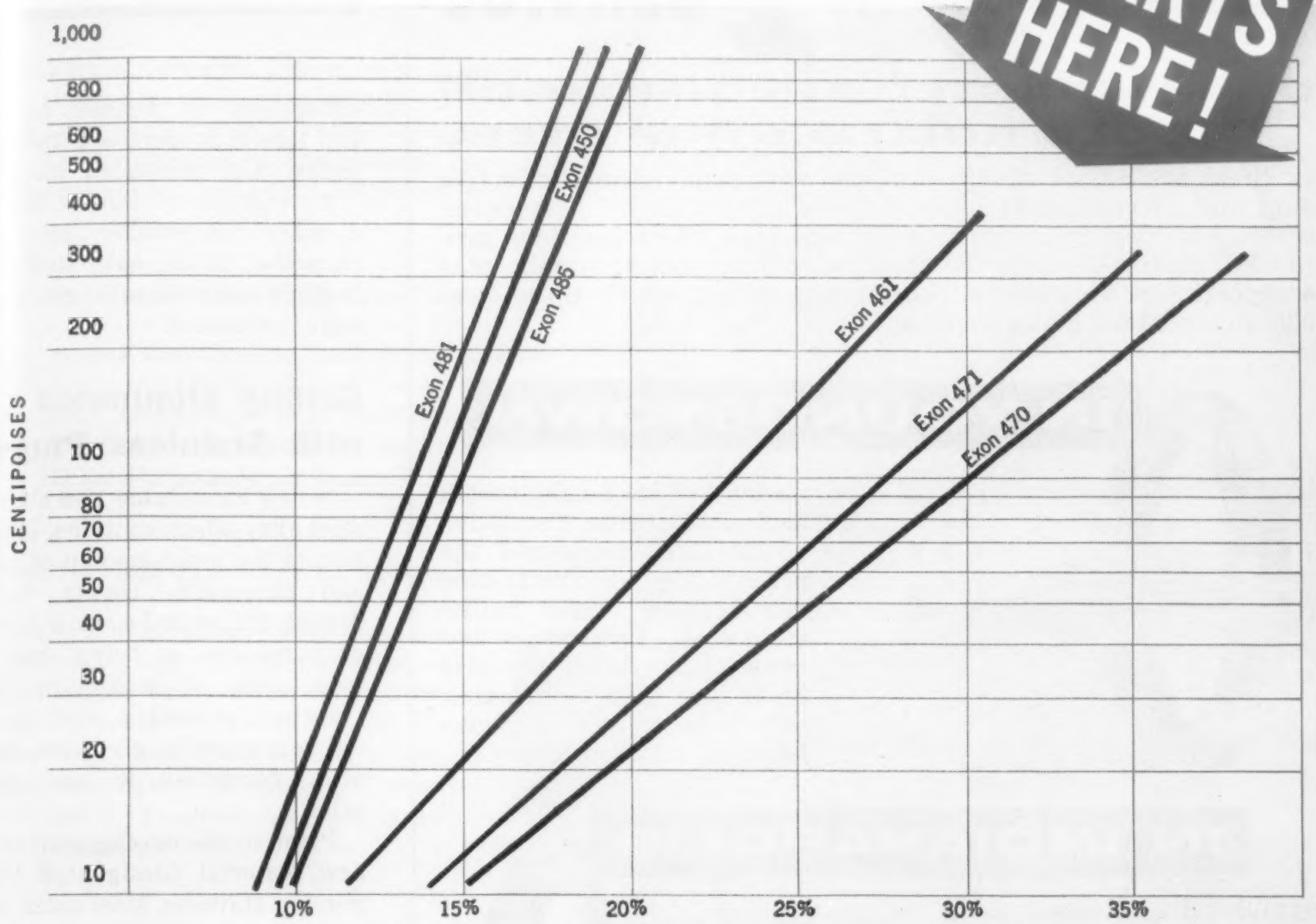


EXON CHARTS SOLUBILITIES to help you choose the resin with properties Pin-Pointed to your special needs!

EXON 450 Ideal for strip coatings. Good solubility, tensile strength and durability.

EXON 461 A unique fluorine-containing resin combining high solubility, unusual chemical resistance, heat stability and weatherability.

EXON 470 Excellent adhesion to metals, alkyd and vinyl surfaces. Compatible with wide range of drying oils, alkyds, phenolics, melamines. High solubility in inexpensive solvents.

EXON 471 Excellent for weatherability and durability in a protective coating. Corrosion resistant. No measurable change after sunlamp exposure for 360 hours as 1 mil film.

EXON 481 Makes possible colorful, abrasion-proof, washable coatings that resist fading or cracking.

EXON 485 For superior strip coatings. Lower viscosity makes application easier and shelf-life better. Good clarity.

Firestone

EXON

RESINS

THE special nature of Exon resins — "Pin-Pointed Properties" to supply specific answers to special needs — is particularly desirable in the manufacture of coatings.

Because products and processes vary, Firestone Exon has engineered 6 solution resins to help you formulate a successful coating. Each resin differs in properties, such as the solubility factor charted above, to suit various applications.

One property in common: superior quality of performance with the resultant production speed and savings which have made Firestone Exon industry's No. 1 source of specifically engineered vinyl resins.

We suggest you keep this chart handy—to help you put your finger on the right resin for *you* — at a glance.

For complete information and technical service, call or write:

CHEMICAL SALES DIVISION

FIRESTONE PLASTICS COMPANY, DEPT. 73F,
POTTSTOWN, PA.
A DIVISION OF THE FIRESTONE TIRE & RUBBER CO.

CHEMICAL PROGRESS WEEK-APRIL 8-12

INDUSTRY'S MOST COMPLETE LINE OF VINYLS ENGINEERED TO YOUR SPECIFIC NEEDS

For more information, turn to Reader Service Card, Circle No. 376

differences in Brinell hardness and tensile properties between the leaded and nonleaded materials.

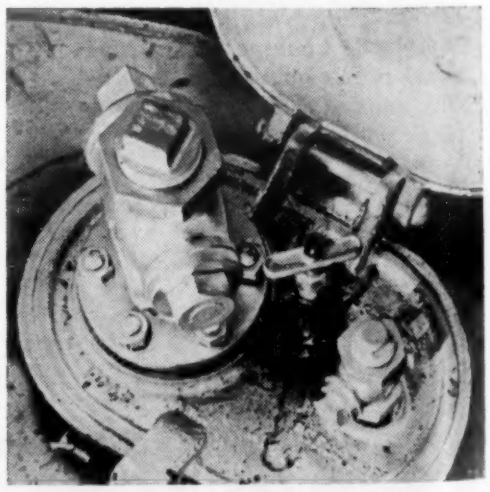
3. Addition of lead resulted in a somewhat smaller grain size than that of the base steel; both ferritic and austenitic grain sizes were influenced.

Galling Eliminated with Stainless Plugs

A new hardenable 18-8 stainless steel alloy which contains, in addition to the usual amount of nickel and chromium, copper, molybdenum, silicon and a small amount of beryllium, is being used for plug cocks on tank cars which transport chemicals such as tall oil, acrylonitrile, glycerine, acetic acid, formaldehyde and nitric acid.

Prior to the development of the new material (designated V2B), regular stainless steel cocks were used, but replacement was frequent because of galling. According to Cooper Alloy Corp., manufacturer of the plug cocks, this problem has been completely eliminated.

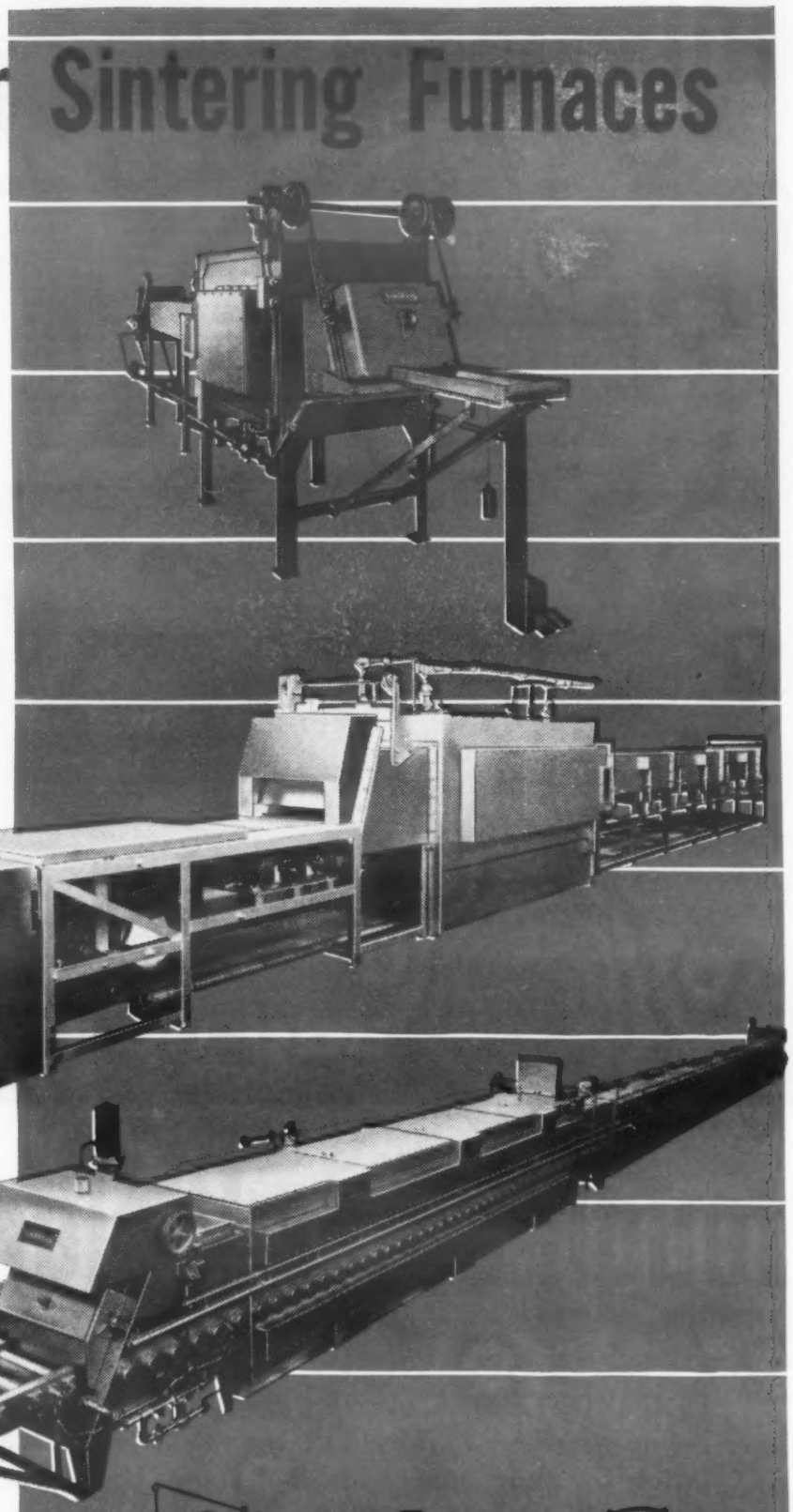
The new hardenable alloy is soft enough to be readily machined in the quench-annealed condition. It is normally water quenched from 2000 F, which puts the beryllium in solution and also



***New stainless alloy** plug cocks, installed on General American Transportation Corp. tank cars, are corrosion resistant and nongalling.*

Look to Lindberg for Sintering Furnaces

For sintering furnaces, just as in all types of industrial heating equipment, you can depend on Lindberg's ability to supply exactly the right equipment for your needs. Here are some typical Lindberg sintering furnaces:



This Hand Pusher Batch Type Furnace →

is used for small production lots and experimental sintering. It is an all-purpose unit for operation from 1300°F to 2500°F. Made in various sizes for sintering from 25 to 300 pounds per hour.

This Mesh Belt Continuous Type Furnace →

is a popular sintering furnace for small light parts in copper, bronze, brass or steel with a temperature range from 1300°F. to 2100°F. It can be used for low temperature silver brazing, bright annealing, as well as sintering of powder metals. Production ranges up to 500 pounds per hour.

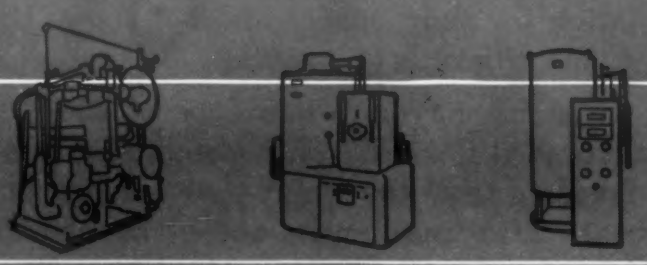
This Roller Hearth Continuous Type Furnace →

is especially designed to handle heavier loads up to 2200 pounds per hour. It has an effective temperature range from 1300°F. to 2100°F. It can be used for bright annealing, low temperature silver brazing as well as sintering of powder metals.

Atmosphere Generators →

To obtain the best work from any sintering furnaces, the proper atmosphere is required. The atmosphere generators described here provide the proper atmospheres recommended for use with Lindberg Sintering Furnaces.

If you have a sintering or brazing problem why not talk it over with Lindberg. Just get in touch with your nearest Lindberg Field Representative or write us direct.



1. The HYEX Generator produces atmosphere composed of approximately 4% carbon dioxide—18% hydrogen—12% carbon monoxide and 66% nitrogen.

2. The HYEN Generator produces a neutral atmosphere composed of approximately 21% carbon monoxide—40% hydrogen—38% nitrogen and 1% methane.

3. The HYAM Generator produces atmosphere composed of approximately 75% hydrogen and 25% nitrogen.

LINDBERG

ENGINEERING COMPANY

Los Angeles Plant: 11937 S. Regentview Ave., at Downey, Cal.

2451 W. HUBBARD ST., CHICAGO 12, ILL.

For more information, turn to Reader Service Card, Circle No. 581

What's new IN MATERIALS

keeps in solution carbides which are detrimental to corrosion resistance. After quenching, the metal is machined, hardened by holding at 925 F for 8 hr, and subsequently furnace cooled. No distortion or harmful carbide precipitation is produced in the relatively low temperature hardening operation.

Epoxy Potting Resin for Electrical Parts

A new epoxy resin designed especially as a potting and encapsulating compound for electrical parts is being marketed by Furane Plastics, Inc., 4516 Brazil St., Los Angeles 39.

When cured, Epocast 15-E has a nominal Shore D hardness of about 46, but it is possible to adjust the hardness by varying the proportions of the material with a hardener. Materials ranging from semisolids to soft rubberlike solids are possible from this combination of resin and hardener.

The new epoxy requires elevated temperatures to effect cure —generally 6-10 hr at 200 F, followed by 2 to 3 hr at 250 F.

The material may be used as a sealant for porous metal castings, as an impregnant for woven mats and gasketing fabrics, and as an integral casting for use as a shock absorber.

(more What's New on p 197)

TYPICAL PROPERTIES OF EPOCAST 15-E

Tensile Strength, psi	12,000
Elongation, %	70
Shore D Hardness	50
Density, gm/cu cm	1.16
Water Absorption (24 hr), %	0.2
Dissipation (power) Factor	
110 kc	0.039
1.0 mc	0.042
11.0 mc	0.053
Dielectric Constant	
110 kc	3.20
1.0 mc	3.10
11.0 mc	3.00

What's new IN MATERIALS

New Chemical Process for Descaling Titanium

Development of a process that efficiently descales titanium and its alloys without adversely affecting physical and chemical properties has been announced by Turco Products, Inc., Los Angeles.

Claimed to eliminate the disadvantages of descaling titanium by sand blasting, vapor blasting or immersion in molten salt baths, the new process requires only relatively low temperatures (270-280 F, as compared with 800-900 F in salt baths). Two immersion steps (one for scale conditioning and one for scale removing) and two rinsing steps are required.

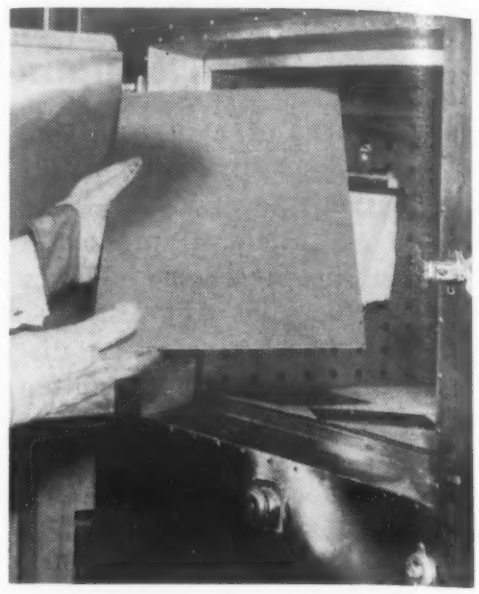
The process is said to give 100% chemical cleanliness without warping thin gage material. It does not cause salt entrapment on the metal's edges nor does it create fire hazards. The descaling bath is suitably inhibited to prevent hydrogen pickup and resultant embrittlement, and it keeps metal loss low (0.0001-0.0003 in. per side).

Hard Vinyl Coating for Metal Surfaces

An organosol formulation specifically designed as a metal coating has been developed by the Goodyear Tire & Rubber Co., Chemical Div., Plastics Dept., Akron 16, Ohio. Based on a vinyl dispersion resin, the coating is formulated with 35 parts of plasticizer per 100 parts of resin. The coating's low plasticizer content permits a harder coating with less tack and greater chemical resistance than is possible with comparable formulations having higher plasticization.

An adhesive plastisol primer is recommended for use with the coating to assure maximum adhesion to metal surfaces. Dilution with a mixture of mineral spirits

For more information, Circle No. 619



***Vinyl coated panel** is placed in oven to insure good adhesion and adequate surface hardness.*

and diisobutyl ketone is recommended for spray application.

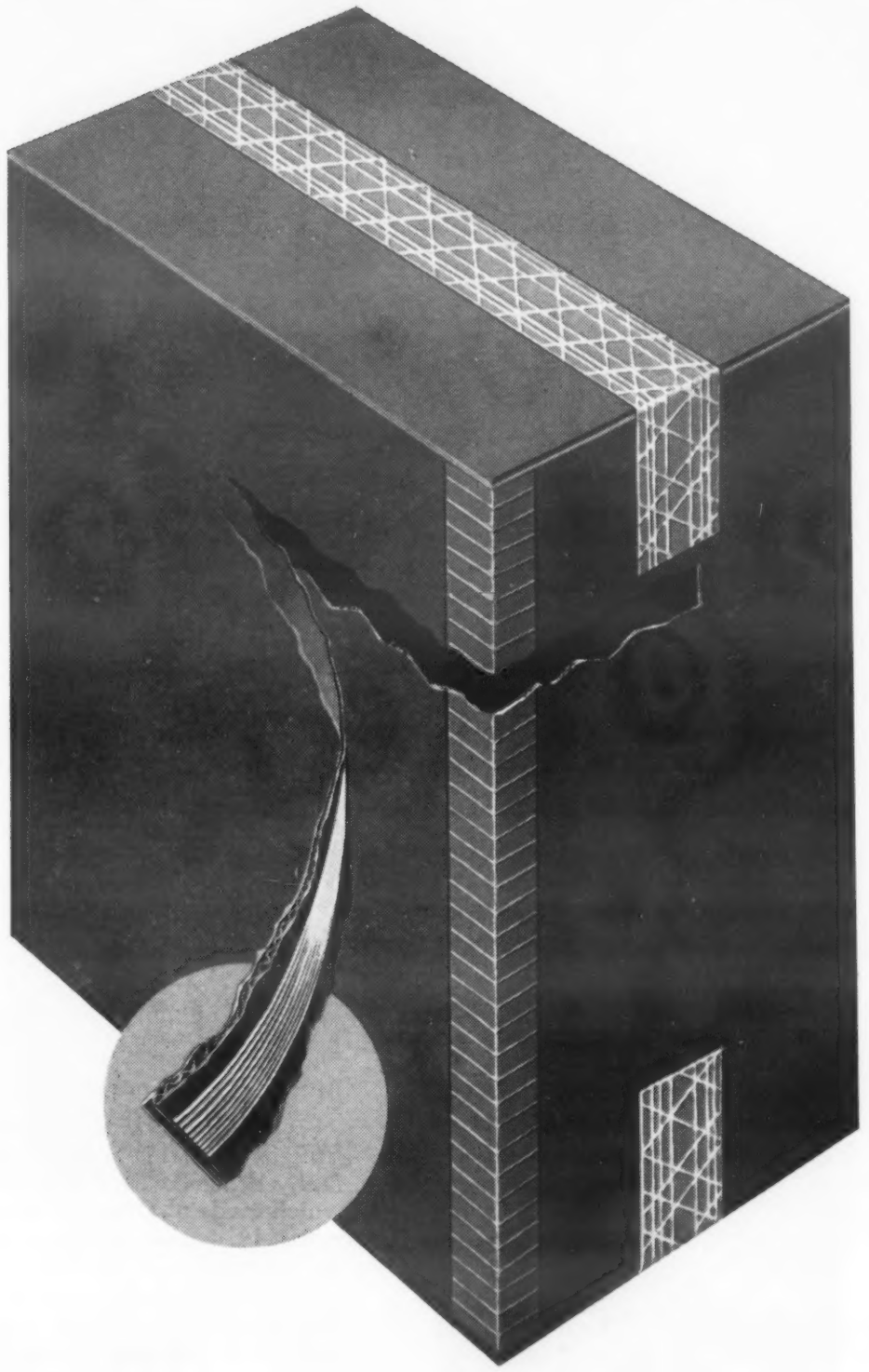
The organosol formulation was developed for such applications as coating of sheet stock, machine parts, tool handles, metal ducts, hoods and machine housings.

Styrene Compound Is Heat Resistant

Bakelite Co., Div. of Union Carbide & Carbon Corp., 260 Madison Ave., New York, has introduced an improved high impact, heat resistant polystyrene molding compound called TMD-5161. The compound is said to have a heat distortion temperature considerably higher than that of conventional high impact polystyrene molding compounds. It is designed primarily for electrical appliance housings because of its resistance to breakage and warpage by heat. The molding compound also has good electrical insulation values and is resistant to chemicals.

Characterized by uniformity, versatility, good flow, fast set-up and low bulk factor, the modified polystyrene is said to make possible intricate injection moldings on fast cycles. However, the material has slightly stiffer flow properties than usual, and the

RIP CARTONS OPEN FAST



AVISCO rayon high-strength yarns put cords of extra toughness in all kinds of tapes for quick protective sealing, slash-free opening.

Here's one way high-strength Avisco rayon helps save money and man-hours. Carton opening time is reduced to seconds, and damage to merchandise due to using sharp carton-opening tools is completely eliminated.

Tear tapes, corner stay tapes, and reinforced sealing tapes are just a few of thousands of ways Avisco rayon is used to add strength and tear resistance to packaging materials.

Here are several other examples of how the flexibility, shock resistance and utility of Avisco rayon reinforcements add strength and quality to products at an economical price:

Multi-wall bags for agricultural and chemical products
Case covers and liners · Wrappings for shipping and storing
Wrappings for sheet metals to protect highly finished surfaces
Backing for stucco · Temporary tarpaulins

Whatever your reinforcement requirements, American Viscose can supply fibers and yarns for every application. Our extensive technical facilities and experience are geared to help solve every conceivable design and production problem. Just tell us about your needs on the coupon, and send it in. You'll hear from us immediately.

AVISCO® RAYON

American Viscose Corporation, 350 Fifth Avenue, New York 1, New York

Name _____

Name of company _____

Address _____

Reinforcement requirements _____

For more information, turn to Reader Service Card, Circle No. 532

What's new IN MATERIALS

PROPERTIES OF TMD-5161

Specific Gravity	1.04
Heat Distortion Temp (264 psi), F	
⅛-in. Bar	189
¼-in. Bar	192
½-in. Bar	198
Water Absorption (24 hr immersion), %	0.140
Bulk Factor	1.72
Molding Shrinkage, in./in.	0.004
MECHANICAL PROPERTIES	
Rockwell L Hardness	78
Izod Impact Strength, ft-lb/in. notch	2.6
⅛-in. Bar	2.6
¼-in. Bar	1.1
Compressive Yield Stress (½-in. bar) psi	10,300
Tensile Strength (⅛-in. bar), psi	6700
Elongation in Tension, %	5
Mod of Elast in Tension, psi	3.5×10^5
Flexural Strength (¼-in. bar), psi	9200
ELECTRICAL PROPERTIES	
Dielectric Strength (short time), v/mil	460
Volume Resistivity, ohm-cm	10^{14}
Dielectric Constant (60 cycles)	2.60
Dissipation Factor (60 cycles)	0.002

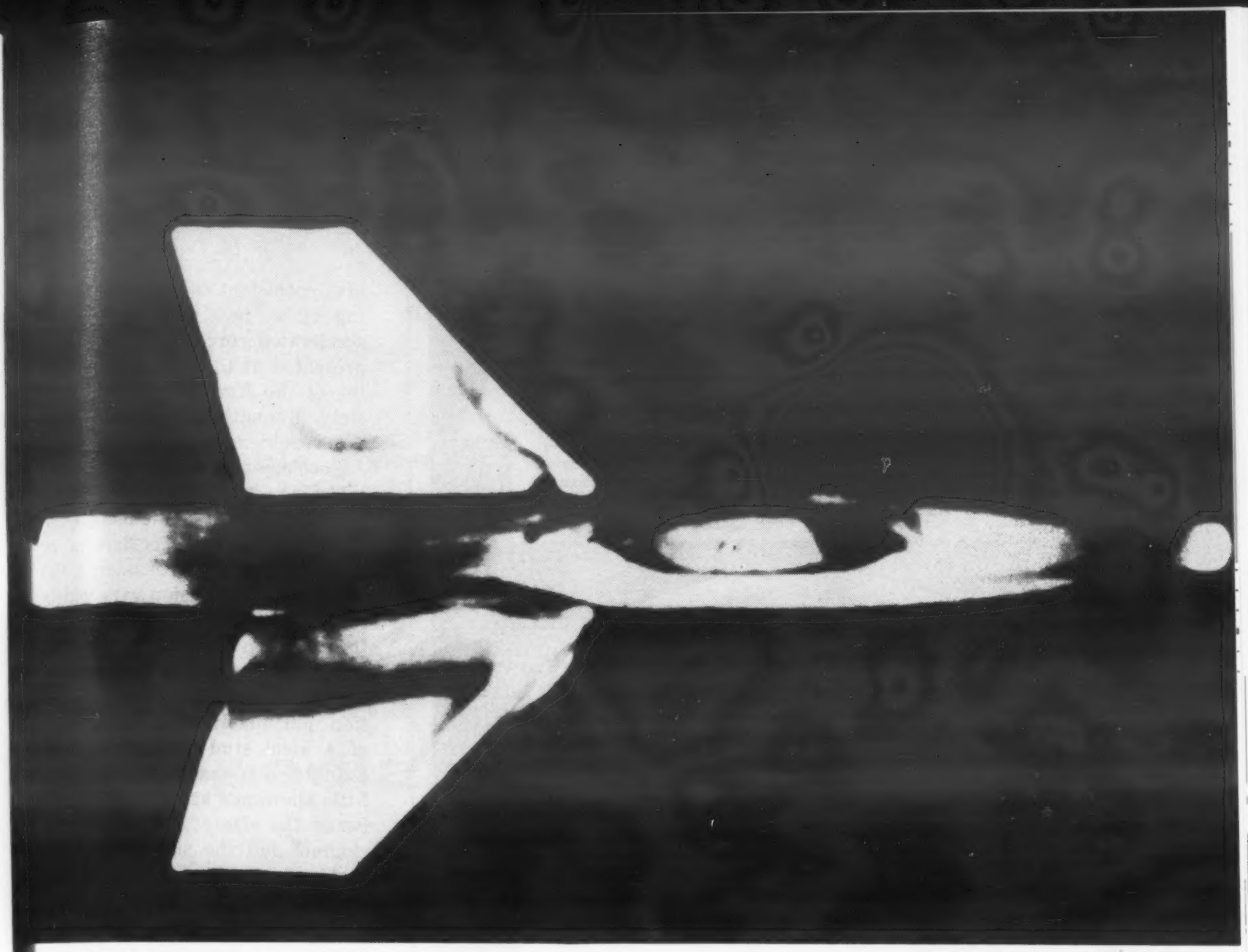
producer recommends a preheat period of 1 hr at 174 F to ensure faster set-up and better quality in the finished product.

According to the producer, the compound is easily molded to provide parts with good mechanical strength and shock resistance, high gloss and good appearance. It is available in a range of colors and is supplied in cylindrical pellets about 0.1 in. in diameter and length.

The material is recommended for such applications as radio cabinets, photographic equipment, electric fan housings, vacuum cleaner parts and air conditioning grilles.

Joining Aluminum to Other Metals

Advanced materials and methods now make it feasible to join aluminum to dissimilar metals without serious limitations. However, some problems are still encountered. The four major factors that must be taken into account



thermal thicket

The thermal barrier which now limits the speed of ultra high speed aircraft can be cracked. Needed: Structural components of elevated temperature alloys. Problems: Finding the right alloys; making them easy to forge and machine with regular production-line tools; maintaining uniformity of physical properties in production lots.

Right now, Carpenter is producing elevated temperature alloys which set new standards for consistent ability to meet tough aircraft specifications, high quality, improved forgeability and machinability. Engine builders find them ideal for many critical parts. Forge shops can work them to closer tolerances, get better finishes that require far less than usual machining. Work goes faster. Rejects are fewer.

You can get the full story of these alloys — their application, fabrication and engineering properties — in the new booklet, "Carpenter Alloys for Elevated Temperature Service". Get your personal copy by writing on your Company letterhead. The Carpenter Steel Company, 135 W. Bern Street, Reading, Pa.

Carpenter STEEL

Improved alloys for elevated temperature service

For more information, turn to Reader Service Card, Circle No. 365

What's new IN MATERIALS

are: coefficient of expansion, heating cycle, heat conductivity and accelerated corrosion. In a paper presented at the annual fall meeting of the American Welding Society, Kenneth V. Lutz discussed these problems and their remedies.

Coefficient of expansion—When soldering, and therefore raising the temperature of the metals, the difference in the coefficients of expansion must be considered. Coefficients of expansion vary widely for different metals. For example, the coefficient (per °F) for iron is 0.66×10^{-5}, compared to 1.33×10^{-5} for aluminum. In a production job involving the soldering of a steel stud to an aluminum channel, it was found that so little allowance had been made between the size of the hole in the channel and the size of the stud that when the assembly was heated to soldering temperature there was, in effect, a shrunk fit between the assembled parts. The solder was not thin-flowing enough to penetrate. The solution to this problem was entirely mechanical: the hole was made slightly larger.

Heating cycle—Fluxes are carefully compounded for special solders. This does not mean that only one flux can be used with only one solder. However, it is extremely important that the active point of the flux correspond to the flow point of the rod. Also, the component chemicals of the flux are balanced for maximum wetting action and minimum injurious fumes. If heat is maintained too long or too slowly built up, the active ingredients evaporate or burn out. This makes the flux ineffective for its purpose and this is sometimes worse than not having any flux at all.

In fabricating aluminum with stainless steel, solder No. 430 is specified. It is a strong solder, producing joints that can withstand a pull of 10,000-28,000 psi depending upon the type of joint. Flux No. 37 is specified for this solder. It is a nonflame flux and

What's new IN MATERIALS

is applied with indirect methods of heating. Therefore, the combination may not be used under circumstances where the parts are prefluxed, assembled and brought slowly up to the soldering temperature.

A typical problem involved a furnace application using this 430-37 combination to join aluminum to stainless steel. The belt carrying the prefluxed assembly through the furnace was so slow that all the active ingredients of the flux were gone before the preplaced solder was melted. The solution involved nothing more than speeding up the belt and raising the temperature of the furnace so that all elements of the soldering operation reached the required temperature at the same time.

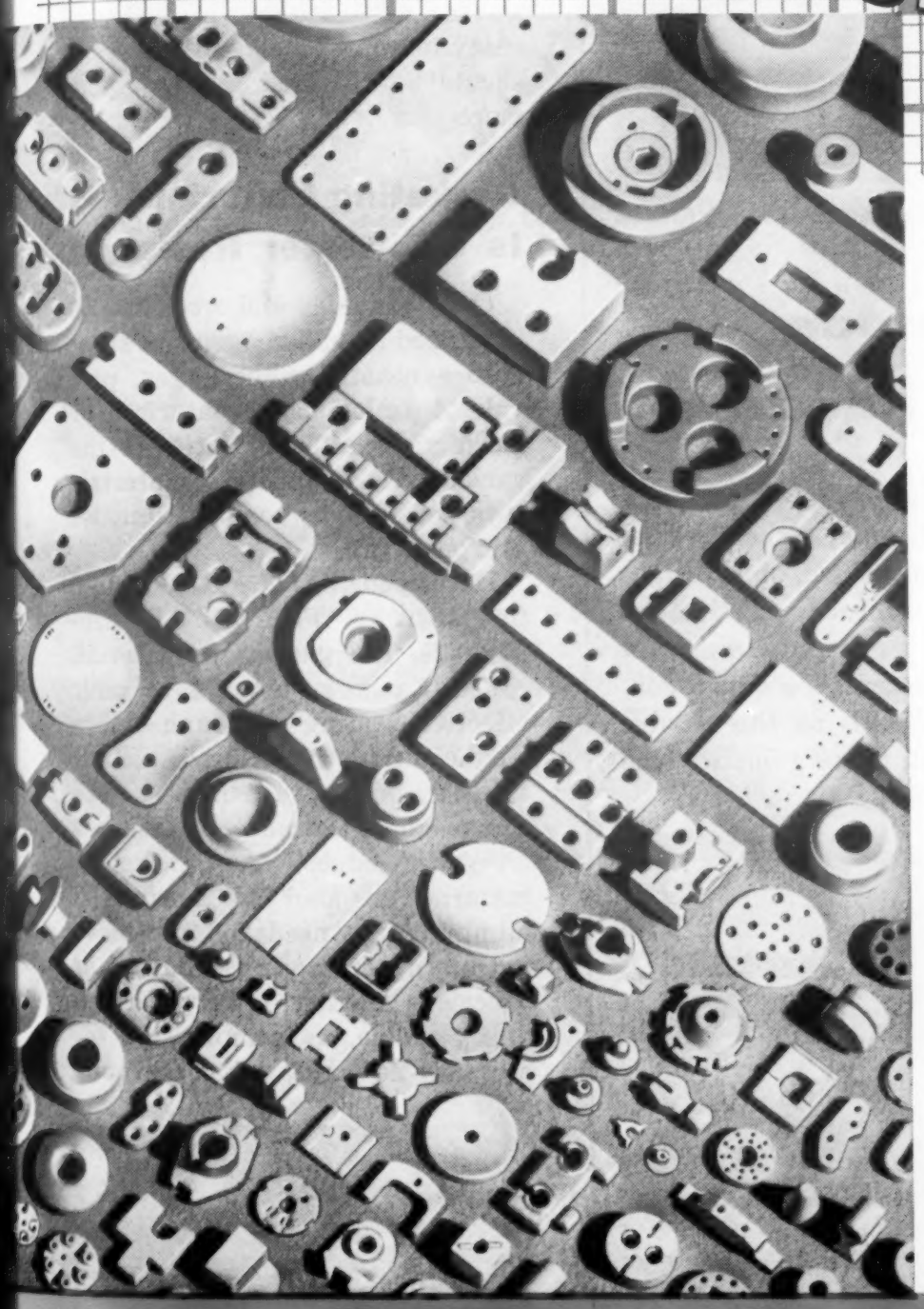
Heat conductivity—Where heat conductivity problems are encountered in welding, brazing or soldering aluminum to other metals of approximately the same size, it is advisable to play the heat on the part that is the best heat conductor. On differently sized parts, the heat should be played on the largest part. When the problem is complicated by a second soldering operation, the approach is considerably different because the second soldering may melt the first. For every job there are a number of different solders available. The logical solution, therefore, is to select a high temperature solder for the first operation and the lowest possible for the second.

Accelerated corrosion — Flux residue causes accelerated corrosion. Although after-soldering cleaning involves a relatively simple operation of washing with hot water, there are times when this is not practical, e.g., in underground installations of aluminum cable where the cable is joined to copper lugs.

In applications where flux would be detrimental because it

Improves your product. Lowers your costs...

AlSiMag® die pressed ceramics



If you need a strong, low cost component . . . custom made for your application . . . with superior electrical characteristics . . . great thermal shock resistance . . . produced to close dimensional tolerances . . . available in volume . . . it will pay you to investigate the "plus" values of AlSiMag pressed ceramics.

Most complete choice of special characteristic materials in the industry, including new and rugged AlSiMag Alumina "super ceramics." Wide latitude in design. Strict Quality Control. Dependable uniformity. Fast deliveries. Batteries of high speed presses. Complete equipment for the most efficient and economical production of parts to specification in any quantity. Ample facilities for volume raw material preparation, firing and machining.

Prototype service available. Check performance under actual operating conditions **before** placing orders for tooling, quantity lots.

Send sketch with detailed specifications for prices and suggestions from our highly specialized Engineering Department on material and design. No obligation.

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55TH YEAR OF CERAMIC LEADERSHIP

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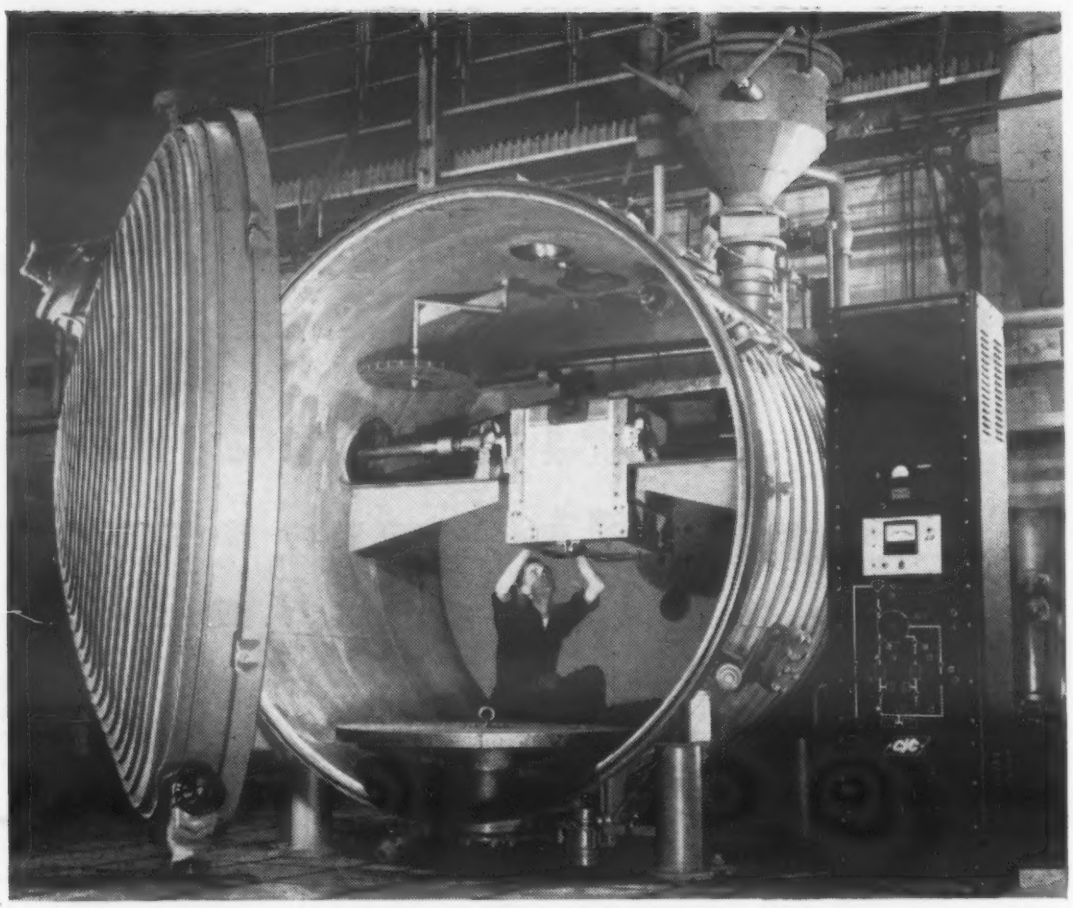
For more information, turn to Reader Service Card, Circle No. 490



CEC's new 300 to 1000 pound vacuum induction melting furnace.

Get a vacuum furnace that *grows* with your needs

Save costly alterations, or the purchase of another furnace, when your requirements change. Make sure you get these features:

Flexible capacity. Expand the furnace's basic 300-pound capacity to as much as 1000 pounds simply by changing the crucible-coil.

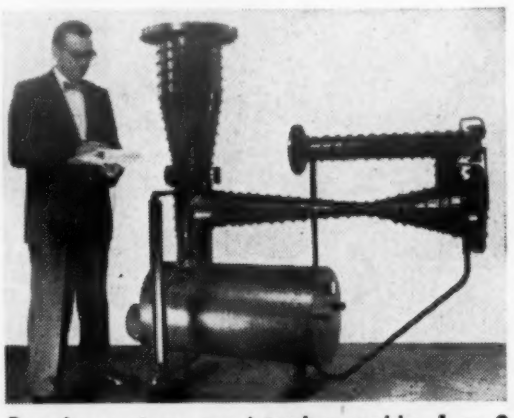
Add an interlock valve to the charging assembly and process as much as 3000 pounds of metal without breaking vacuum.

Flexible pumping system. Add a pump, or switch to larger pumps, and double, triple, even quadruple the pumping system's speed and capacity.

Flexible casting. Cast a single large mold or many small ones; add such accessories as arc hot-topping equipment in ports already provided.

Flexible accessories. All necessary accommodations for a sampler, immersion thermocouple, optical sight tube, vacuum throttling valve, interlock valve for charge addition, or any other accessories you want to add.

For more details on this flexible CEC induction melting furnace send for Bulletin 4-35.



Pumping systems are interchangeable: 1 or 2 KS-2000 (shown here), 1 or 2 KS-4000, or one KS-16,000.

Consolidated Electrodynamics
Rochester Division, Rochester 3, N. Y.
formerly Consolidated Vacuum

OFFICES IN PRINCIPAL CITIES THROUGHOUT THE WORLD

For more information, turn to Reader Service Card, Circle No. 405

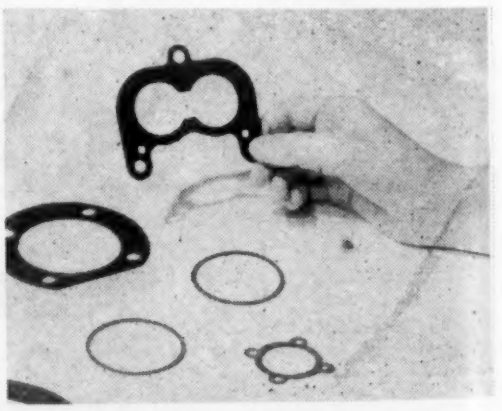
What's new IN MATERIALS

is difficult to remove residue, it is often preferable to use a mechanical tinning method. This is easily accomplished by heating the base metal to a point where the solder to be used melts when touched to the base metal. The temperature is maintained and the solder scrubbed into the pores with a clean wire brush. If the solder does not stick to the base metal, leaving a surface that is clean and shiny in appearance, the operation should be repeated using a little more heat.

Gasketing Material Is Oil, Water Resistant

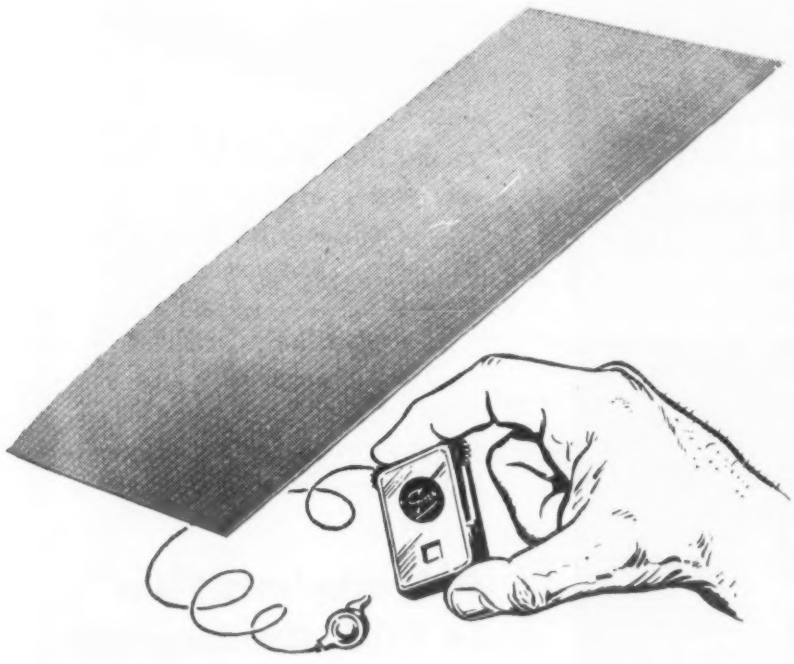
Cork granules and wood fibers, combined in an homogeneous sheet with synthetic rubber latex, provide a tailor-made material for gaskets. By altering ratios of the various components, materials with different compressibilities are possible.

Developed by F. D. Farnum Co., 4940 W. Flournoy St., Chicago 44, the gasketing material, called Kaokork, is said to offer effective seating of rough flange surfaces and to permit seals for thin-sectioned housings with sharp edges. Because it cushions irregular edges, the gasketing material is said to frequently eliminate the need for expensive machining of castings. Design of junctions having fewer bolts is also possible, as compression effectively seals gaps that normally

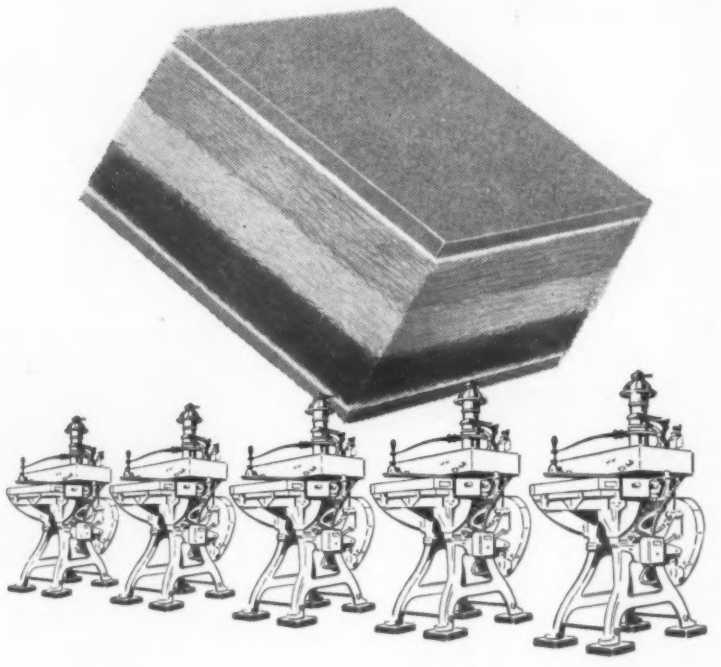


Gaskets *made of wood, cork and rubber can be tailor-made.*

A paper-thin battery separator felt for hearing aids



. . . or Vibra-Mount felts to cut machine vibration*



Put the MAGIC *of American Felts to work for you*

New things are happening most every day at American Felt Company. Exciting things you never dreamed could happen with felts. The battery separator, for example, is made from one of our Feutron** Felts, a combination of synthetic fibers that makes this separator more resistant, longer lasting than the usual material employed.

On the other hand the unusual properties of wool fibers as combined in American's Vibra-Mount Felt eliminate as much as 85% of a machine's vibration, no bolts are needed to fasten machines to concrete or wood floors, "walking" of machines is prevented.

These are just two of the many uses for the felt wonders constantly being produced through the ingenuity of American's Research and Engineering Staff. Use your imagination and many more uses will come to mind.

For the first things in felt it will pay you to call American first. Design with American Felts.

*Trademark Reg. **Trademark Reg.

American Felt Company
TRADE MARK

GENERAL OFFICES: 24 GLENVILLE RD., GLENVILLE, CONN.

SALES OFFICES: New York, Boston, Chicago, Detroit, Cleveland, Rochester, Philadelphia, St. Louis, Atlanta, Greenville, S. C., Dallas, Boynton Beach, Fla., San Francisco, Los Angeles, Portland, San Diego, Seattle, Montreal.—PLANTS: Glenville, Conn.; Franklin, Mass.; Newburgh, N. Y.; Detroit, Mich.; Westerly, R. I.—ENGINEERING AND RESEARCH LABORATORIES: Glenville, Conn.

For more information, turn to Reader Service Card, Circle No. 531

What's new IN MATERIALS

would require additional fastenings.

The combination of cork granules, wood fibers and nitrile rubber latex is said to provide a gasketing material having good oil, water and solvent resistance, yet maintaining maximum compressive properties and high strength.

It is available in sheet stock up to 100 in. in width and ⅛ in. in thickness. The company is equipped to prepare dies and cut gaskets in production quantities.

Polyethylene Film Is Stiff, Greaseproof

A moderately high density polyethylene resin, recently introduced by Spencer Chemical Co., 610 Dwight Bldg., Kansas City 5, Mo., is said to make possible a film that is two-and-a-half times stiffer, less than half as permeable to gases and water vapor, and at least three times more greaseproof than conventional polyethylene films.

Designated Poly-Eth Hi-D 2504, the resin has a specific gravity of 0.938 and is produced by Spencer's modified high pressure process (see M&M, Oct '56, p 145). It is available in truckload quantities at a price of 47¢ per lb.

The resin is claimed to make possible a film with a high degree of clarity and good gloss, and

PROPERTIES OF HI-D 2504

Specific Gravity	0.938
Melt Index, gm/10 min	1
Vicat Softening Point, F	235
Ultimate Tensile Strength, psi	
Machine Direction	3050
Transverse Direction	3225
Yield Tensile Strength, psi	
Machine Direction	1900
Transverse Direction	2000
Ultimate Elongation, %	
Machine Direction	455
Transverse Direction	600
Tear Strength, gm/mil	
Machine Direction	93
Transverse Direction	97
Coefficient of Friction	0.6

greater yield strength than conventional film. Impact strength of the new film is somewhat less than that of conventional film. The film withstands pasteurization and boiling, and it can be heat sealed and printed. Its slip characteristics are said to be superior to those of unlubricated conventional polyethylene films.

The resin can be processed on conventional film-making equipment but requires temperatures roughly 25 °F higher than standard film materials. Both flat and tubular film have been made with thicknesses of less than 1 mil.

Three New Finishes

Recent developments in finishes include white and light colored flow coating enamels and a 22-carat gold ceramic finish.

1. Hammered-effect lacquer

A one coat, fast drying, hammered-effect lacquer enamel called Dulac One-Coat Hammertone has been developed by Maas & Waldstein Co., 2121 McCarter Highway, Newark 4, N. J. It is said to have excellent adhesion to most metals and can be easily applied with a standard spray gun. It is available in a wide range of metallic colors.

2. Flow-coat enamels

Interchemical Corp., Finishes Div., 224 McWhorter St., Newark 5, N. J., has recently announced a line of white and light colored flow coating enamels and primers. The enamels can be used over primers or as one coat finishes on appliances.

Known as IC Ultraflo primers and enamels, the paints are said to flow quickly and completely in the first seconds after application, then undergo an increase in viscosity that causes them to "stay put" around sharp edges and holes. Because of their inherent stability and controlled evaporation rate, the enamels are claimed to change less and require

◀ For more information, Circle No. 491

What's new IN MATERIALS

less control than conventional enamels.

3. Gold ceramic finish

A 22-carat gold ceramic finish, said to be competitive in price with other commercial finishes, has been developed by Bettinger Corp., Gore St., Waltham, Mass. The paint is said to be permanent, since gold is fused into the surface of the ceramic material.

Low cost is possible because only a thin application of gold is needed; the ceramic material makes the finish more stable than the gold itself. The gold finish is presently being used on gasoline pumps.

Silicone-Insulated Unit Has Run 14 Years

In a series of tests to determine the minimum and maximum life of silicone insulation in electric motors, a much abused, silicone insulated motor finally broke down after running 60,173 hr. Minimum life was decided some time ago when the high temperatures either oxidized the copper or warped the rotor, of similar motors causing failure while the insulation was still effective.

Started in October, 1943 as a joint project of Dow Corning and Westinghouse, the test used eight

***Lamination slippage** broke down this silicone-insulated, 10-hp motor after it had run 60,000 hr at 464 F.*

For more information, Circle No. 492 ➤

10-hp, 1190-rpm, 3-phase induction motors. Six motors were insulated with silicone-bonded and impregnated materials and two were Class B insulated.

All eight motors were generator loaded to produce average copper temperatures ranging from 392 to 590 F. Operating time at temperature was divided into "heats" each a 25th of the motor's estimated maximum life. The heats were alternated with 24-hr conditioning periods at 100% relative humidity. Minimum life was defined as the point at which crazing appeared on the varnish surface, and maximum life was defined as actual insulation failure.

Both Class B units failed and caught fire, as expected. One Class B unit ran 3760 hr at a temperature of 392 F before failure; the other ran 1056 hr at 527 F before failure.

Five silicone insulated motors failed at various times and temperatures. One motor ran 5131 hr at 590 F before breaking down. Another motor, still operating in January 1957, has so far run a total of 61,500 hr at 464 F.

The test revealed that the "failure mechanism" of silicone insulation was far different than that of organic materials. After the varnish had crazed, silicone insulation still maintained a good bond, holding the other components in place. It never evolved into a conductor because of its silica backbone, and it stayed hydrophobic.

Lead and Polyethylene Make an Atomic Shield

A lead-filled thermoplastic compound containing 95% lead and 5% polyethylene by weight is available from Telectro Industries Corp., 35-18 37th St., Long Island City 1, N. Y. Called Leadolene, the material melts at a temperature of 220 F. It can be used for

Facts to consider when you're buying

Chromate Conversion Coatings

for Corrosion Protection, Paint Base, Decorative Finishing

WHAT IS IRIDITE®?

Briefly, Iridite is the tradename for a specialized line of chromate conversion finishes. They are generally applied by dip, some by brush or spray, at or near room temperature, with automatic equipment or manual finishing facilities. During application, a chemical reaction occurs that produces a thin (.00002″ max.) gel-like, complex chromate film of a nonporous nature on the surface of the metal. This film is an integral part of the metal itself, thus cannot flake, chip or peel. No special equipment, exhaust systems or specially trained personnel are required.

If your company is manufacturing or buying parts or complete assemblies made from or plated with any of the more common non-ferrous metals—zinc, cadmium, aluminum, magnesium, silver, copper, brass or bronze—you've probably already run up against the question of finishing these surfaces with a chromate conversion coating. These coatings are used to protect against corrosion, or to provide a base for paint or to provide a decorative finish for sales appeal or shelf life. Since chromate conversion coatings represent a relatively new means of obtaining these finishes, this digest of facts to consider may be of value to you.

1. THE COATINGS THEMSELVES. There are many brands on the market. All are similar in many ways. Each, of course, offers its own specific advantages and these may relate to operating techniques, performance under actual use conditions, cost, availability, etc. Naturally, you'll want to choose a coating that is widely known and accepted under both military and civilian specifications.

2. THE COMPANY BEHIND THE PRODUCT. Is it a reliable, established organization? Does it offer experienced technical service, both from the field-engineering organization as well as the home office and laboratories? The man who sells and services your installation should be thoroughly familiar with not only chromate conversion coatings and their applications, but also with the characteristics and performance of related finishing operations such as precleaning, electroplating, painting, etc. This is most important since all steps of the finishing cycle must be functioning properly for the satisfactory performance of the ultimate finish produced.

3. AVAILABILITY OF THE PRODUCT. Ideally, of course, the material should be readily available to you from nearby warehouses to avoid time loss in long distance shipping and to provide emergency service, should the need arise.

4. COST. Naturally, the initial price of the material is important to you. However, just as you consider ultimate cost when you are buying mechanical equipment, ultimate cost must be considered for these finishing chemicals. So, it will pay you to investigate consumption costs, labor costs and the other factors which go into the determination of ultimate cost. Further, cost alone gives no indication of product performance, so careful attention must be given to the purpose the finish must serve and the value that finish will add to your product.

5. FACILITIES FOR RESEARCH AND DEVELOPMENT. Perhaps the existing types of chromate conversion coatings do not include a compound that will accomplish exactly what you wish. Then, it is important to deal with a supplier who has adequate research and development facilities available to work with you to produce a material to meet your needs. Naturally, such a project is seldom completed overnight. But, with complete cooperation and confidence from both you and your supplier, chances are a satisfactory program can be completed.

These are the concepts of sales and service on which we, Allied Research Products, Incorporated, have developed and marketed the line of Iridite chromate conversion coatings . . . superior product performance, complete sales and technical service, easy product availability, economical cost, extensive research and development facilities. No doubt you are familiar with our line and have seen this trademark—

IRIDITE®

—in our advertising, technical literature or on shipping containers in your plant. Remember this trademark when you're buying or investigating chromate conversion coatings for your company. It's your assurance of quality, economical products from a reliable and established company, skilled sales and technical service from both our home office and a national network of representatives, immediate availability from warehouses in strategic industrial areas and our willingness to work with you to develop new finishes to meet your needs, should the present line fall short.

For complete information on Iridite chromate conversion coatings, write today for your free copy of our technical data file. Or, for immediate advice, call in your Allied Field Engineer. He's listed under "Plating Supplies" in your classified telephone book.

ALLIED RESEARCH PRODUCTS
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Manufacturers of Iridite chromate conversion coatings for corrosion resistance, paint systems, final finishing of non-ferrous metals; ARP Plating Brightener & Chemicals. West Coast Licensee—L. H. Butcher Co.

For more information, turn to Reader Service Card, Circle No. 436

simple castings. Cast pieces can be remelted and cast again with no loss of material due to oxidation.

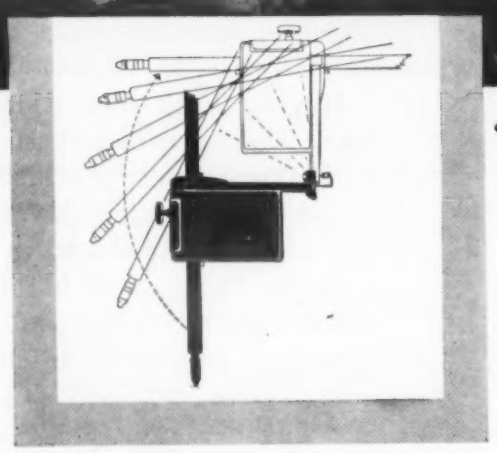
The high lead content is helpful in shielding against beta and gamma rays, and the hydrogen in the polyethylene aids in shielding against neutrons. Hydrogen can be increased by changing the ratio of polyethylene to lead. Specific gravity of the final compound can be controlled by changing the ratio of lead and polyethylene in accordance with specific requirements.

The material is not soluble in most solvents at room temperatures, but at temperatures above 180 F it is readily soluble in either aliphatic or aromatic hydrocarbons. It is soluble to a small degree in hot ester type solvents and high molecular weight alcohols. It cannot be joined by glue or adhesives, but only by melting the edges together or by pouring the liquid lead-polyethylene material into joints or between interlocking members.

Tensile Ductility of Swaged Chromium

D. J. Maykuth and R. I. Jaffee, of Battelle Memorial Institute, have compared the properties of iodide chromium and chromium-base alloys in bar form with those previously reported for strip. They found that swaged and recrystallized (nonfibrous structure) chromium-base alloys with 50% iron or nickel, tested as bar stock, have excellent tensile ductility; but ductility becomes low at 40% iron and is lost at 40% nickel. The investigators also determined that swaged chromium must have a fibrous structure for optimum tensile ductility.

The modulus of elasticity was found to be 42 million psi at room temperature, decreasing to 36 million at 1472 F. This particular



New Airco Model C Heliweld automatic head operates at all angles from horizontal to vertical.

Airco introduces New Automatic Heliweld Head for long-run production welding

The Model C Heliweld automatic head is specifically designed for long-run production on regular or irregular contours — aluminum tubing, motor stators, irregularly-shaped pressure vessels. Its prime advantage is that once the required arc length is set the head will automatically maintain this distance by moving the holder up or down to follow the contours of the work piece. Other benefits are:

- **Versatility** — unit provides good arc voltage control using either argon or helium shielding gases or mixture of both.
- **Adaptability** —the head can be operated at all angles from the horizontal to the vertical (normal) position. The maximum raise-lower distance of the electrode holder is a full 16″.
- **Flexibility** — the assembly can be used for AC or DC welding, with or without filler wire. Electrode diameters range from .020 to ⅛″.

The use of the new automatic head will be required where welds of consistent dimensions and quality are important and where good weld appearance is necessary or where welding specifications are very high for the electrical, aircraft, and refrigeration industries. Complete information covering the wide range of applications and detailed specification data is available. Write Airco at the first opportunity.

range was studied because it was felt that there was a lack of accurate data over the temperature range of interest in gas turbines.

This information was originally presented at the 38th annual convention of the American Society for Metals.

Phenolic Laminate Punches Clean, Sharp

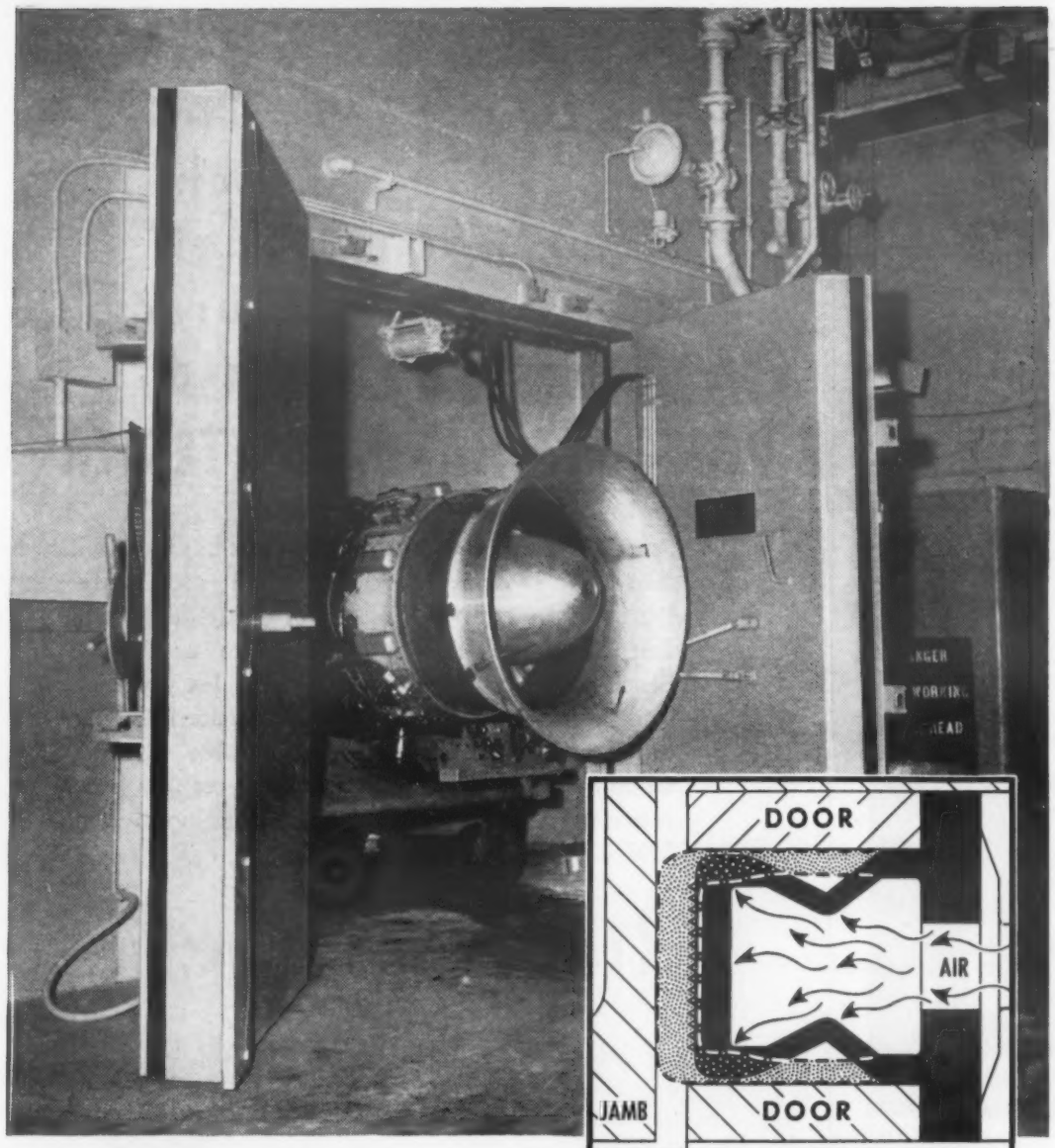
A paper-base phenolic laminate with good cold punching and cold shearing characteristics has been developed by Synthane Corp., Oaks, Pa. The new grade, called P-25, is said to eliminate the need for heating equipment and shrinkage allowances because it punches clean and sharp at room temperature.

Having high insulation resistance and low dielectric loss at high frequencies, the laminate is especially recommended for copper-clad laminates used in printed circuits. It is available in plain sheet form or copper-clad, in both semigloss and dull finishes.

(more What's New on p 218)

PROPERTIES OF P-25

PHYSICAL PROPERTIES	
Tensile Strength, psi	
Lengthwise	12,400
Crosswise	9500
Compressive Strength, psi	
Flatwise	25,000
Edgewise	—
Mod of Elasticity in Flexure, psi	
Lengthwise	1,000,000
Crosswise	700,000
Shear Strength, psi	11,000
Izod Notched Impact (edgewise), ft-lb/in.	0.30
Specific Gravity	1.30
Coef of Thermal Expansion, per °F	2×10^{-5}
Water Absorption (24 hr), %	
1/16 in.	1.00
1/8 in.	0.75
ELECTRICAL PROPERTIES	
Dielectric Strength (perp to lam, short time), v/mil	
1/16 in.	200
1/8 in.	150
Dissipation Factor (1 mc)	0.030
Dielectric Constant (1 mc)	4.6
Max Constant Operating Temp, F	250



Dotted area shows gasket inflated

Photo courtesy General Electric Co.

Pneumatic Rubber *Door Seal* Muffles Test Cell Noises

To more effectively suppress noise, General Electric jet engine test cells are equipped with a unique pneumatic rubber door seal. Mounted on door perimeter, this seal is designed to expand proportionally and insure a perfect seal over its entire sealing surface *including the corners*. Not only does this gasket dampen the noise but it permits more accurate testing through quieter working conditions.

Continental engineers developed this pneumatic gasket for this and similar applications. Compounded of special flex-resistant rubber, this versatile gasket can be operated with intermittent flexing cycle *or* as a continuous seal—can be adapted to various other types of doors—for *either* pressure or vacuum rooms.

The design of this gasket typifies the engineering skill offered by Continental. When you need "engineered rubber parts"—molded or extruded—enlist the service of specialists—consult Continental.

Engineering Catalog.

In addition to custom-made parts, Continental offers an extensive line of standard grommets, bushings, bumpers, rings and extruded shapes. Hundreds of these are shown in the No. 100 Engineering Catalog. Send for a copy or refer to it in Sweet's Catalog for Product Designers.

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For more information, turn to Reader Service Card, Circle No. 571

What's new IN MATERIALS

Creep Tester Holds Strain at Same Point

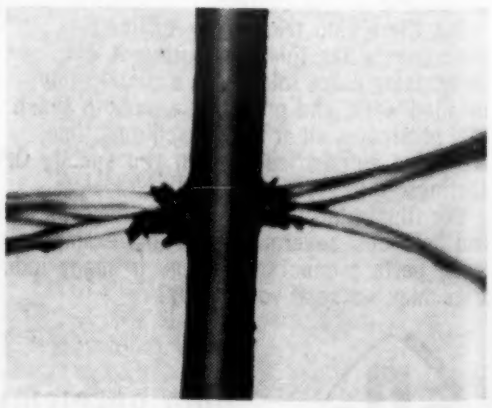
A new creep-strain tester that is said to automatically maintain a fixed extension of the specimen at elevated temperatures has been introduced by Tinius Olsen Testing Machine Co. Operating on a principle directly opposite to that of ordinary creep testers, the machine is started at a desired loading speed and load is applied to the specimen until the predetermined extension is attained. As the specimen tends to strain further, the amount of load is automatically reduced to maintain fixed extension.

A circular testing furnace, mounted between the crossheads of the tester, can be used for testing at any temperature up to 2000 F. A separate unit contains temperature controls and an automatic recorder.

Very Thin Copper Wire Used in Electric Watch

A copper wire one-fifth the thickness of a human hair, an 0.0056-oz permanent magnet made of a platinum alloy, and a gold plated power unit the size of a shirt button help power a new electric watch introduced by Hamilton Watch Co.

Chemical energy, stored in a tiny energizer, is converted into electrical power as it releases a



Copper wire, *0.0006 in. thick, is shown being strung through a hole bored in a human hair.*

Cleaning Specialists*

*[SPE'CIAL·IST—One who devotes himself to some special branch of activity.]

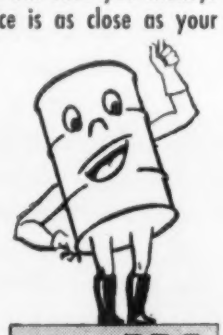
At Northwest our "special branch of activity" is solving your cleaning problems.

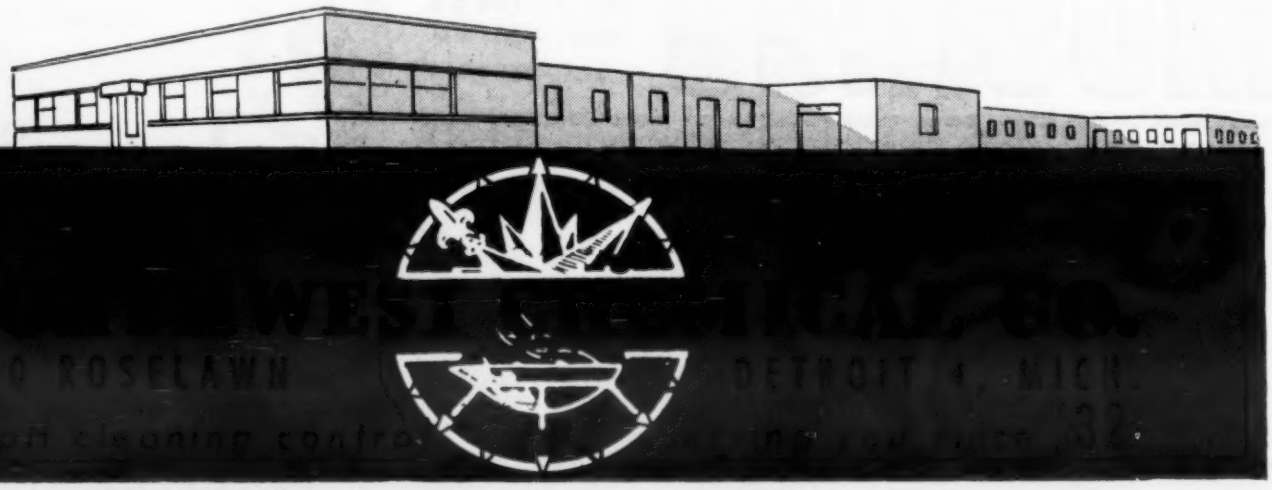
Behind your friendly, competent Northwest Sales Engineer stands a reputation for providing industry with low-cost, analytically-correct, job-adjusted chemical cleaners.

From Northwest's years of experience in formulating the RIGHT cleaner for your specific needs have come such developments as the LO-HI pH PROCESS—for cleaning prior to plating, painting, or vitreous enameling; ALKALUME PROCESS—for preparing aluminum and magnesium for finishing and spot welding; INTERLOX PROCESS—for phosphate coating; SPRA-LUBE—to control over-spray of "today's" paints in water wash paint booths; PAINT STRIPPERS—specific to your needs; SUPER-DRAW & FLUID FILM—for drawing metals.

Remember—YOUR COST PER FINISHED ARTICLE IS THE TRUE COST OF YOUR CLEANER.

Northwest's production-tested chemicals and "Right the first time" recommendations will save you money. Northwest Service is as close as your phone.





What's new IN MATERIALS

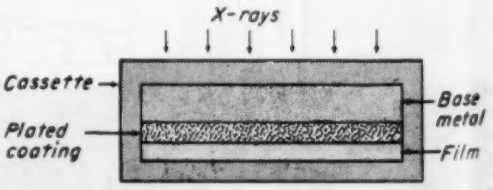
stream of electrons through a coil of fine copper wire fixed on a balance wheel. The electrical energy, through interaction with permanent magnetic fields, causes the balance wheel to oscillate, providing the mechanical energy that runs the watch.

The tiny energizer eliminates the use of a mainspring and is said to be able to run the watch for more than one year at an accuracy greater than 99.995%. The electric watch has about one-third fewer parts than present day automatic watches.

Radiation Detects Pores in Electroplates

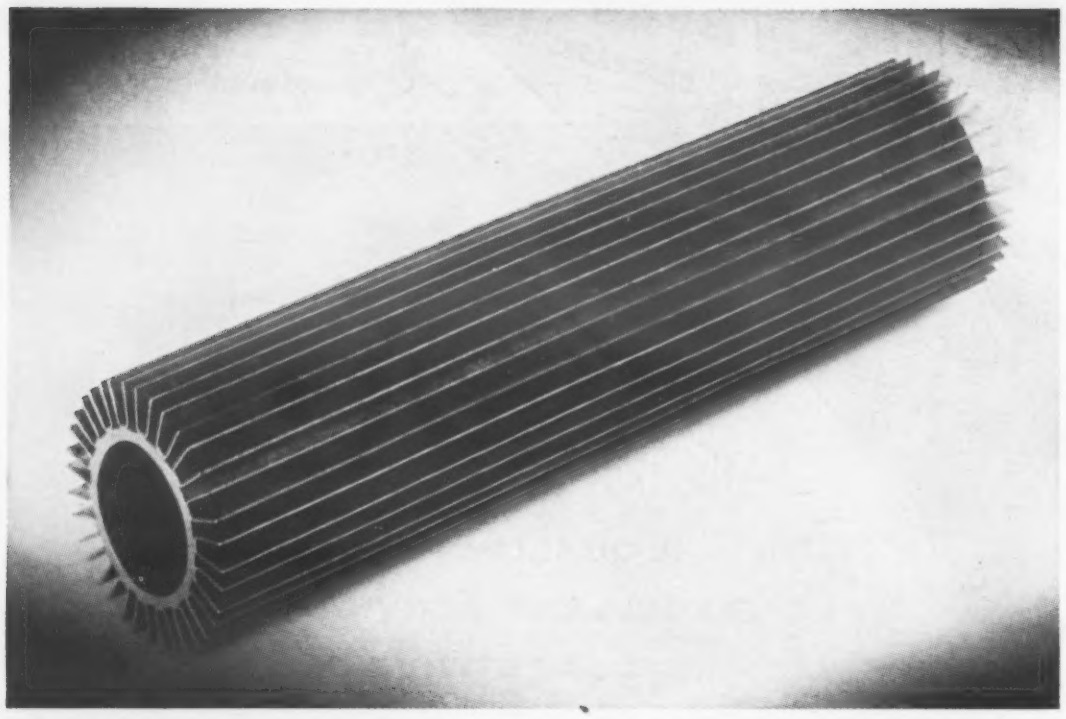
Until now it has been difficult to determine the location and size of pores and other flaws in industrially produced electroplated coatings. Recently, however, the National Bureau of Standards, in cooperation with the American Electroplaters' Society, has developed a nondestructive method for determining both the size and position of pores by exposing an electroplated specimen to radiation.

First step in the procedure, developed by F. Ogburn of the Bureau staff and Margaret Kilkert, AES research fellow at the Bureau, consists of placing a flat sheet of plated metal a few thousandths of an inch thick on a photographic film with the plated coating against the film emulsion. Thickness of the base metal is limited to a few thousandths of

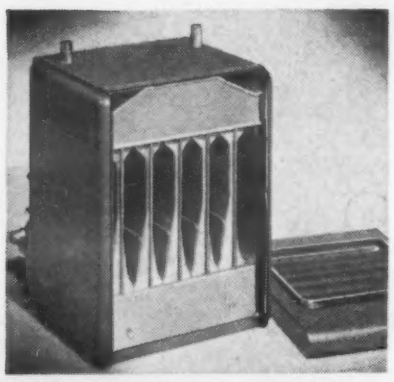


***Method** for investigating porosity of electroplated coatings. The coating is placed against the emulsion of the film (bottom) and the base metal side (top) is exposed to x-rays or radiation from a radioactive material.*

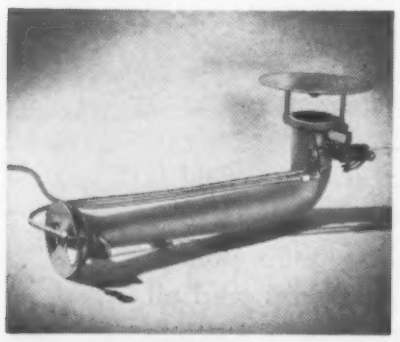
For more information, Circle No. 610



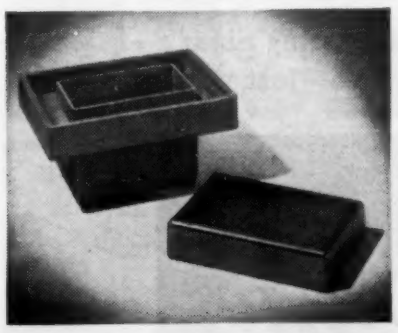
Heat exchanger used in evaporators and condensers will withstand 1600° F indefinitely.



Stainless Alloy Surface protects heat exchanger element in gas-fired unit heater which operates at approximately 1600° F.



Stainless Alloy Surfaced flame spreader replaces Stainless Steel spreader normally used in fuel burner nozzle at a 40% cost saving.



Heat treatment retorts operating up to 2600° F can be protected against heavy oxidation which reduces service life.

Heat Protection

Up to 2600° F.

Steels having a carbon content from 1008 to 1053 can now be given a *Stainless Alloy Surface* providing heat resistance equal to that afforded by Stainless Steels. A new, low-cost process — ASC Metal Diffusion — creates by atom interchange a chromium-rich surface that gives unlimited heat protection at 1600° F. and limited protection up to 2600° F.

Unlike coatings, platings and claddings, an ASC Stainless Alloy Surface becomes an integral part of the processed work. It will not chip, peel, craze or crack. The Process is applicable to all iron, steel, and ferrous alloys — and forming, welding, brazing and soldering, can be done by methods in general use.

ASC Metal Diffusion also gives low and medium carbon ferrous products *corrosion* resistance equal to that of 430 stainless. Medium and high carbon content products can be given *wear* resistance surface hardness of RC 70-72. For more information about this revolutionary process write for data, consultation, or product demonstration.

ALLOY SURFACES COMPANY

103 South Justison St., Wilmington 1, Del.

For more information, turn to Reader Service Card, Circle No. 406

an inch because thicker metal absorbs too much of the low energy x-ray beam and requires too long an exposure time. The assembly is held in a cardboard cassette The base metal side of the plated material is exposed to x-rays or radiation from a radioactive material, such as radioactive iron, nickel or cobalt. Soft x-rays are used to insure good contrast of the flaws on the film.

After a suitable exposure time, the film is removed and developed. Satisfactory radiographs result from 3 or 4-min exposure to an x-ray machine or 24-hr exposure to 1 millimicron of radioactivity. Wherever a pore exists in the coating a black spot appears on the developed film. A fine grain industrial x-ray film gives the most readable radiograph.

Wood Chip Sheet Is Moisture Resistant

A new wood product recently developed in Europe utilizes wood chips that were formerly discarded. Called Novopan, the material is made up of three layers of wood chips consisting of a porous middle layer and a top and bottom layer of thin flat chips arranged crosswise.

Tests indicate that the three ply sheets are partly fire resistant and that they possess good sound and heat insulating properties. The wood chip sheets are also said to be one-third more resistant to fungi and insects than solid fir wood sheets. Fir and hemlock chips with a maximum leaf wood content of 10% give especially good results. However, all kinds of wood chips can be used to make the sheets.

The sheets are made by slowly mixing 5 to 8% (sometimes 10%) of urea-formaldehyde resin with wood chips, then drying them at 158 F to reduce the moisture content of the wood. After drying, the wood chips are shaken, pre-

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What's new IN MATERIALS

pressed at room temperature and hardened in a multilayer hydraulic press at 285 to 300 F under a pressure of 14,000 to 35,000 psi.

A ⅞-in. sheet made by this technique had a bending strength of 220,000 psi and a modulus of elasticity of 42 x 10^6 psi. Moisture content increased only 7% after storage in an atmosphere of 95% R. H. for 152 days. Shrinkage after drying was 2.8% in both length and width; solid fir and hemlock sheets shrank 36% in length and 78% in width.

The wood chip sheets can be painted, varnished and tanned, and are recommended for wall surfaces, furniture and building panels. (Condensed from *European Technical Digests*, Dec '56.)

Copper-Clad Plastic for Printed Circuits

A copper-clad laminated plastics material, said to be an improved XXP grade laminate that also meets specification MIL 3115

PROPERTIES OF CIRPRINT

Flexural Strength (flatwise), psi	
Lengthwise	18,000
Crosswise	14,000
Izod Impact (edgewise, cond E 48/50), ft-lb/in.	
Lengthwise	0.50
Crosswise	0.45
Tensile Strength, psi	
Lengthwise	15,000
Crosswise	10,000
Compressive Strength (flatwise), psi	25,000
Water Absorption (24 hr immersion), % (power)	0.80
Dissipation (power) Factor	
As Received	0.035
24 Hr Immersion	0.040
Dielectric Constant	
As Received	4.70
24 Hr Immersion	4.90
Dielectric Strength (par. to lam), kv	
As Received	80
48 Hr Immersion	60
Dielectric Strength (perp to lam), v/mil	
Short Time	700
Step-by-Step	500
Insulation Resistance (cond C-99/35/90), megohms	50,000

IBM GROWTH promoted these men

Research Engineer: Before his recent promotion, this man was a member of a small research team comprising three E.E.'s and a technician. His specific project entailed the creation of a transistorized electronic converter combining both digital and analog circuitry. "Research is really on the move at IBM," he says. "Personnel has increased ten-fold since 1950 and we expect to maintain this pace for some time."

Manufacturing Engineer: Also promoted recently, this man worked in one of IBM's many manufacturing plants. He was responsible for the analysis, design and procurement of equipment and facilities to produce the giant IBM electronic computers. "In a field as new as electronic computers," he'll tell you, "*unique* manufacturing equipment is often imperative. Creating this new equipment is a real challenge to an engineer's ingenuity."

Could you handle their responsibilities?

Jobs like these continually open up at IBM—due to rapid expansion. If you are an engineer or scientist—or have equivalent experience—you may be qualified for such a position. Innumerable opportunities exist in:

- Computer systems planning
- Computer systems testing
- Electronic circuit design and packaging
- Electrostatic phenomena
- Manufacturing process control
- Numerical analysis and programming
- Photo and magnetic device memory
- Real time systems engineering
- Semi-conductor research, development, and manufacturing
- Test equipment design

The electronic computer field offers one of the best ground-floor career opportunities today. Economic experts rank it with automation and nucleonics in growth potential. Sales at IBM, the recognized leader in this fast-growing field, have doubled, on the average, every five years since 1930. Engineering laboratory personnel has quintupled in the past five years. IBM's excellent salary and employee benefit program is instrumental in achieving an employee turnover rate far below the national average.

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For more information, turn to Reader Service Card, Circle No. 564

What's new IN MATERIALS

B, has been introduced by Formica Corp., 4408 Spring Grove Ave., Cincinnati 32, Ohio.

Designated Cirprint, the paper-base material is said to have good insulation resistance, low moisture absorption and good cold punching qualities. The material is translucent; its translucency is said to offer two advantages: 1) it permits a visual check on the register of a circuit printed on both sides, and 2) it permits a visual check for voids, blisters or other impurities that might reduce electrical insulating properties of the sheet.

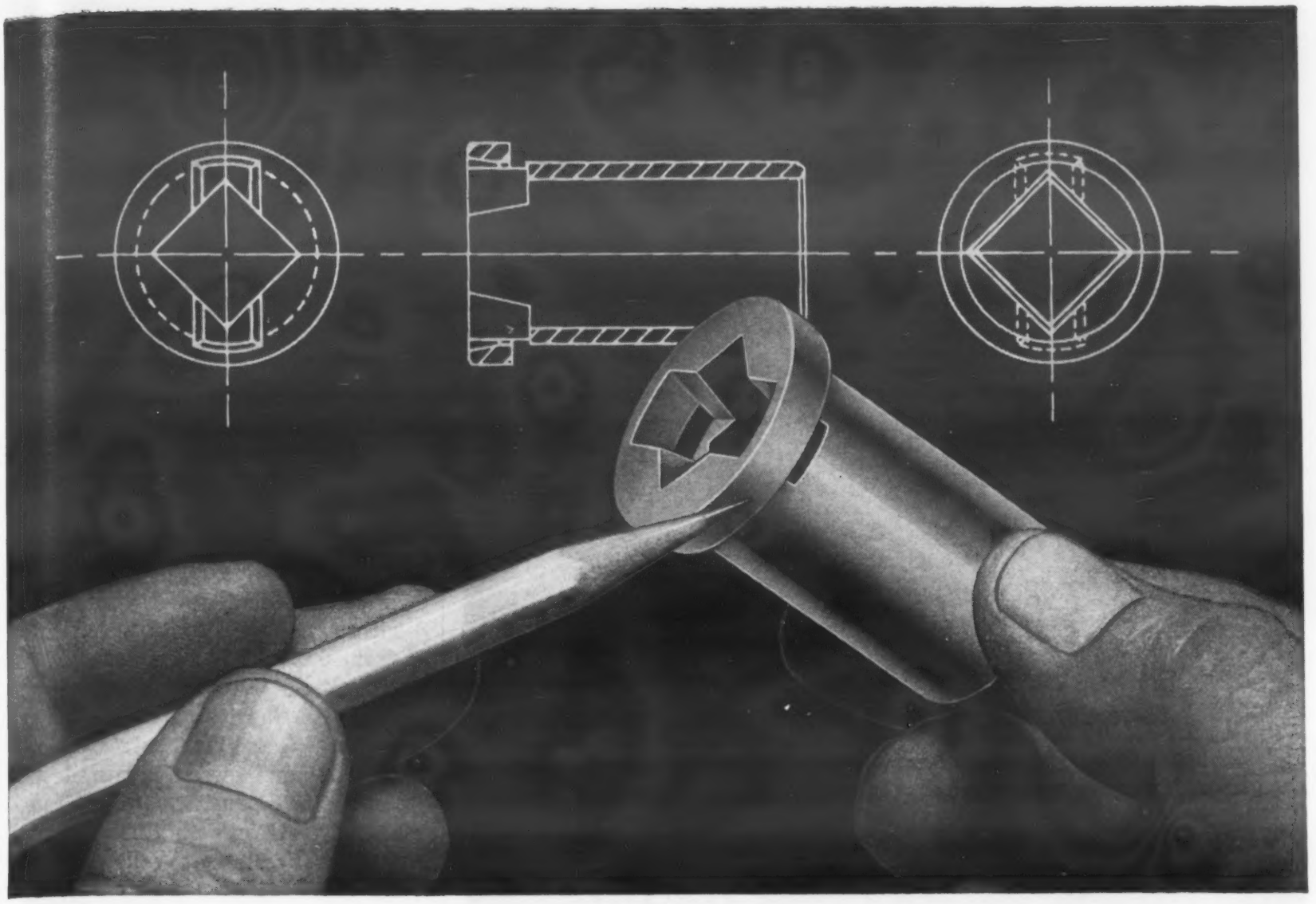
Tank Lining Sheet Needs No Field Curing

A ready-cured, synthetic rubber tank-lining sheet that is said to eliminate the necessity of curing in the field or of moving equipment from its operational location, has been announced by E. I. du Pont de Nemours & Co., Inc., Fabrics Div., Wilmington 98, Del. Called Fairprene T-5594, the synthetic rubber lining material is offered as part of a packaged consisting of primers, adhesives and putties.

The material is stable in storage and requires no refrigeration. Its stretch is said to approach that of natural rubber lining materials, and applied cost per square foot is said to be appreciably lower than that of natural rubber and other materials now in use. It is available as a two ply, 50-in. wide sheet ⅛ in. thick.

Magnesium Properties Vary with Heating Rate

Aerodynamic heating of aircraft and missiles has led to considerable research on the strength of materials at elevated temperatures. Recent investigations have shown that materials exhibit



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Can't be done? Parker did it . . . sharp internal corners, lateral holes, chamfers, flanged end and all . . . by fast, low-cost powdered metal pressing and sintering. No subsequent machining . . . no scrap-metal loss. Just think of the savings compared with conventional machining methods.

In addition to these inherent cost savings, Parker-engineered Powdered Metal Parts offer a wide choice of tensiles, ductility, density, impact resistance and other physicals. Tooling-up is done quickly and at relatively low cost.

It will pay you to check on the economies and design possibilities of Parker-engineered Powdered Metal Parts. Just call the nearest sales engineer listed here or write the factory direct.

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WILTON, Conn.
Girard L. Palmer • Belden Hill Road
SYRACUSE, N. Y.
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POWDERED METAL PARTS

For more information, turn to Reader Service Card, Circle No. 482

What's new IN MATERIALS

greater tensile strength when heated at rapid rates than under conventional constant temperature test conditions. The latest of these investigations, by Ivo M. Kurg, of the National Advisory Committee for Aeronautics, was conducted on AZ31A-O magnesium alloy sheet. Kurg's work shows that:

1. At all stress levels tensile yield and rupture temperatures increase linearly with the logarithm of the heating rate for rates from 0.2 to 100 F per sec.

2. Yield stresses obtained from rapid heating tests can be greater or less than yield stresses obtained from stress-strain tests, depending upon temperature rate. Rupture stresses obtained in rapid heating tests at all heating rates investigated are appreciably greater than the ultimate tensile stresses from stress-strain tests.

3. Yield and rupture temperatures, or the corresponding stresses, can be predicted for any heating rate by master curves and heating rate parameters.

A new material, HK 31XA-H24 magnesium alloy sheet, was also tested under the same conditions. Results indicate that the experimental sheet material has elevated temperature properties under both constant temperature and rapid heating conditions that are superior to those of AZ31A-O alloy. However, because the material is still in the developmental stage, these results may not be typical.

Two Epoxy Resins for Potting, Casting

Two epoxy resins for casting, potting, laminating, encapsulating and other purposes have recently been introduced by Marblette Corp., 37-31 30th St., Long Island City 1, N. Y.

One resin, designated Maraset Rubber-Like Resin No. 636, is a flexible compound having an elon-

For more information, Circle No. 621 ➤

gation of 200% and a tensile strength of 2500 to 3500 psi. It can be used to produce low-cost castings in unlimited thicknesses and a wide range of hardnesses. Ideal for potting, sealing and encapsulating electronic components, it can also be used as a replacement for rubber or plastisols in gaskets and other applications.

The other resin combines the properties of rigid and resilient epoxies in a single resin system. Designated Maraset Casting Resin No. 650, it is described as a low-irritant formulation with an elongation of 3 to 5% and an unnotched Izod impact strength of 7 ft-lb per in. The rigid epoxy compound has a Rockwell M hardness of 100 and an ultimate compressive strength of 40,000 psi.

Wood Flake Board

A particle board for furniture and other nonstructural applications has been introduced by Formica Corp., 4819 Spring Grove Ave., Cincinnati 32, Ohio. The wood particle board, composed of wood flakes and resins, is made under pressure and heat. Called Flakeboard, the material is not easily splintered or broken, and it can be sawed and planed without difficulty. It has a modulus of 3500 psi and a direct screw holding power of 350 lb. It will be available in sheet sizes up to 6 x 12 ft, ranging in thickness from ¼ to 1¼ in.

Stainless Pipe to Take Steam at 5000 Psi

For the first time in turbine history a stainless steel pipe will carry steam at 1200 F at a working pressure of 5000 psi. The pipe, 10 in. in dia with a 3½-in. wall and 9-ft length, will be used in Philadelphia Electric's Eddystone, Pa., power plant.

Modified type 316 stainless steel

ingots weighing five tons were bloomed into billets by Sharon Steel Corp. and forged by Pennsylvania Forge Co. The final product will be fabricated and installed by M. W. Kellogg Co.

Evaluating Paper As a Core Material

Considerable savings in core materials for sandwich construction may be afforded by the use of resin-impregnated paper. Over the years the search for a suitable core material for use in sandwich panel construction has included an economic, chemical and mechanical evaluation of numerous core materials, including balsa wood and rubber and plastics foams. From the standpoint of economics and availability, resin-impregnated paper has played a large role in the development of the sandwich panel.

Recently the Forest Products Laboratory undertook a study to see whether the cost of resin-impregnated paper honeycomb cores could be further reduced. This was done by evaluating the effects of 1) lowering the resin content, 2) reducing the weight of the paper, and 3) using less costly adhesives on the strength, decay resistance and other properties of the sandwich panel. The study was done in cooperation with the Housing and Home Finance Agency and the University of Wisconsin, and the investigators included R. J. Seidl, E. W. Kuenzi, D. J. Fahey and C. S. Moses. Details of this study may be found in Report No. R 1796 issued by the Forest Service Div., U.S. Dept. of Agriculture.

Effect of resins

From the standpoint of lowering the resin content, the properties of paper cores containing 5, 10 and 15% of phenolic resin were compared with those of unimpregnated paper. The base

TAYLOR
Laminated Plastics
Vulcanized Fibre

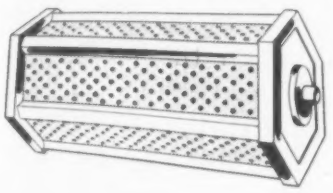
Shop Talk

TAYLOR FIBRE CO.

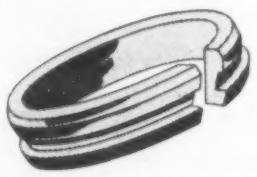
Plants in Norristown, Pa. and La Verne, Calif.

PHENOLIC—MELAMINE—SILICONE—EPOXY LAMINATES • COMBINATION LAMINATES • COPPER-CLAD LAMINATES • VULCANIZED FIBRE

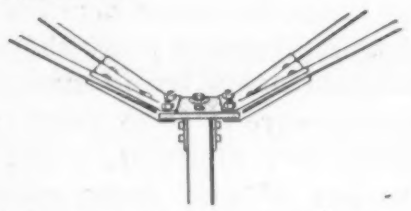
Tips for designers



"Metal-plating barrels" of Taylor Grade C-5 melamine withstand corrosion and erosion successfully in alkaline solutions. Downtime and maintenance costs are substantially reduced.



Self-retaining grommets cut from Taylor phenolic tubing shield cables and wires passing through bulkheads . . . offer good electrical insulating properties.

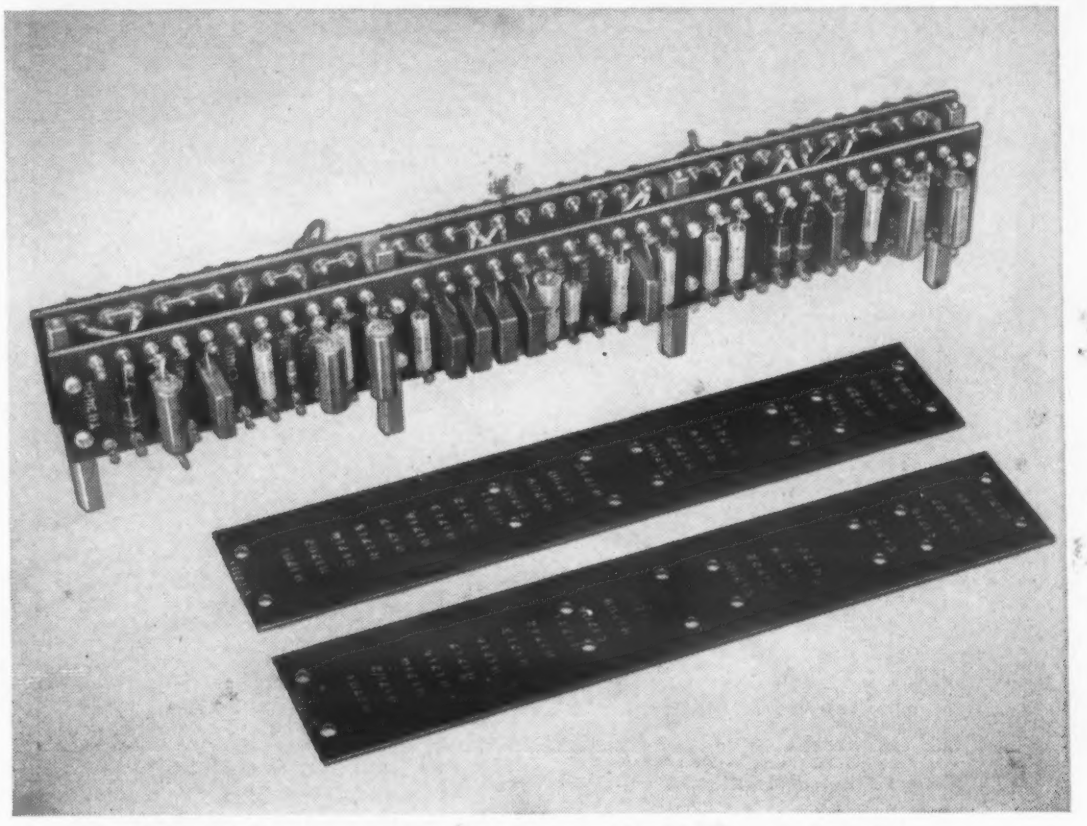


Insulation support of TV antenna rods is made of Taylor laminated phenolic which assures dependable, moisture-resistant insulation . . . is unaffected by weather.

Identification tag, easily fabricated from Taylor super-white vulcanized fibre, is non-abrasive and non-corrosive, can be printed and has safe, non-cutting edges.

NEW TAYLOR COPPER-CLAD LAMINATES

Taylor GEC (glass epoxy) Copper-Clad and Taylor XXXP-242 cold punching (paper-phenolic) Copper-Clad. Taylor uses high purity rolled copper on base materials with outstanding electrical properties.



Six resistor board assemblies on the new Martin Matador guided missile are of Taylor Grade GEC (glass epoxy) laminate, chosen for this tough application because of its stable electrical properties and humidity resistance.

Taylor Glass Epoxy Laminate meets critical insulation needs

Taylor GEC (glass epoxy) meets the Matador's exacting electrical insulation requirements. These requirements consist of . . . high strength to withstand the G's . . . low moisture absorption to withstand the varying humidity and temperature . . . electrical and mechanical stability. Your requirements, which are no doubt different, may be equally exacting. Taylor's wide range of laminates include that combination of electrical, mechanical and chemical properties that you require.

Designed for ease of fabrication . . . Taylor laminates are the result of resin formulations and production techniques developed to make fabrication of completed parts easier and less costly. They are especially suited to punching, staking, milling, sawing or drilling when accurately sized parts are a must.

When specifications call for stability, specify Taylor laminates. They maintain their original characteristics over long periods of time and under rugged operating conditions.

To help you in your selection of a laminate, Taylor's engineering staff and fabricating facilities are at your service. Contact your nearest Taylor sales engineer for a discussion of your particular requirements.

For more information, turn to Reader Service Card, Circle No. 402

material of the cores consisted of Kraft paper of 30-, 50- and 65-lb weight, and the densities of the cores ranged from 1.6 to 3.0 lb per cu ft.

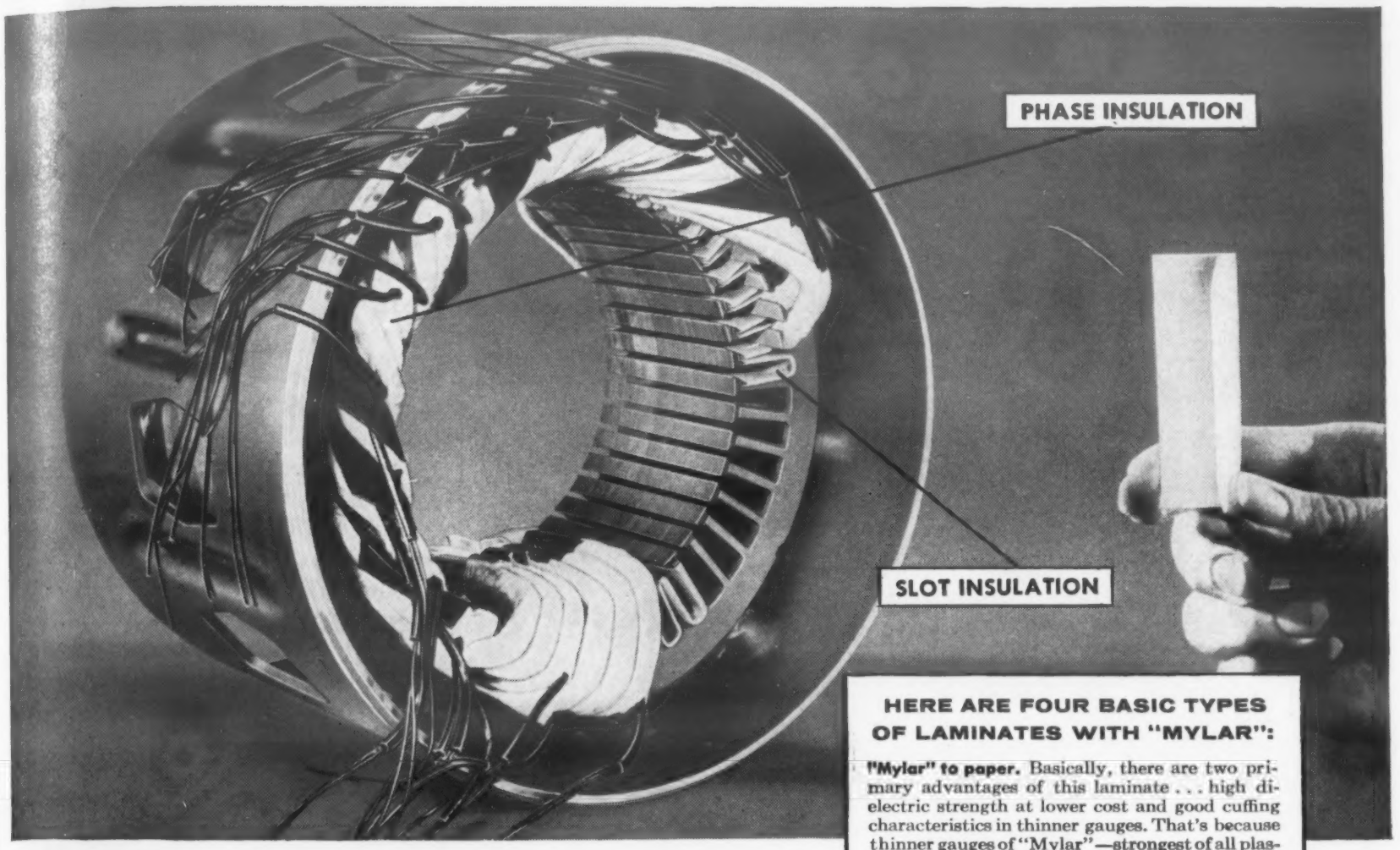
The effect of phenolic resin impregnation on the physical properties of the paper was reflected chiefly in greatly increased tensile strength of the paper, particularly in the wet condition. The greatest increase in wet tensile strength of the paper was obtained from the first 5% of resin. Wet tensile strength in the machine direction increased from 3 to 30 lb per in. of width with a 5% resin addition, and to 40 lb per in. with a 15% resin addition. Dry tensile strength of the paper increased from 35 to 42 lb per in. of width with a 5% resin addition and 50 lb per in, with 15% resin.

With respect to the effects of decay fungi, the researchers found that unimpregnated paper showed a complete loss of tensile strength after exposure to decay fungi for two months. However, a paper containing 15% of water soluble phenolic resin had practically no loss in strength under similar exposure. Paper impregnated with water soluble phenolic resin was much more resistant to decay fungi than paper containing alcohol soluble phenolic resin. Pentachlorophenol added to paper containing 5% resin was found to suppress the action of the fungi.

Effect of adhesives

To explore the effect of the quality of the bond between sheets of paper on the properties of a sandwich construction, a series of tests was made to compare phenolic, urea and sodium silicate adhesives. Results gathered from a number of tests indicated that maximum strength, regardless of adhesive, was obtained by placing the web of the corrugated paper parallel, not perpendicular, to the span of the shearing specimen. Other test results indicated that the tensile and shearing strengths

DU PONT MYLAR®



MYLAR—and laminates with MYLAR—offer superior insulation performance

As most of the nation's leading electrical manufacturers have discovered, Du Pont "Mylar"* polyester film and laminates with "Mylar" offer a wide range of superior insulating properties. The superior qualities of this thin, flexible film can be translated into performance benefits when manufacturing a variety of electrical products! Examples include:

MOTORS—Manufacturers have been able to extend motor life by as much as 100%.

TRANSFORMERS—Manufacturers have been able to reduce size, weight and insulation costs.

CABLE—Manufacturers have been able to speed up production while reducing size and weight.

MAGNETIC AMPLIFIERS—Manufacturers have been able to reduce rejects due to moisture penetration.

The common denominator in each instance is "Mylar". . . with its resistance to moisture, chemicals; its high physical and dielectric strength even in thin gauges; and its thermal qualities. If you have a particularly tough insulation problem, write Du Pont today.

HERE ARE FOUR BASIC TYPES OF LAMINATES WITH "MYLAR":

"Mylar" to paper. Basically, there are two primary advantages of this laminate . . . high dielectric strength at lower cost and good cuffing characteristics in thinner gauges. That's because thinner gauges of "Mylar"—strongest of all plastic films—can be used.

"Mylar" to glass cloth. Because "Mylar" remains dimensionally stable from −60° to 150° C., "Mylar" laminated to glass cloth offers superior insulation at both high and low temperatures. In addition to high flexibility, this laminate has good forming characteristics in thinner gauges.

"Mylar" to asbestos. Excellent for motors and generators operating in the Class "B" temperature range. Coated asbestos laminated to this tough polyester film produces a stronger product with increased moisture resistance.

"Mylar" to mica. This laminate offers *maximum* insulation plus flexibility. In short, mica is easier to work with when laminated to "Mylar". Costs are lower too because thinner gauges of mica can be used . . . Du Pont "Mylar" gives the mica "body."

• If you like to compare the properties and cost of the insulating materials, send for our new pocket-size Cost and Property Comparator. It operates like a slide rule . . . quickly determines costs of insulating materials on a sq. ft. basis . . . quickly compares the properties of "Mylar" and seven other materials.

Du Pont manufactures the basic material "Mylar"—not finished electrical laminates.

**"Mylar" is Du Pont's registered trademark for its brand of polyester film.*

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BETTER THINGS FOR BETTER LIVING . . . *THROUGH CHEMISTRY*

DU PONT ® MYLAR POLYESTER FILM

☐ Please send "Cost and Property Comparator".

☐ Please send me more information on properties, types and applications of "Mylar" available (MB-11).

E. I. du Pont de Nemours & Co. (Inc.), Film Dept.,
Room MM-4, Nemours Bldg., Wilmington 98, Delaware

I am interested in "Mylar" for_____

Name_____

Firm_____

Address_____

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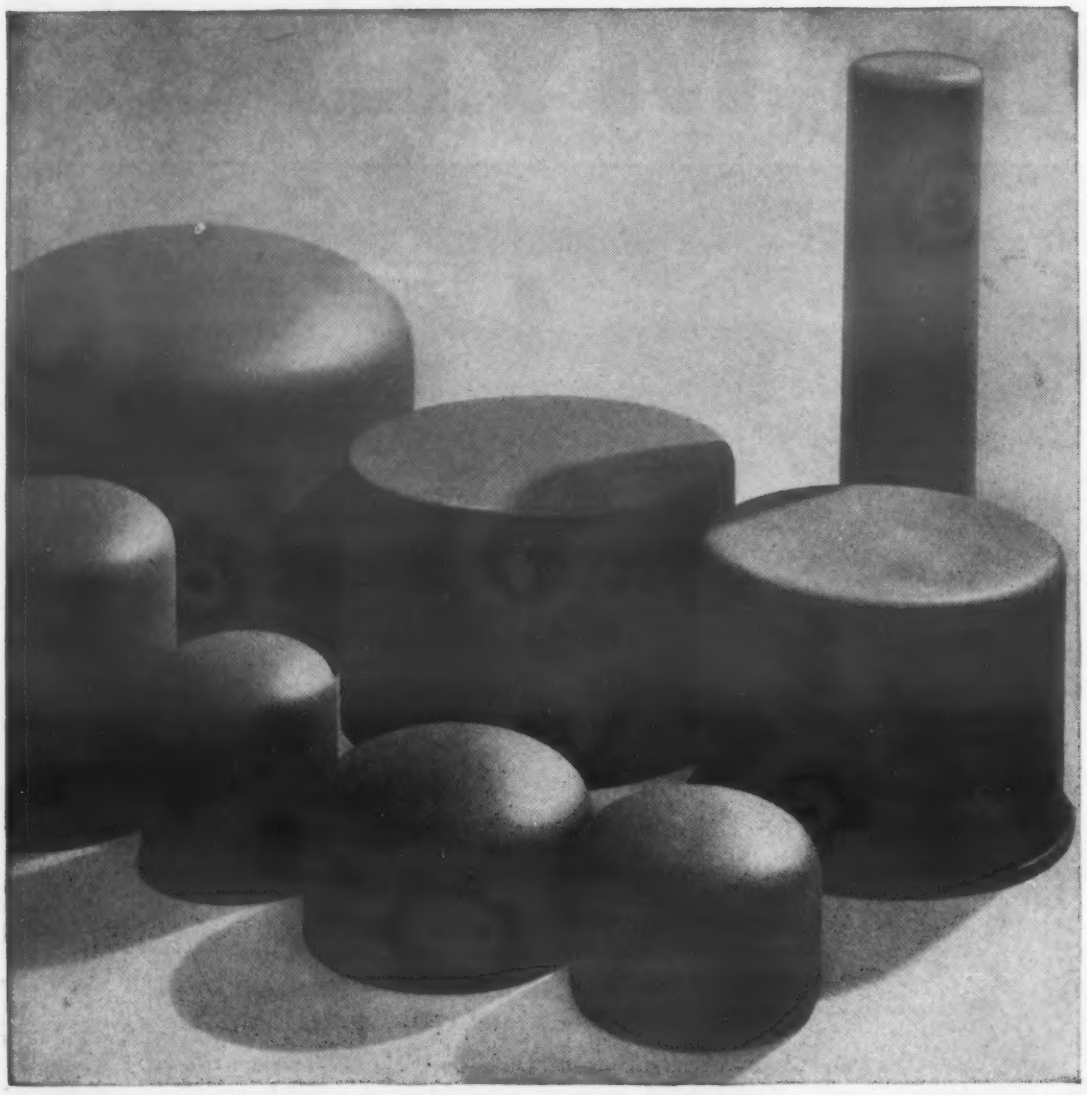
For more information, turn to Reader Service Card, Circle No. 574



of core specimens bonded with sodium silicate adhesive were slightly higher when dry and slightly lower when wet than corresponding values obtained from specimens having cores bonded with phenolic adhesives.

It was also found that the strengths of panels having cores constructed without the use of a crest adhesive were slightly lower than those of panels having cores constructed with a crest-to-crest adhesive, a fact indicating that high quality bonding between individual sheets in cores is not essential.

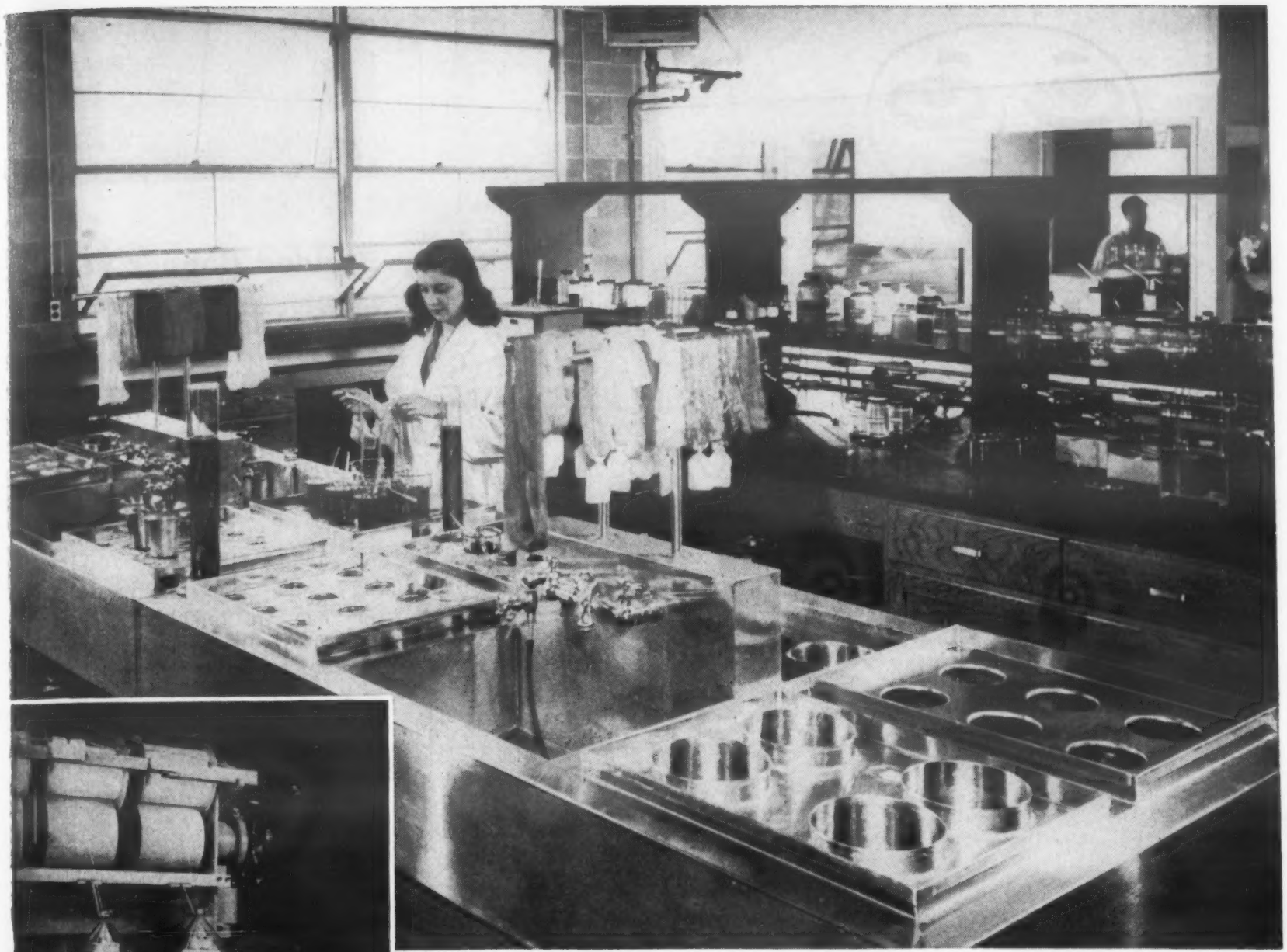
Effect of paper weight

A Kraft paper was used in the test because of its availability in large tonnages at a reasonable price and because it seems to be a stable material. A further economy is possible by using paper made of less expensive fibers. Paper of less than 30-lb weight was not used because it was believed that a lighter paper would present problems of corrugating and handling at high production rates.

As the weight of the paper containing 5% of resin was increased, the shear stress (developed in bending) and the compressive strength of the dry sandwich panels increased considerably. However, there was no significant increase in the physical properties of panels tested in the wet condition.

Increasing the paper's weight from 30 lb to 50 lb increased the dry shear strength from 28 psi to 52 psi for a phenolic resin-bonded core, although the strength of corresponding specimens tested wet remained virtually unchanged. For paper containing 15% resin, the wet shear strength was more than doubled by increasing the weight from 30 lb to 50 lb. The increase in wet compressive strength was not so great. No reason is given for the difference in physical properties of the 5 and 15% resin treated papers tested wet.

(more What's New on p 238)



Wherever you want to protect something

. . . that's a place for A-L Stainless Steel

In a textile plant, like the applications pictured above, Allegheny Ludlum Stainless Steel protects against off-colors in the dyeing and finishing department because it cleans up easily and quickly from batch to batch, leaving no traces of the previous dyes. In yarn twisters and other equipment in the weaving department, A-L Stainless provides the hard, smooth surface and high abrasion-resistance that protects against snagging and binding.

Food, beverage, dairy, drug and chemical plants use A-L Stainless Steel to protect the purity of their products; hospitals, hotels and restaurants use it to protect appearance and sanitary standards; cars, trains and planes use it to protect strength and safety. And they all gain a host of bonus benefits from stainless steel, too: such as far less cleaning and maintenance expense, far longer life in service, and far greater economy in the long run.

No other metal can match stainless steel in these qualities. In addition, A-L Stainless is easy to fabricate and we produce it in every form or shape that you may require.

● Let us help you to profit by it. ***Allegheny Ludlum Steel Corporation, Oliver Bldg., Pittsburgh 22, Pa.***

Write for your copy of "STAINLESS STEEL IN PRODUCT DESIGN"

40 pages of useful engineering and fabricating data, including practical examples showing where, when and how stainless steel improves design, adds benefits, helps sales.

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For Stainless Steel in ALL Forms—call

Allegheny Ludlum

AL STAINLESS STEEL ®

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Warehouse stocks carried by all Ryerson Steel plants

For more information, turn to Reader Service Card, Circle No. 580

What's new IN MATERIALS

Braided Copper Wire in Stretchable Cord

A new electric cord that stretches is composed of a rubber core wound or braided with copper. Fiberglass, rayon, silicone rubber or nylon may be used as insulation.

Called Elasticable and produced by Mutual Electronic Industries Corp., the new cord is designed for use in telephones, switchboards, appliances, and other industrial and military applications.

Pure Titanium Powder Has Good Stability

Development of a pure titanium powder that can be easily formed by powder metallurgy techniques into corrosion resistant parts has been announced by United International Research, Inc., 38-15 30th St., Long Island City 1, N. Y.

Designated UniFide, the powder has a low oxygen content (0.25%) and is stable in air. When exposed to air for three months in an open container, oxygen content of the powder only increased from 0.034 to 0.053%. According to the producer, this stability permits shipping of the powder as a dry material, unlike other titanium powders which must be shipped under water.

How Ceramic Coatings Affect Creep Rates

Refractory type ceramic coatings are being widely used to protect metal parts at high temperatures. It has been found that ceramic coatings affect the creep rates of some alloys; under some conditions, for example, a ceramic coating can reduce creep of a metal by as much as 50%.

In order to learn more about the effects of ceramic coatings on

Just pick up your phone—

get price quotations, expert advice, prompt delivery

from your Superior Warehouse Distributor

Up against a tubing problem? Call your nearest Superior distributor. He's well stocked with quality tubing and information. Often he can make money-saving recommendations. Through his contact with the mill he can expedite information and orders for you. Let him show you why Superior tubing offers you real economy. Call on him today. He can save you valuable time and money.

For general information on Superior tubing, get a free copy of Bulletin 40. Write Superior Tube Company, 2006 Germantown Ave., Norristown, Pa.

Superior Tube

The big name in small tubing

NORRISTOWN, PA.

All analyses .010 to ⅝ in. OD—certain analyses in light walls up to 2½ in. OD

For more information, turn to Reader Service Card, Circle No. 584

What's new IN MATERIALS

the creep rates of alloys, J. R. Cuthill, J. C. Richmond and N. J. Tighe of the National Bureau of Standard's enameled metals laboratory recently began a study of this behavior under different temperature-stress conditions.

The NBS test utilized a ceramic coating made of cerium oxide, enameler's clay and frit on two 80 nickel-20% chromium alloy metal strips machined from thin sheet metal. The alloys differed significantly in manganese, iron and silicon content. Both coated and uncoated samples were tested at various temperatures and pressures over a period of time.

What creep curves show

Creep curves of coated specimens usually remained below the curves of uncoated specimens during the first 20 hr of testing. However, coated specimens generally showed a greater rate of increase in creep than uncoated specimens beginning about 20 to 30 hr after the start of the test. This increase took place during a period of rapidly increasing creep rate, and fractures of the coated specimens usually occurred during this period. A ceramic coated specimen that did not fail under test for more than 1200 hr showed significantly greater creep after the first 100 hr than did the uncoated specimens.

No void formation was found in coated or uncoated specimens tested at 1800 F. Extensive internal voids were found in uncoated specimens tested at 1900 and at 1975 F, whereas little void formation occurred in coated specimens at either of these temperatures. A chemical analysis of an uncoated specimen showed that it lost twice as much chromium as a coated specimen tested at the same temperature.

Better when hotter

At 1900 F and 900 psi and at 1975 F and 600 psi, the creep rate of both alloys was virtually constant for the duration of the test.

(continued on p 242)

J-M CERAFELT insulation . . .

controls heat more effectively in a wide variety of high-temperature industrial services!

Cerafelt® is one of the most recent achievements of Johns-Manville insulation scientists . . . developed specifically for the new high-temperature processes now being employed in the metallurgical, chemical, ceramic and allied industries.

Particularly important in these applications is Cerafelt's infra-red opacity, an advantage that accounts for its unusually low *k* factor at elevated temperatures. Another important advantage is fineness of fiber structure. With fibers averaging only 3 microns in diameter, Cerafelt contains far more heat-blocking air pockets per cubic inch. Hence, it offers far better insulating effectiveness at high temperatures!

Cerafelt is non-alkaline, chemically stable, and contains no corrosion-promoting agents. For information write to Johns-Manville, Box 14, New York 16, N. Y.
In Canada, Port Credit, Ontario.

DENSITIES, SIZES & THICKNESSES

Type	Density lbs. per cu ft		Available Thickness inches		
CRF300	3	¼	½	¾	1
CRF400	4	¼	½	¾	1
CRF600	6	¼	½	¾	1
CRF800	8		½	¾	1
CRF1000	10		½	¾	
CRF1200	12		½		

STANDARD SIZES:
Length: Regularly furnished in 3, 4, 5, 6 and 8 ft. lengths. CRF300 through 800 (except in 1" thickness) also furnished in 26 ft. lengths.
Width: 42 inches (untrimmed).
In loose fiber form the material is known as J-M CERAFIBER; shipped 10 lbs. per bag.

JOHNS-MANVILLE PRODUCTS

Johns-Manville
INSULATIONS
for lasting thermal efficiency

What's new IN MATERIALS

At 1800 F and 2200 psi, the initial creep rate was comparatively low —well below that of the uncoated specimens, but after 20 to 30 hr the creep rate increased rapidly for a few hours and then became gradually less again.

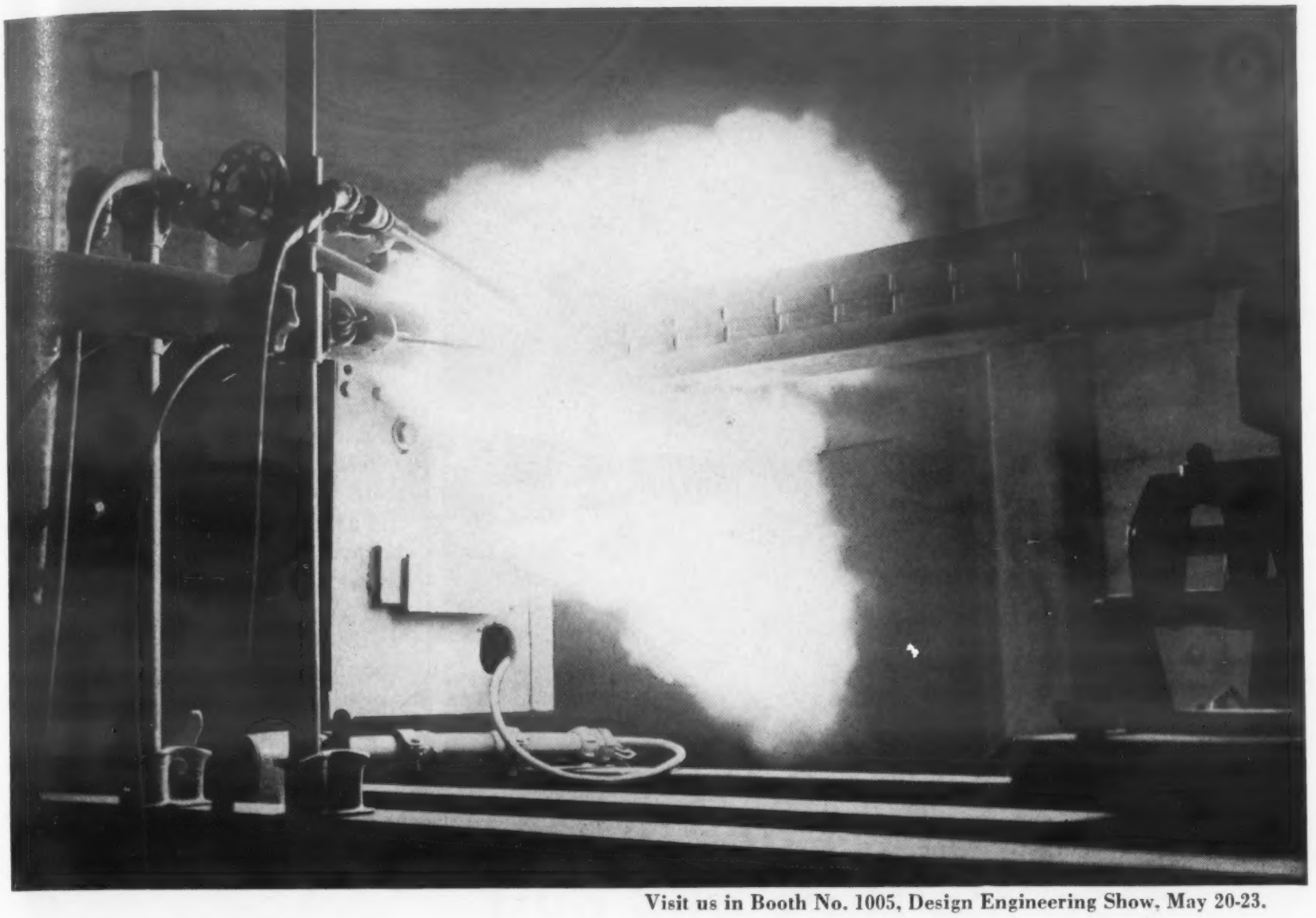
The test results suggest that ceramic coatings are not sufficiently fluid at 1800 F to follow the deformation of the specimen when a stress of 2200 psi is applied. Profuse cracking of the coating occurred in all of the coated specimens that failed at 1800 F and 2200 psi, but in no other specimens. Presumably, at higher temperatures the ceramic coating is more plastic than at lower temperatures and is able to follow the deformation of the specimen at strain rates as high as those which result in failure at the lower temperatures.

Auto Crankshafts Cast of Pearlitic Iron

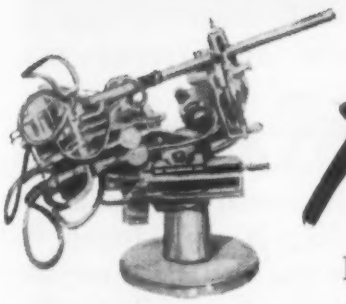
The successful use of cast pearlitic malleable iron for large parts has resulted from 1) additions of bismuth to the molten iron to increase the section size of parts that can be cast in the white condition and 2) additions of boron to facilitate precipitation of temper carbon. As a result of these developments and recent improvements in shell molding techniques, General Motors Corp. specified pearlitic malleable iron crankshafts for its Pontiac cars. Now, after a substantial production run, D. B. Valentine has gathered information on some of the characteristics of the iron crankshafts. He presented his findings at the annual meeting of the Society of Automotive Engineers held in January. A summary of some of his findings:

Modulus of elasticity—Although forged steel crankshafts possess a higher modulus (29 million psi compared to 24-26 million psi),

A LOW-POROSITY, WEAR-RESISTANT ALUMINUM OXIDE COATING



Visit us in Booth No. 1005, Design Engineering Show, May 20-23.



Flame-Plating by Linde
Trade-Mark

LINDE's Flame-Plating method of coating metal surfaces now provides extra wear resistance for parts subject to extremely hard wear and high temperatures. This new high-purity aluminum oxide coating, blasted from the Flame-Plating gun, builds up on the workpiece in desired thicknesses from .002 to .040 inch. With a porosity of *less than 1 per cent*, the aluminum oxide coating can be used at temperatures up to 1750 degrees F.

The hardness of aluminum oxide coatings, Flame-Plated by LINDE, ranges from 1000 to 1200 VPN. Metallurgical properties of the base metal are not modified by the Flame-Plating process because the part being plated always remains at a temperature of 400° F. or below. The bond between coating and base metal is exceptionally strong with aluminum. Aluminum oxide coatings can be used in as-coated condition (approximately 120 microinches rms), or finished to better than 1 microinch rms.

Flame-Plated coatings of aluminum oxide provide resistance to wear, and to chemical action in high temperature applications. Applications are found in thrust bearings, pump plungers, thermocouple tubes, gas turbines, guided missiles, and other devices. Either aluminum oxide or tungsten carbide can be Flame-Plated on most metals. If you have a special wear problem, LINDE's Flame-Plating Department will gladly help you to reach a solution. Write to "Flame-Plating Department N-4."

LINDE AIR PRODUCTS COMPANY

A Division of Union Carbide and Carbon Corporation

30 East 42nd Street UCC New York 17, New York

In Canada: Linde Air Products Company, Division of Union Carbide Canada Limited, Toronto

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Flame-Plating by Linde

For more information, turn to Reader Service Card, Circle No. 438

similar torsional vibration characteristics are obtained by modifying the design of the pearlitic iron crankshaft. Tests have shown that the lower modulus is no detriment to smoothness of engine operation at normal car driving speed.

Fatigue properties — Dynanometer tests and 100,000-mile road tests show comparable endurance of forged and cast crankshafts. Variations in notch sharpness have no effect on fatigue properties.

Tensile strength — Standard ASTM 505 tensile test bars, machined from journals and counterweights of pearlitic malleable iron crankshafts, possess 96,000 psi tensile strength at 228 Brinell hardness. This figure compares with 114,000 psi obtained from 1046 SAE steel.

Wear characteristics—There is no appreciable difference in pin and journal wear between cast crankshafts and forged crankshafts.

Machining—On the basis of 59,000 forged steel crankshafts and 49,000 pearlitic malleable iron crankshafts, it was found that with iron the tool life increased, the number of grinding wheels necessary decreased and the feed rate increased.

Epoxy-Base Enamel for Dark Phenolic Parts

Dark colored phenolic parts, such as telephone handsets (see photo) and electric iron handles, can now be colored economically and permanently without using primers or multiple coats. This is possible through the use of a new epoxy-base enamel developed by Rexton Finishes, Inc., Irvington, N.J. Thermosetting parts rejected for color contamination can be salvaged by application of this epoxy-base finish.

Intended primarily for use on phenolics, the new enamel is said

MicroMach extra-high-tensile stainless steel sheets up to 48" WIDE for aircraft and missile use

As the speed of today's aircraft rapidly approaches the Thermal Barrier, conventional metals are being left far behind in the race to satisfy the structural requirements of supersonic craft. Needed are metals that can withstand the intense heat caused by air friction at high speeds and still retain their strength. One such metal, MicroMach stainless, has been in use for more than a year.

MicroMach is a special aircraft and missile grade of modified type 301 stainless steel sheet furnished to higher mechanical properties than are available in other commercial high tensile grades in the full hard condition.

These sheets are rolled to extremely close tolerances (as low as plus or minus 3%) with micro-accuracy and precise uniformity of gauge. The surface of MicroMach sheet is smooth, clean and dense; qualities so important in minimizing surface friction.

For further information write to Aircraft Steels Dept.

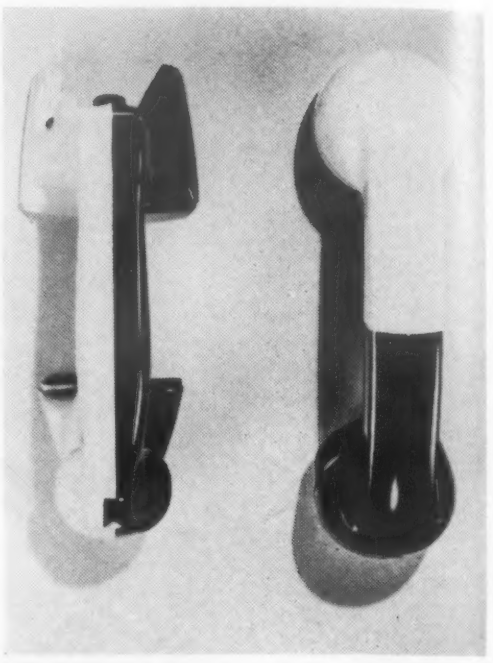
Washington Steel *Corporation*

4-F WOODLAND AVENUE
WASHINGTON, PA.

MicroRold stainless steel is also available in all popular grades and to meet regular government specifications. Sheets up to 36" wide can be had as thin as .005", and over 36" to 48" wide as thin as .010" in all commercial finishes and tempers.

For more information, turn to Reader Service Card, Circle No. 524

What's new IN MATERIALS



Light colored *epoxy-base enamel covers dark colored phenolic part with one coat.*

to work equally well on steel, brass, aluminum, glass and other plastics. The supplier estimates cost of applying the enamel at about 1¢ per sq ft.

The enamel is fast drying and permits the handling of air dry pieces in about 2 hr. It is available in a variety of finishes and colors, including clear and metallic.

Cast Acrylic Sheets Made Extra Large

Extra large, cast acrylic sheets, in sizes up to 8½ x 10 ft, are available in both clear and colored sheets from Rohm & Haas Co., Washington Square, Philadelphia 5. Called Plexiglas RL, the sheet material is designed for use in internally illuminated signs, fluorescent luminaires and skylights.

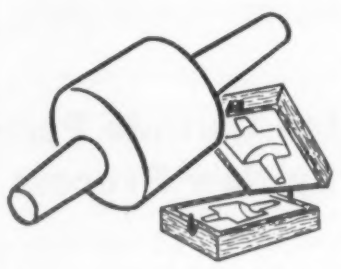
It is supplied as untrimmed, unmasked sheets in standard packages of varying weights, depending on thickness and size of sheets. The sheets are available in thicknesses of 0.187 and 0.250 in. and in the following sizes: 72 x 100, 84 x 84, 96 x 96 and 102 x 140 in.

(more What's New on p 248)

Is there a job for CO_2 in your plant?

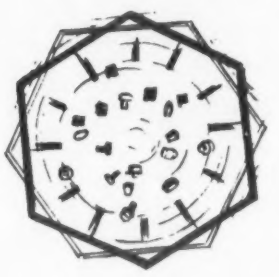
Almost every day another manufacturing or processing plant finds that carbonic gas can improve the product — simplify an operation — cut costs or increase safety.

The applications briefly discussed here are just a very few of the hundreds for which CO_2 is being used today. Some of these may be of direct interest to you, others may be adaptable to your field. If you'd like a broader list, we'll be glad to send you our booklet "CO_2 Applications Unlimited." Just check it on the coupon below. If you'd like detailed technical data on any of the applications listed in this advertisement check those in the coupon too.

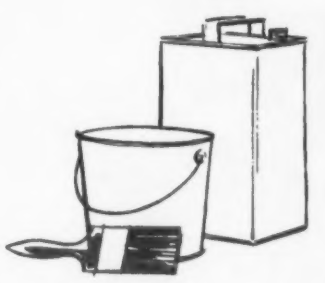


CURING CORES AND MOLDS FOR FOUNDRY CASTINGS—Ordinary foundry sand cores can be cured in 20 seconds flat, molds cured in an unbelievably short time. CO_2 gas reacting on a special sand binder gives an instantaneous chemical reaction . . . eliminates baking, gives sound, hard, perfectly formed cores and molds of any shape or size. CO_2 curing gives more accurate dimensions, too. CO_2 cured molds can be left for several days before pouring.

ECONOMICAL GAS SHIELDED WELDING—Costing only 1½ cents per cubic foot, CO_2 gas replaces expensive argon or helium gas in metal-arc gas shielded welding operations. Users report saving an average of seven cents per cubic foot of gas. Low-cost CO_2 also produces welds that are equal, or superior, to welds made with argon or helium gas. No expensive installations are necessary . . . present equipment can often be used "as is" or with modifications.



RUBBER TUMBLING—Flash or rind is quickly and smoothly removed from molded rubber parts by tumbling them in a CO_2 tumbling barrel. The parts are frozen with either dry ice or liquid CO_2, which is expanded directly into the tumbling barrel. As parts may be tumbled in large quantities, production costs are greatly reduced by this method over hand-trimming. Liquid also manufactures and sells the finest, most efficient, insulated tumbling barrel for this purpose.



PAINT AND VARNISH MANUFACTURE—Sparged up through the oils during the cooking process, CO_2 gas performs two important functions. Used in conjunction with conventional mechanical agitation, CO_2 sparging cuts oil cooking time as much as 60%. In addition to markedly increasing agitation, the CO_2, as it passes through the mixture, actually "sweeps" unwanted moisture along with it allowing the cooking mixture to reach a higher temperature. CO_2 is also used to advantage in the thinning, storage, filtration and other phases of paint and varnish manufacture.

INERTING—
There are many times when an inert atmosphere is needed to prevent fire or explosion. Before welding a tank that has been used for the storage of flammable liquid, CO_2 is used to inert the atmosphere in the tank so that welding can be done with no danger of explosion.

WEAK ACID—
CO_2 is used in the textile industry and many other applications as a weak acid for neutralizing.

FREEZE-DRYING—
Freeze-drying is used to dehydrate heat sensitive substances at low temperatures. In the manufacture of Pharmaceuticals dry ice is used to condense the moisture as it is sublimed under vacuum.

World's Largest Producer of

THE LIQUID CARBONIC CORPORATION

Chicago 23, Illinois

- ☐ Curing Cores and Molds
- ☐ Gas Shielded Welding
- ☐ Rubber Tumbling
- ☐ Paint and Varnish Manufacture
- ☐ Freeze-Drying
- ☐ Weak Acid
- ☐ Inerting

THE LIQUID CARBONIC CORPORATION
3172 South Kedzie Avenue • Chicago 23, Illinois

☐ Please send me a copy of "Applications Unlimited". I would also like more detailed information on the uses of CO_2 as checked.

Name _____

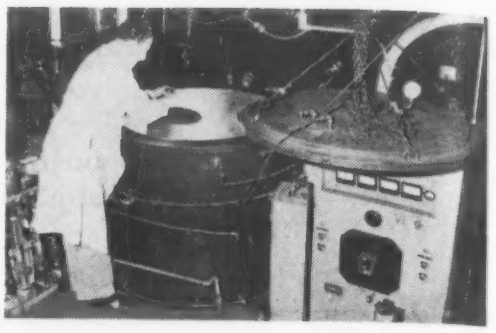
Title _____ Company _____

Address _____

City _____ Zone ___ State _____

For more information, turn to Reader Service Card, Circle No. 567

What's new IN MATERIALS



Vacuum sintering furnace *where complex carbide tool blanks are hardened.*

Tungsten Carbide Parts Made by New Process

Sintercast Corp. of America is using a new process to make intricately shaped, cemented tungsten carbide tool blanks that are said to be true-to-shape. The new process produces a part having uniform density in the presintered form so that after shaping and high temperature sintering it retains its shape and dimensional stability.

The pressing technique consists of three operations: 1) hydrostatic compacting, which applies equal pressure to the tungsten carbide powder from all directions; 2) projection grinding to produce exact shapes and precise dimensions; and 3) sintering in a vacuum furnace to harden the part.

Structural Efficiency of Steel 'Sandwiches'

New data on the structural efficiency of stainless steel sandwich plates is becoming increasingly essential as new developments in high speed aircraft and missiles rule out the use of lighter metals. Fabrication difficulties, which previously limited the use of this high strength cellular core material, have now been overcome and the only remaining question concerns the efficiency of the sandwich materials.

In Technical Note 3751 of the

UNICHROME
Trade Mark

News about
COATINGS for METALS
Metallic.....Organic.....Decorative.....Protective

Simple bronze plating process gives gold-like finish

- ***M&T copper-tin process deposits extraordinary, golden-glow decorative plate . . .***
- ***Also cuts need for nickel as undercoat***

BRONZE plating has proved itself a practical finish in large and small installations. The copper-tin process developed by Metal & Thermit eliminates usual difficulties and disadvantages in alloy plating. It is as easy to operate and control as normal processes depositing a single metal.

Equally important, this bronze can be deposited with brilliant 24K gold color by using a trouble-free brightener. Protected with a clear organic coating, it provides a high quality decorative finish with unusual appeal and long life. Overall cost of this bronze rivals that of copper and is less than that of a brass plate.

M&T Bronze gets the trophies. Golden-glow finish for die cast trophy cups wins over copper-nickel-gold formerly used by leading producer.

VALUABLE UNDERCOAT

As an undercoat, M&T Bronze has these qualifications: Good corrosion resistance; hardness better than copper and virtually equal to nickel; more ductility than nickel.

Undercoat-bronze can be plated semi-bright or matte. Both buff more readily than copper and with less chance of cut-through on edges.

OPERATIONAL ADVANTAGES

M&T Bronze offers better than twice the speed of fast copper plating solutions. There are numerous installations working at normal current densities of 60-75 amps per sq. ft. Densities of 100 amperes deposit over one-tenth mil a minute smoothly.

Golden-glow bronze delivers uniform color on intricate decorative work. So outstanding is its throwing power, it is being used to replace copper on complex automobile parts. It uses single anode circuits, and copper anodes which corrode uniformly. The tin is supplied by potassium stannate additions, assuring simple, economical control of the process.

For an unusual finish, both in appearance and protective function, the golden-glow M&T Bronze Process offers interesting possibilities to metal finishers and designers. Send for data.

New economy in chromate finishing

Several newly developed Unichrome Dip Compounds work at extreme dilutions. They offer chromate solutions with still lower make-up and operating costs than previously delivered by economical Unichrome Dips. These new Dips make it practical to preserve shelf life and appearance of galvanized, zinc plated or die cast items, even those having low unit price or narrow margin of profit.

MATCHED TO THE NEED

Unichrome Dip Solutions form corrosion-resistant finishes integral with zinc, improve and protect its eye appeal.

But chromate dips are active solutions which strip away zinc as well as convert its surface into an attractive but inactive film. As a result, the type of equipment used and the operating time or cycle affect results. The differing needs of manual or automatic finishing must be satisfied to produce the color, corrosion resistance, uniformity of finish—as well as the economy desired. Since no single chromate solution is equally suitable for all applications, many specialized Unichrome Dip Compounds are made available.

Metal & Thermit will gladly recommend the proper dip to meet specific needs. Simply submit details of product and requirements.

Unichrome is a trademark of Metal & Thermit Corp.

METAL & THERMIT
CORPORATION

General Offices: Rahway, New Jersey
Pittsburgh • Atlanta • Detroit
East Chicago • Los Angeles
In Canada: Metal & Thermit—United Chromium of Canada, Limited, Rexdale, Ont.

For more information, turn to Reader Service Card, Circle No. 555

What's new IN MATERIALS

National Advisory Committee for Aeronautics, Aldie E. Johnson, Jr. and Joseph W. Semonian present data comparing the efficiency of optimum-proportioned steel sandwich plates with that of solid plates of high strength steel, aluminum and titanium alloys when subjected to compressive end loads at temperatures of 80 and 600 F. Their tests showed that:

1. Comparative efficiency of a steel sandwich plate increases with decreasing core density at first, but as the core density is reduced below about 2% of that of the facing material, shear stiffness of the core becomes an important factor and finally results in a decrease in efficiency at higher loads. At low loads, little efficiency is gained by reducing core density below approximately 2% of that of the facing material. At high loads, core densities approximately 5% of that of the facing material are near the optimum.

2. At room temperature, it is possible to make steel sandwich plates that are more efficient than solid plates of titanium alloy over the entire loading range considered, and more efficient than solid plates of aluminum alloy over the lower part of the loading range. Steel sandwich plates maintain their advantage over solid titanium alloy at 600 F. At low loads the efficiency of steel sandwich plates is greater at 600 F than the efficiency of solid plates of aluminum or titanium alloys at 80 F.

3. The proportion of the weight of the core material in relation to the weight of the complete sandwich decreases with increasing loads. Except for low compressive loads, the core thickness in steel sandwich plates of efficient design is small; consequently, the weight of the core material is only a small percentage of the weight of the sandwich plate.

(more What's New on p 252)

NEW HAMMARLUND RADIO RECEIVER

FEATURES DIE CAST PANEL

CASE HISTORIES FROM MT. VERNON FILES

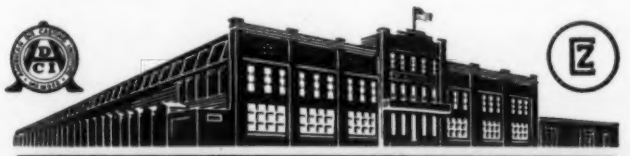
In their new HQ-100, Hammarlund Manufacturing Company brings to reality a completely new concept in receiver design. It is beautiful. It gives the radio amateur the utmost in performance. And it sells for far less than other comparable short-wave receivers.

A chief reason for this great economy is the front panel—the first die-cast panel in the history of commercial radio equipment. This 3-dimensional, channeled die-cast aluminum panel is used because it affords both rigidity and great structural strength. To produce its equivalent in sheet metal —the currently used method in the industry—*would cost 4 times as much.*

This remarkable panel is the result of thorough collaboration between Hammarlund and the die-making experts at Mt. Vernon, who made practical suggestions which simplified its design.

In addition to the production economies of die casting, the panel benefits from these other important advantages: (1) Die casting's inherent accuracy enables Hammarlund to assemble the chassis with what they call "camera precision construction." (2) All rejects on the production line are eliminated. (3) In finishing—die casting enables them to work out clearly divided areas for the elegant two-tone treatment that is both functional and beautiful. Also, the amount of finishing is minimized.

When you are out to break precedent, as Hammarlund did, you too can find the kind of skilled help you need in the complete service available from Mt. Vernon's coordinated designing, die-making, casting, and machining facilities, all under one roof, which can supply die cast zinc and aluminum parts ready for use. A switch to a die casting service like ours may be your next step. Let's discuss it.



MT. VERNON DIE CASTING CORP.
STAMFORD, CONNECTICUT

SALES REPRESENTATIVES

Mr. Grant Eller
6 East 194th St., Cleveland, Ohio

Mr. Jerome J. Theobold
9 East Genesee St., Skaneateles, N. Y.

Mr. Arthur Diamond, Tools Incorporated
86 Bethlehem Pike, Philadelphia, Pa.

Mr. Anker Anderson
Cascade Road, Stamford, Connecticut

Mr. William Sauers
101 Briarcliff Road, Rochester, N. Y.

Mr. David King
230 Grant Boulevard, Syracuse, N. Y.

Mr. George E. Hahl
39 South Munn Ave., East Orange, N. J.

For more information, turn to Reader Service Card, Circle No. 380

What's new IN MATERIALS

Small Teflon Tubing for Electronic Parts

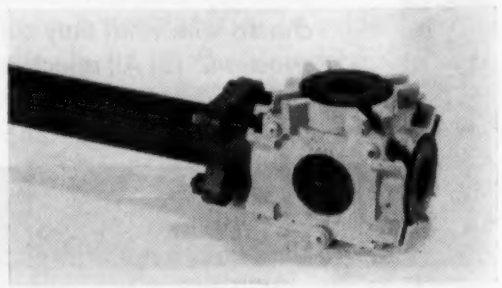
Teflon spaghetti tubing, available from Polymer Corp. of Pennsylvania, Reading, Pa., is now being produced in AWG wire sizes of 0, 1, 2, 3, 4, 5, 6, 7 and 28 and 30. Known as Polypenco tubing, it is used as a low and high frequency insulation sleeving for electronic parts. It has a minimum dielectric strength of 750 V per mil, a dielectric constant of 2.0 and a surface resistivity above 10^{12} ohms per cu cm. All sizes are available in ten coded colors for circuit identification.

Glass Fabric Covering Used on Graphite Pipe

Carbon and graphite pipe and fittings are now available with an external glass fabric covering. The covering strengthens the pipe, holds line pressures and prevents leakage in case of pipe breakage. Called Karbate armored pipe, it is available from National Carbon Co., 30 E. 42nd St., New York 17, N. Y. in 1 to 4-in. dia and lengths up to 9 ft, with either flanged or plain ends. Armored fittings are available as 90-deg elbows, tees, couplings and flange collars.

The carbon and graphite pipe and fittings are corrosion resistant and are free from metallic contamination. They are also resistant to thermal shock and easy to install.

(more What's New on p 254)



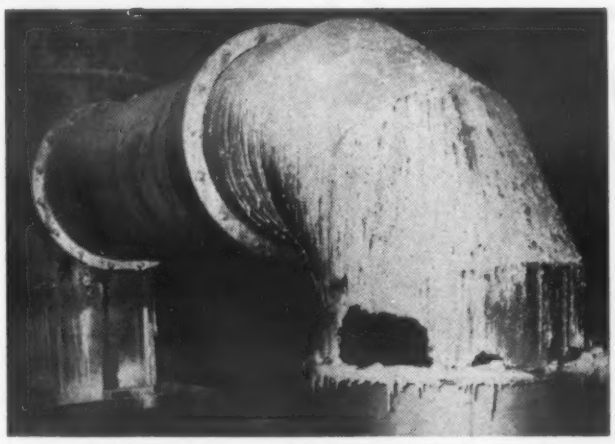
***Metal housing** protects graphite fitting from external mechanical stresses.*

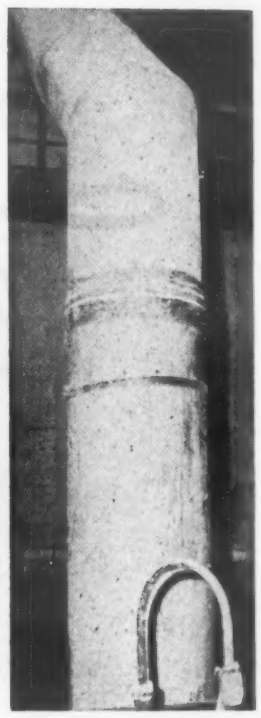
CYANAMID

PLASTICS NEWSFRONT

THREE YEARS IN CORROSIVE SERVICE WITHOUT MAINTENANCE

That's the record established by reinforced LAMINAC® polyester resin in venting service on alum digesters at Cyanamid's Warners plant. The carbon steel breech (left) in an alum evaporator required frequent maintenance, failed after less than three year's service. Glass-reinforced LAMINAC stacks (right) in even more severe alum digester service, have needed no maintenance in more than three years. The LAMINAC units cost less in the long run, and were easier to erect and assemble, using either telescope joints wrapped and polyester-welded on the site, or flange-type joints.





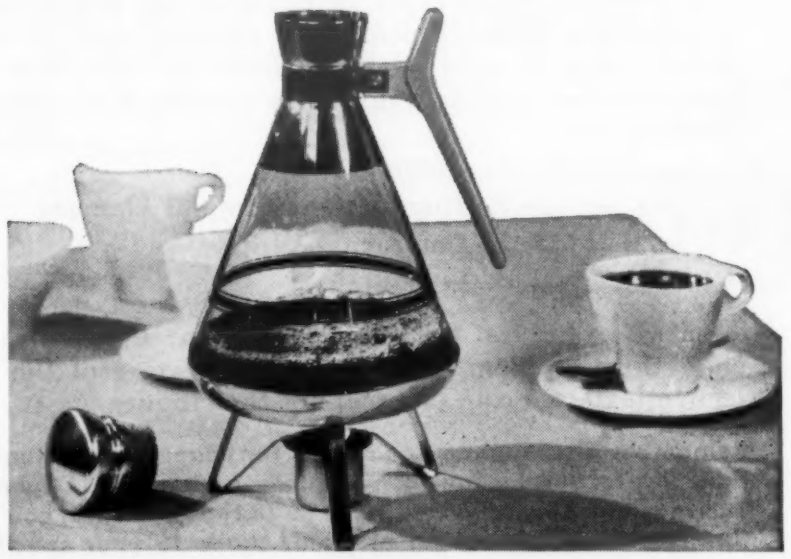
ATTRACTIVE, AIRTIGHT CASE FOR STICK COLOGNE

Six new scents of Avon Stick Cologne are packaged in smartly styled, practical cases molded of BEETLE® urea molding compound. Cases have a white base with contrasting closures in a different color for each scent. Airtight, the BEETLE case stops evaporation of the cologne. Yet the closure opens easily, and with a twist of the wrist the stick pops up for use. The case resists alcohol, essential oils and chemicals as well as staining from perspiration and grime, which wipe off easily.

FUNCTIONAL HANDLES GRACE CARAFES

Any dining or buffet table would be graced by this attractive carafe with its stylish, beige-colored handle molded of CYMEL* melamine molding compound. Elegance and function are combined in the handle, balanced for easy, comfortable pouring. Harmonizing with the carafe's gold decoration, the molded-in color won't chip or wear off. In keeping with its function, CYMEL is exceptionally strong, resistant to heat and flame, and stays cool even when the carafe, made by Club Aluminum Products Company, is full of hot coffee.

*Trademark



AMERICAN CYANAMID COMPANY
PLASTICS AND RESINS DIVISION
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CYANAMID Plastics and Resins Division
MATERIALS FOR TOMORROW

For more information, turn to Reader Service Card, Circle No. 497

What's new IN MATERIALS

Laminate, Aluminum Used in Panel Board

A panel board material consisting of a thermosetting plastics laminate sheet bonded to aluminum has been introduced by Panellit, Inc., 7401 N. Hamlin Ave., Skokie, Ill. It is recommended for control room panels including conventional large case and large case graphic panels, and miniature graphic panels.

According to the producer, the material permits reduction of time, effort and cost in revising panels in the field. Other advantages are resistance to scratching and denting, reduction of panel weight and good appearance.

Colored Oxide Finishes for Copper and Brass

A new oxide finish for coloring copper and its alloys has been developed by Enthone, Inc., 442 Elm St., New Haven, Conn. Called Enthocolor 220, the finishes are applied by immersing parts in a solution of an alkaline salt mixture for periods of 1 to 15 min at temperatures of 180 to 225 F. The process gives brown and shiny blue-black coatings on almost all copper alloys. Brown colors can be produced on copper and brasses; blue-black colors can be produced on brasses containing 20% or more of zinc. Unlike sulfide finishes, the new oxide finishes do not spot and can be severely deformed without cracking.

Glass Flake Paper for Electrical Parts

Transparent, colorless glass flakes averaging 0.25 x 0.25 x 0.0003 in. in size have been successfully converted into a paper-like product by T. D. Callinan

New Rokide* Coatings Resist Heat and Abrasion

Rokide spray coatings help solve many high temperature and wear problems

WITH the rapid increase in modern high temperature applications there has been a corresponding increase in demands for resistant materials. Norton ROKIDE spray coatings are meeting such demands with great success. These hard, adherent crystalline refractory oxides offer many important advantages. For example:

They are both thermally and electrically insulating . . . Their hardness, chemical inertness and stability in combustion temperatures provide high resistance to excessive heat, abrasion, erosion and corrosion. Their high melting points and low thermal conductivities reduce the temperatures of the underlying materials and permit higher operating temperatures.

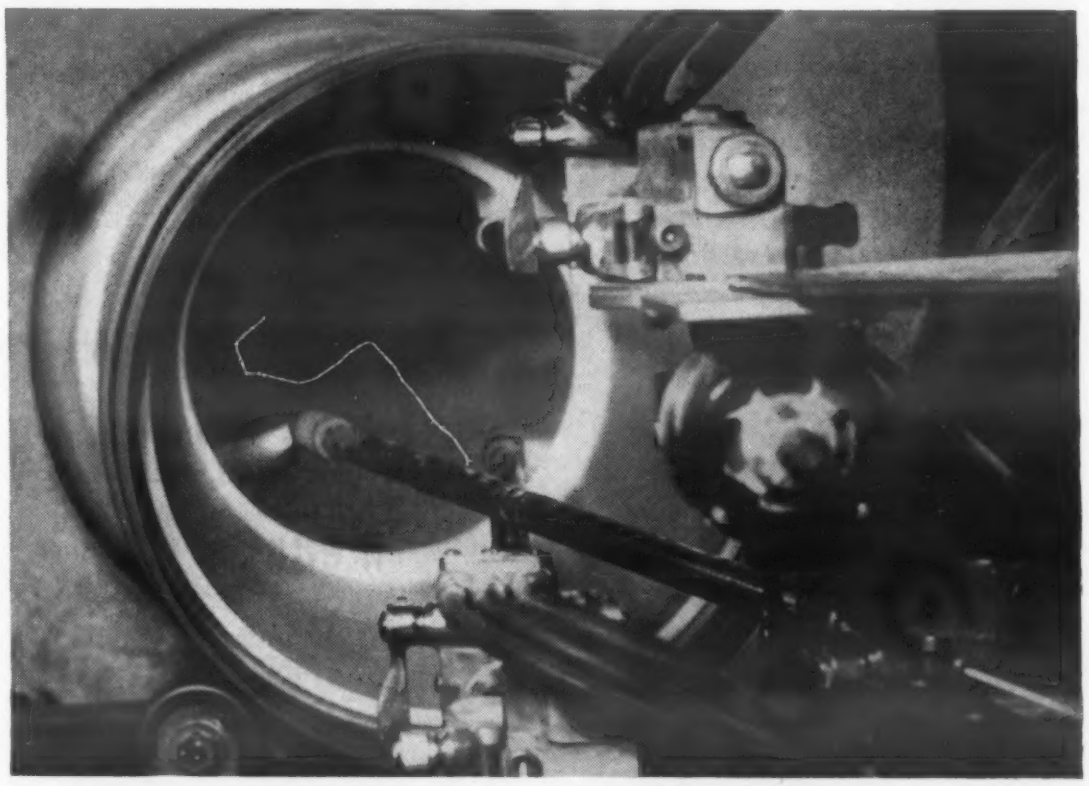
ROKIDE Coatings vs. Stainless Steel

Analyses of Norton ROKIDE spray coatings and of stainless steel reveal interesting comparisons. While less dense than the bare steel, the ROKIDE coatings are very much harder, have considerably higher melting points and are very much lower in thermal conductivity and thermal expansion.

Proof

There are three Norton ROKIDE coatings: ROKIDE "A" aluminum oxide, ROKIDE "ZS" zirconium silicate and ROKIDE "Z" stabilized zirconia. These have been proved in such critical applications as reaction motors, as well as in AEC projects.

ROKIDE spray coatings are also helping to solve industrial problems involving: Electrical insulation • Thermal barriers • Electronic applications • Bearing surfaces • Erosion protection • Corrosion retardation • Chemical barriers • Positioning medium • Material up-grading • Altering emissivity and characteristics of surfaces • Surface catalytic activity • General wear resistance.



ROKIDE Spray Coatings are applied in a molten state by means of a metalizing type spray gun*. The oxide is fed into the gun in rod form at a carefully controlled rate. The coatings can be applied to parts of any size and to all shapes accessible to the spray gun equipment. Multiple gun set-up shown in illustration.

Although ROKIDE coatings are most commonly applied to metals they are effective on other materials, such as ceramics and certain plastics. Thicknesses of the coatings generally range from .005″ to .05″.

For more detailed information on ROKIDE coatings, write to: **NORTON COMPANY,** ***New Products Department,*** Worcester 6, Mass.

NORTON

NEW PRODUCTS

Making better products... to make your products better

*Trade-Mark Reg. U. S. Pat. Off. and Foreign Countries

Facilities for applying ROKIDE coatings available at:
NORTON COMPANY
Worcester, Massachusetts
and
2555 Lafayette Street, Santa Clara, California

* Manufactured by Metallizing Company of America, Chicago 32, Ill.

What's new IN MATERIALS

PROPERTIES OF IMPREGNATED GLASS PAPER

Properties	Impregnants		
	Alkyd	Phenolic	Silicone
Resin Content, %	39	40	55
Density, gm/cu cm	1.14	1.16	1.74
Ten Str, psi	900	1800	700
Water Absorp, %	0.4	1.5	0.0
Dielec Const (10,000 cps)	2.30	1.69	1.80
Power Factor (10,000 cps)	1.69	0.25	0.20
Dielec Str, v/mil	100	120	105
Volume Res, ohm-cm	10^{13}	10^{13}	10^{13}

and R. T. Lucas, of the U. S. Naval Research Laboratory. (See also article on glass fiber paper, M&M, Dec '55, p 99.) The two researchers seem to think that the physical and electrical characteristics of glass flake products tested by them justify pilot and mill trials of glass flake paper.

Details of glass flake preparation and a discussion of the properties of glass flake paper are contained in the Oct '56 issue of the *Journal of the Electrochemical Society*.

Making glass paper

The glass flake paper used in the evaluation was made on a laboratory scale by blending glass flakes in a water and acid solution to a fine and dispersed pulp. The pulp was then placed in a standard sheet mold where a uniform, porous, brittle and transparent sheet approximately 10 mils thick was obtained.

The glass flakes used in the manufacture of the paper-like product were a borosilicate glass, type E (10 boron oxide, 54 silicon dioxide, 16 calcium oxide, 16 aluminum oxide and 5% sodium and potassium oxide) that softens at 1544 F. The flakes were made by rapidly cooling a thin film of molten glass that shattered into fine particles.

The transparent sheet made of the glass flakes had a glass content of 100% and a thickness of 0.010 in. Tensile strength of this

This composite picture represents 100 Richardson tool and die men with a combined experience of 12 centuries.

. . . . better molded parts because of

1200 years of tool and die experience

At least 50% of getting a good molded part depends on the quality of your mold.

The composite photo shown to the left represents the broad and varied experience needed for the design and production of quality molds to close tolerances . . . it represents 100 Richardson men with more than 1200 years combined experience in the design and production of tools and dies for the production of molded plastic parts.

The men who make Richardson molds know and respect the many "ifs" encountered in the design and production of quality molds. They know that . . .

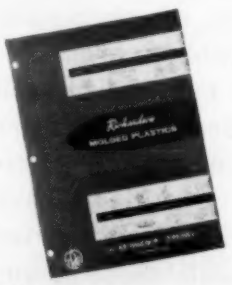
. . . if your mold isn't correctly designed, the resulting parts will not be according to specifications.

. . . if your mold is not properly designed, the parts cannot be ejected quickly, production speed will be reduced, and unit cost increased.

The Richardson mold and die shop at Melrose Park, Illinois, is one of the largest in the plastics industry.

. . . if your mold walls are not of uniform thickness, curing time is increased.

. . . if your mold is not properly designed, resulting excessive flash must be removed by hand . . . a costly procedure.



Richardson engineers can assist your engineers in (1) redesigning parts for conversion from other materials to molded plastics, and (2) designing to improve molded parts now in production.

For additional information and a copy of the newly published catalog, "Richardson Molded Plastics," write or phone, today . . . Chicago number, MAnsfield 6-8900.

The RICHARDSON COMPANY

MOLDED AND LAMINATED PLASTICS

. . . better plastics for better parts

Dept. 17, 2782 Lake St., Melrose Park, Illinois

For more information, turn to Reader Service Card, Circle No. 472

What's new IN MATERIALS

material was 86 psi and density was 0.75 gm per cu cm. The material had a Mullen burst number of 1 and an Elmendorf tear strength of 20 lb.

Resin impregnation

Although the glass flake product was self-supporting, it was difficult to handle without a binder. Thus, three resins were studied as impregnants for the glass material: an alkyd varnish (GE 1202), a phenolic enamel used in motor insulation (Du Pont 8995 Formvar), and a silicone (Dow Corning 993). The glass paper was readily saturated and, on drying, yielded mechanically strong, water resistant, transparent dielectric sheets.

The impregnated papers were air dried for 16 hr, then subjected to a temperature of 250 F for 8 hr. The silicone-impregnated paper was heated 16 hr longer than the alkyd and phenolic-impregnated papers.

All impregnated papers had substantially greater tensile strength, density, dielectric constant and water resistance compared to the nonimpregnated papers. Physical, mechanical and electrical properties of the impregnated glass papers are given on page 256.

Modified Butyl May Be Used in Tires

Several hundred automobile and truck tires made of chemically modified butyl rubber are presently undergoing exhaustive road tests. The modified butyl rubber has less heat build-up than previous butyls and is said to have resilience and strength properties approximately double those of unmodified butyl.

The new rubber is made possible by a chemical modifier, called Elastopar, now being produced in semicommercial quantities by Monsanto Chemical Co. It is added to butyl rubber in the course of conventional processing

Grandmother-

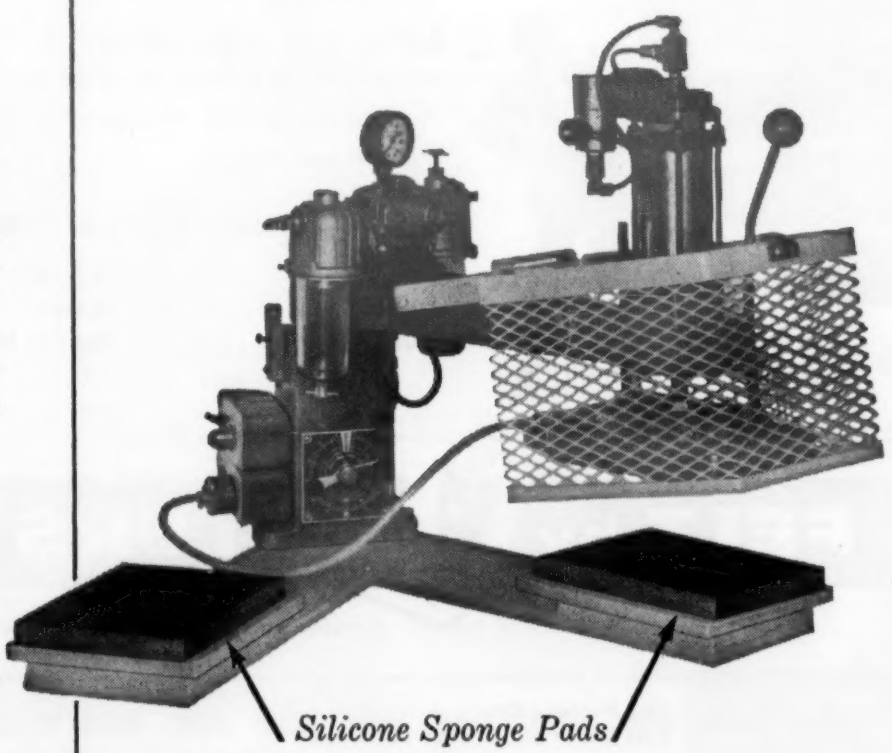
YOUR PATCHING DAYS ARE OVER...

ROTH developed silicone sponge rubber pads solved heat and pressure adhesion problems of commercial patcher

High heat and high pressure are required to melt the adhesive and to make a lasting seal in commercial patches used in the overall and uniform supply industry. An automatic patching machine had been developed for this purpose but production was held up as patches were not getting the proper adhesion . . . particularly over seams and under buttons.

ROTH RUBBER Technical Knowledge and Experience developed a silicone sponge that would withstand the 400°F. temperature required and the 80 pounds per square inch pressure. Not only does a pad of this Roth silicone sponge withstand this pressure and temperature but it retains its resiliency over thousands of patching cycles.

The American Heat Seal Patching Machine, manufactured by American Heat-Seal Inc., Chicago, provides complete safety for the operator and automatically controls time, temperature and pressure for applying "Stay On" patching material. For faster output, two pads of Roth developed silicone sponge are used and the operating arm of the machine is swung from one pad to the other.



IF YOURS IS A PROBLEM IN RUBBER...LET ROTH'S EXPERIENCE WORK FOR YOU

Write for technical data on Roth developed silicone sponge and molded silicone rubber parts

ROTH RUBBER COMPANY Division of Vapor Heating Corporation
1860 South 54th Avenue • Chicago 50

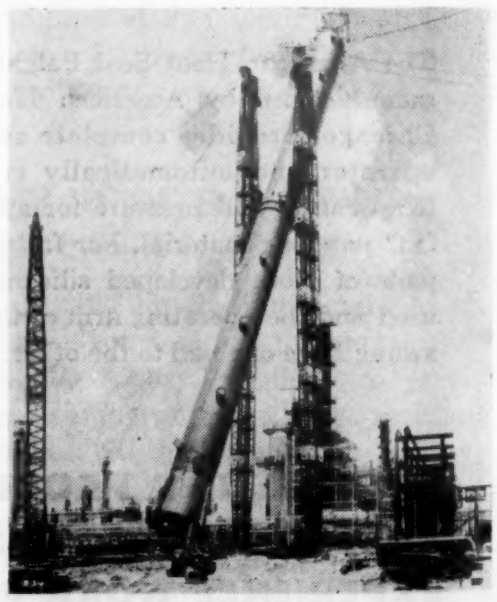
For more information, turn to Reader Service Card, Circle No. 439

steps and is said to provide all of the benefits of a long heat treatment during a normal mixing cycle. It also gives easier mixing and smoother, faster extruding and calendering.

Improved Hot Strength in 302 and 316 Steels

For some time alloy producers and jet engine manufacturers have exhibited interest in the possibility of using leaner alloys for aircraft production. One approach has been to add titanium and boron to 302 and 316 stainless steels in order to improve their hot strength.

J. Salvaggi and L. A. Yerkovich, of Cornell Aeronautic Laboratory, have evaluated the 100-hr rupture life at 1500 F of a substantial number of such compositions prepared as 15-lb heats and rolled to approximately 0.050-in. sheet. Although the nominal 100-hr rupture strength at 1500 F is in the 5000-9000 psi range for the



Fractionating tower—This massive tower was fabricated in a single piece from 1-in. thick steel plate. Believed to be the largest ever built, the tower is 21 stories high, weighs 410,000 lb, and has an 11-ft, 8-in. dia. It was built by Delta Tank Mfg. Co. for Esso Standard Oil Co.

"Customer Savings" is the Reason 1956 was the Best Year in Setko's 20-Year History

Set Screw News
& Mfg. Co.

We specialize in Solving Puzzling Set Screw Problems

Issue No. 4 — Bartlett, Illinois — EXTRA!

SPECIAL SET SCREWS SAVE One Manufacturer $42,000

. . . Another $35,000 . . . and Another SAVED the ENTIRE COST OF SET SCREWS

These and similar *savings* are being accomplished by using special type Setko Set Screws to overcome costly difficulties such as vibration . . . close-precision setting . . . fastener-failures . . . floor loss . . . or to obtain production set-up (increases up to 10 times) and screw inventory reduction, etc. Let us show you how we can Save YOUR Plant Some Real Money in 1957 with Set Screws designed to solve *your* particular problems. Use coupon below to get Test Samples.

SETKO

A Score of Manufacturers Find Hopper-Feeding Pays for Itself...then goes on SAVING

In the first year of its operation, a number of manufacturers report that savings from Hopper-feeding of various type set screws have already paid back cost of installing special mechanism. Because it requires 1/5 to 1/10 former time, eliminates cross-threading, rejects misfits, etc. Use on metal or plastic products. Let us send you list of users and arrange for special Hopper-Feeding Demonstration at our plant. Check Coupon Below.

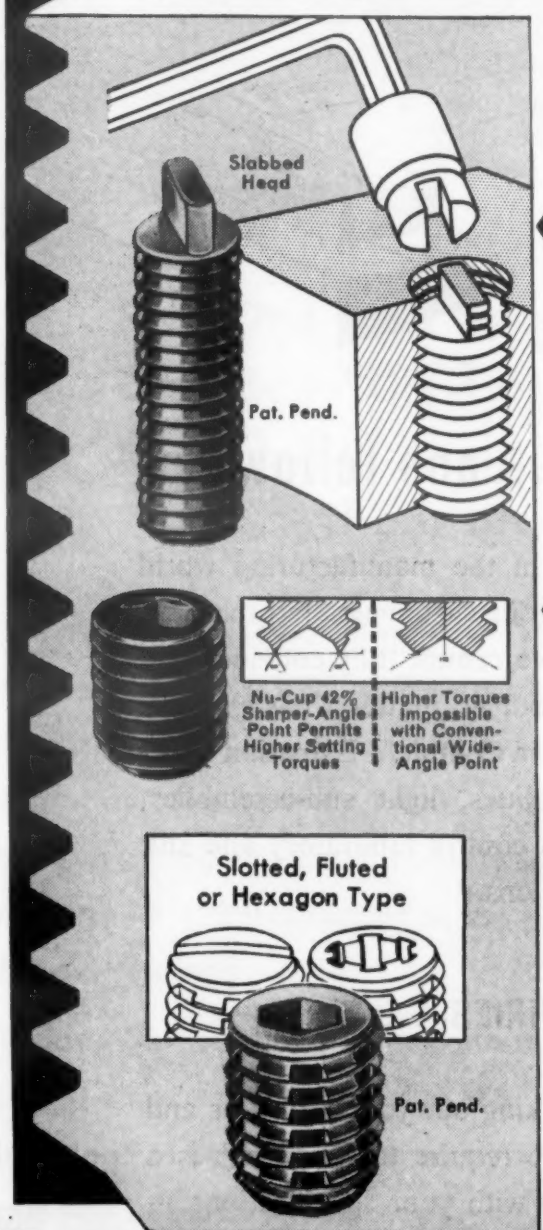
SETKO

Learn How To Get MONEY-SAVING Jewel Case of Set Screw Ideas

Over 30 different actual Setko Set Screws and Socket Keys sent on loan, to those responsible for specifying or ordering set screws. Send for Bulletin giving full details.

Check "Jewel Case Bulletin" on Coupon.

Such SAVINGS were made possible by New Type SET SCREWS like these



Here are only a few of the more than 30 different kinds of Setko Set Screws that can save you money. Send for full details; check on coupon below, space marked "Jewel Case Bulletin."

Flush-Lok Self-Locking Set Screws

Effect *Savings* of 25 to 50%

For use where "flush" insertion is desired; made with an undersized slab; can be set to same holding power as equivalent size socket screw, at 25 to 50% less cost.

SETKO

This screw and others can be supplied with NU-CUP POINT for *Greater Holding Power.*

Saves Money by eliminating costly slippage, cracked screw heads, etc. Proved by actual comparison Test.

SETKO

Multi-Fluted Self-Tapping Set Screws

Cut Costs . . . Save Taps . . . Save Time

Additional cutting edges make tapping easier, produce better thread. Especially good on plastics applications. Complete size range includes smaller sizes. For full details check "Jewel Case Bulletin" on coupon below.

Fill Out and Mail Coupon Now.

1321R

☐ Hopper-Feeding
☐ Test Samples (To meet our problem described on separate sheet.)
☐ "Jewel Case" Bulletin
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Set Screw & Mfg. Co. 149 Main St., Bartlett, Illinois
I am interested in *Saving Money.* Please send me information or materials on subjects checked in column at left.

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ADDRESS..... CITY..... STATE.....

For more information, turn to Reader Service Card, Circle No. 545

What's new IN MATERIALS

conventional steels, values of 18,000-20,000 psi were obtained for several of the titanium and boron modifications of these alloys. A number of alloys demonstrated similar gains at 1350 F. Other conclusions resulting from this work originally presented at the 38th annual convention of the American Society for Metals, are:

1. Titanium, boron and carbon are all capable of improving the 100-hr, 1500 F rupture strength of type 302 and 316 stainless steels heat treated in the range of 2100 to 2300 F. Rupture ductility remains good and in most cases is better than that obtained for base compositions solution treated at these temperatures.

2. For the range of compositions studied, maximum high temperature strengths increase as carbon levels are raised. The largest strength increment occurs between 0.07 and 0.15% carbon. Rupture ductility is relatively unaffected, particularly in alloys containing combined titanium and boron additions.

3. High temperature strength of the modified type 316 stainless steels is superior to that of the modified type 302 steels under similar conditions of heat treatment and at similar titanium, boron and carbon levels.

4. When titanium and boron are added jointly to type 302 and 316 stainless steels, peak 100-hr rupture stresses occur at progressively lower titanium contents as boron increases.

5. Maximum rupture strengths of stainless steels containing titanium and boron as single additions and also in combination are greatly improved, in most cases, by utilizing higher heat treating temperatures. These gains are generally accompanied by a decrease in rupture ductility. This decrease in ductility is not as pronounced for the boron-bearing steels as it is for the steels containing titanium alone.

(more What's New on p 268)

The Zinc that originally put Zinc-Base Die-Castings on a High Level . . . and has kept them high!

BUNKER HILL ZINC, when its 99.99+ quality came into the market back in 1928, quickly proved to be a boon to the die-casting industry. It enabled die-casters to take full advantage of the inherent merits of zinc-base castings. Bunker Hill pioneered this basic change in the development of the industry. It is still a leader in the production of quality zinc for die-castings.

Today, the die-caster who wants the best is able to get the purest zinc available—Bunker Hill. If you would be interested in *trying out* Bunker Hill, let us know your requirements. We'll put you in touch with a small tonnage supplier.

Eastern Sales Agents

ST. JOSEPH LEAD COMPANY • 250 PARK AVENUE, NEW YORK 17, N. Y.

BUNKER HILL 99.99+% ZINC

Sales Office for Pacific Coast

THE BUNKER HILL CO. • 660 MARKET STREET, SAN FRANCISCO 4, CALIF.

What's new IN MATERIALS

Cementable Tapes for Insulation, Linings

A line of cementable glass-reinforced and unsupported Teflon tapes has been announced by Continental Diamond Fibre Corp., Newark, Del. Both the reinforced and unsupported tapes can be bonded with ordinary adhesives to metal, plastics, glass, wood, ceramics and rubber. They are produced in widths from ¼ in. to 12 in. and in thicknesses from 0.002 to 0.060 in.

The tapes may be used as coil and motor winding insulation, noncorrosive linings, facings for conveyor belts, and duct linings.

Nylon Fabric Used in Inflated Warehouse

A pneumatically supported warehouse made of paper-thin, vinyl-coated nylon fabric, has been developed by U. S. Rubber Co. The building, 80 ft long, 40 ft wide and 20 ft high, contains more than 64,000 cu ft of storage space and can be erected by three men in 1 hr.

It is erected with air from a compressor. The compressor maintains a constant stream of low pressure air which enables the building to keep its shape and taut appearance.

The vinyl-coated nylon material, called Fiberthin, weighs 8 oz per sq yd and is resistant to scuffing, sunlight, oils, gasoline, most acids, alkalis and salt water.

***Portable warehouse** is large enough to hold two million pounds of packaged goods.*

PRICES AND SUPPLY

The Outlook by Herman B. Director, *Consultant, Washington, D.C.*

Steel production to continue at a high rate

Steel production has not dropped below 95% of capacity since the work stoppages last summer. This can be attributed to several factors: 1) even when the automotive industry sells less than six million cars, as it did in 1956, it still consumes almost 14 million tons of steel; 2) production of heavy products, such as structural and plate, now accounts for over 16% of total mill shipments, compared to 14% in 1955; and 3) a careful study of what actually happens to the 20%, or 18 million tons, of steel shipped to warehouses shows that, contrary to AISI figures, the construction industry consumes not 12% of steel shipments but closer to 15%. Similarly, the machinery industries consume about 16%, rather than AISI estimates of 9%.

Steel industry expansion is directed toward heavy products; of the $2 billion which the steel industry has indicated it is prepared to spend on expansion, almost $800 million will be used for further expansion of structural and plate capacity. This increase in capacity should be ready in sufficient time to meet the expanding needs of highways, freight cars and ships. In fact, we are quickly catching up with the freight car backlog. The highway program is slow in expanding due to legal and financial problems, but the shipbuilding program, which will require a very large portion of its heavy steels sometime beginning in late 1958 and on through 1960, should have its needs met without much difficulty.

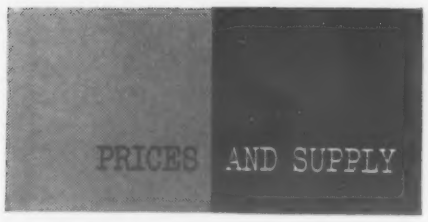
Pressure on Government to purchase copper

Copper prices continue to fall. However, U.S. producers are reluctant to drop the price in the face of Chilean dependence on U.S. markets. This accounts for the recent two-stage drop, i.e., from 36¢ to 34¢ and then to 32¢ per lb. As soon as the market dropped to 32¢ per lb, custom smelters lowered their price to 31¢. This foreshadows a further drop in price to 31¢ per lb by U.S. producers. When the producer price reaches 31¢ per lb, there will be increasing pressures for the U.S. Government to bolster the market. This will be accomplished in two ways: 1) domestic producers with Government contracts to deliver copper to the Government at 31¢ per lb or higher will deliver to the Government; 2) the Commodity Credit Corp. will be under strong pressure to put copper on its list of materials desired for barter.

Pressure on the Government to go into the copper market is, in fact, beginning to show up in some unusual places. The *Waste Trade Journal*, in an editorial on Jan 19, makes a case for the Government to enter the market and begin to buy copper which is in excess of demand. We wonder whether this plea for the purchase of copper on the part of the secondary industry is not designed to set the stage for a program which will urge the Government to buy secondary ferrous materials in the event they too become surplus. We are mindful of the 1954 situation when, in the face of declining prices for scrap iron and steel, the secondary industry urged the Government unsuccessfully to stockpile metal scrap in order to bolster the scrap market.

Attempt to cut mineral subsidy fails

The House of Representatives cut $30 million from its appropriation for the purchase of asbestos, columbium-tantalum and fluorspar. The Senate, in acting on the same appropriation bill, promptly restored these funds for a continuation of mineral subsidies. In support of continuation, Felix Wormser, Assistant Secretary for Mineral Resources, Dept. of the Interior, said he favors continuation of the subsidy until such time as the Government acts in favor of increased tariffs on zinc, lead and other materials in order to protect domestic producers. He stated categorically that these materials were not needed by the Government for its stockpile program and emphasized the fact that until tariff protection is afforded, he



must continue to support a subsidy program as a less desirable alternative.

With regard to these materials, we would like to point out that there are abundant supplies of columbium-tantalum; all domestic tungsten goes to the Government and commercial needs are met from foreign sources; asbestos has more than met its match in fiberglass for strategic applications; and there is an abundant supply of fluorspar. The net result, of course, is that domestic consumers, in addition to paying their share of the subsidized price via the tax route, must also pay higher prices for the materials they consume.

Price cutting in aluminum extrusions

All producers of extruded aluminum shapes used largely in storm windows, doors and decorative hardware are engaged in price cutting competition. This struggle is attributed to the fact that after an extremely rapid growth following the Korean War, the industry has 100 companies competing for business at a time when growth of residential housing is at a low point. As a result, extrusions are available in the market at 10¢ per lb less than the 60¢ list price.

Zirconium comes of age

Zirconium production is now reaching a level of commercial availability. In addition to the widely publicized applications of zirconium for atomic energy, zirconium-containing alloys are being used in such nonstrategic applications as flatware and dinnerware on board ships.

Shortage of pure tantalum and columbium

The demand for pure tantalum, used in electronics equipment, exceeds the supply. This situation will exist for the next two years, even though the major producer of tantalum is expanding his plant and four other companies are toying with the idea.

The situation with regard to pure columbium is similar. Demand for pure columbium for heat exchangers and other process equipment exceeds the supply. Furthermore, expansion of facilities for the production of pure columbium appears to be lagging behind expansion of facilities for pure tantalum.

Reinforced plastics consumption continues to grow

Reinforced plastics consumption, which increased in 1956 to 140 million pounds—30% over the previous year's figure—will probably increase again in 1957. However, the increase will not be so spectacular.

Production of low pressure polyethylene up

In 1957 high density (low pressure) polyethylene capacity should increase to about 100-150 million pounds. This material is far superior to low density (high pressure) materials for such applications as wire and cable insulation. In some cases it will supersede conventional polyethylene as a cable covering, and it might even replace conventional polyethylene as a jacketing material over lead.

Selenium, bismuth prices to drift lower

Demand for selenium, mercury, bismuth, platinum and rare earths, though at a reasonably high level, will not put a squeeze on the supply. Export restrictions on these materials have been progressively relaxed and are, in effect, restrictions in name only. We expect the prices of these materials to continue to drift downward. In the case of mercury we expect the price to drift down to the Government purchase price of $225 per flask, as compared to the current market price of $255.

Nickel supplies to increase somewhat

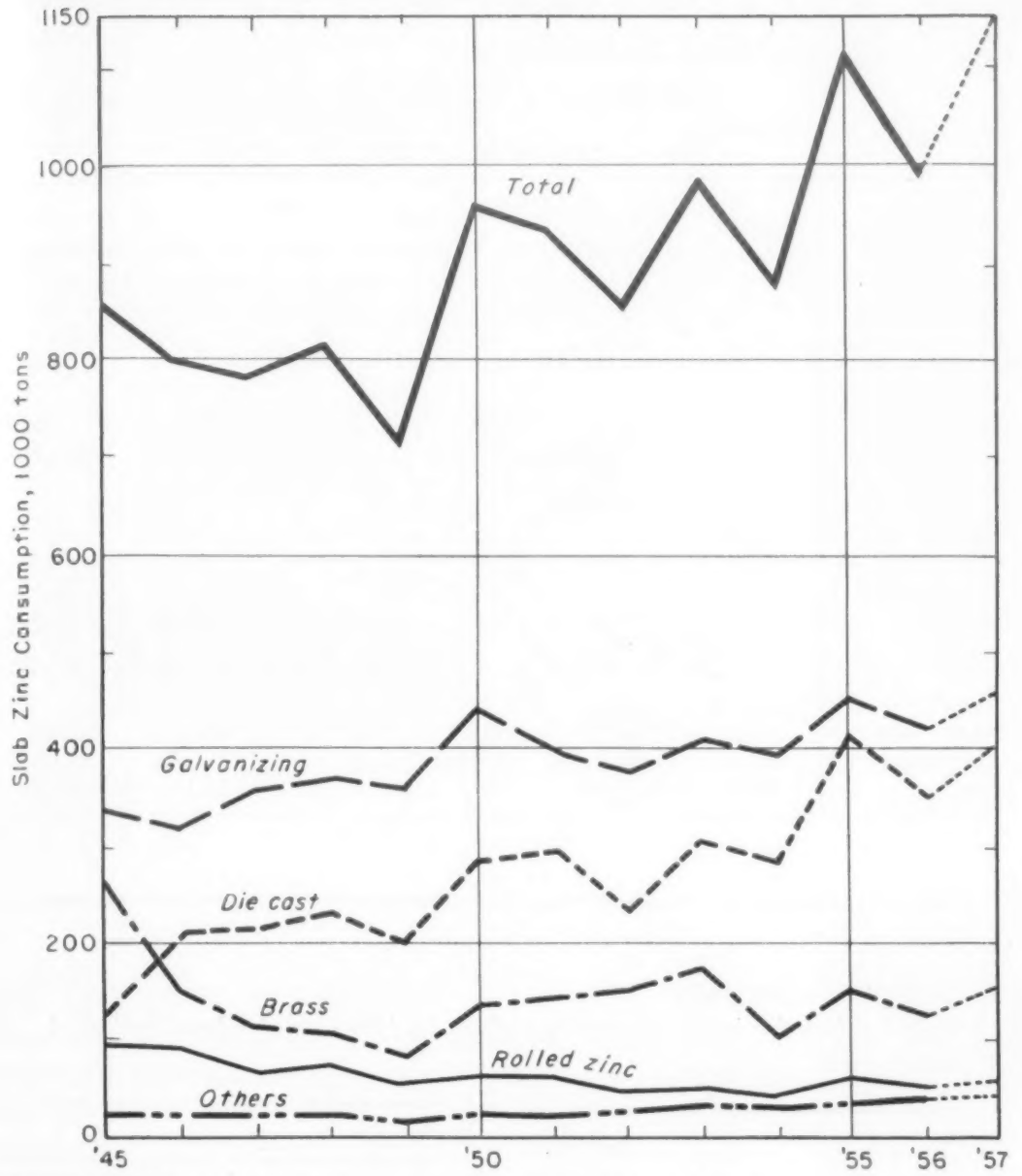
If the defense program does not require more nickel than it is currently using, additional supplies should become available to civilian consumers during the second quarter. Recent arrangements concluded by the Government will provide market-price nickel to small consumers who use 100 lb of nickel per month. Larger consumers will benefit from increased supplies of high price nickel which the Government has arranged to divert from U.S. account to industrial consumers. The current outlook, however, is that all consumers will still be willing to build inventories now virtually nonexistent, at prices above the 74¢ base price for nickel.

Tin price remains firm

The International Tin Council, which controls supplies and prices of tin, is expected to turn down Bolivian proposals to increase the price. The Tin Council purchases tin in the event price drops below a fixed level. The U.S. buys about 50% of the world's tin and, though not a member of the Tin Council, has maintained a very close liaison with this organization. Members of the Council are shying away from the Bolivian proposal unless it can be demonstrated to the satisfaction of the United States that price increases are actually required.

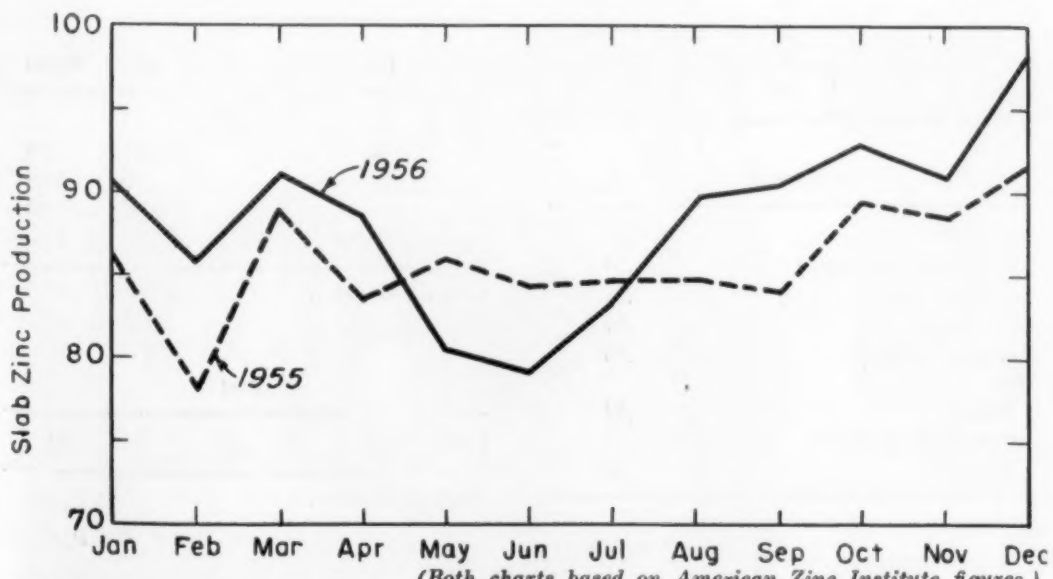
On the other side of the picture, work stoppages in Malaya have prevented tin prices from decreasing. It was originally anticipated that tin ores normally coming to the Texas City tin smelter would enter world markets, increase the supply and result in reduced tin prices.

Insofar as smelting facilities are concerned, there has been a fairly easy and successful transition from use of the Texas City facilities to other facilities available in Western Europe, including Holland, Germany and the United Kingdom. The extremely high production rate of tin plate here in this country should keep tin prices firm.



Consumption *of slab zinc by industry, from 1954 to 1957.*

Production and Use of Zinc Expected To Be Highest in '57



(Both charts based on American Zinc Institute figures.)

Comparison *of zinc production (1000 tons) in the last two years.*

■ Domestic smelter production of slab zinc during 1956 reached an all-time high of 1,062,955 tons. This represents a 3% increase over the industry's previous high of 1,031,018 tons registered in 1955. And, although consumption of zinc in 1956 was slightly below consumption in 1955 — 994,000 tons compared with 1,119,812 tons, indications are that 1957 will see all records broken.

According to John L. Kimberley, executive vice president of the American Zinc Institute, three factors are responsible for the zinc industry's confidence: 1) the growing market for zinc in die-casting, 2) its expanding use in galvanizing of steel, and 3) the integral place it holds in brass manufacture, rubber and paint formulation.

The average 1957 automobile carries 65 lb of zinc, with die castings used for head and tail light assemblies, and instrument panel assemblies, as well as such functional parts as carburetors, windshield wiper motors, door handles, window cranks, etc. Last year 60 lb of zinc were used per car.

Mr. Kimberley points out that the steel industry is continually expanding its use of continuous sheet galvanizing lines. At present more than 75% of the galvanized sheet being produced comes from some 34 of these lines now operating. The figure is expected to increase to 90% in the near future.

The AZI is currently winding up an important stage of a major research program aimed at improving the use of zinc anodes for the cathodic protection of a wide variety of structures, including piers, pipelines, ship hulls, and gas distribution systems and tanks. Success in this and other

(continued on p 278)

SLAB ZINC CONSUMPTION, TONS[a]

End Use	1955	1956
Galvanizing	451,000	429,000
Brass Products	146,000	121,000
Zinc-Base Alloys	431,000	360,000
Rolled Zinc	52,000	47,000
Zinc Oxide and Others	40,000	37,000

[a]Based on American Zinc Institute figures.

Prices of Materials

Changes since last month are bold faced.

NONMETALLICS

Prices for large quantities for range of grades, color, sizes; given in $/lb

RUBBER

Material	Dry	Latex
Butadiene-Acrylonitrile	.49-.65	.44-.54
Butadiene-Styrene	.16-.30	.26-.32
Butyl	.23-.28	—
Neoprene[a]	.39-.75	.37-.47
Silicone[a]	1.90-4	—
Polysulfide[a]	.47-1	.70-.92
Natural	**.33**[b]	—

[a]Less than carload quantities.
[b]Average spot price for month of Jan.

GLASS FOR REINFORCED PLASTICS

Fabric ($/yd, 38 in. wide)[a]	
112 Woven	.48
181 Long-shaft satin weave	1.03
143 Unidirectional	1.00
Roving[a]	
Continuous	.40
Continuous spun strand	.36
Continuous chopped spun	.38
Milled fibers (1/32-¼ in.)[a]	.45
Mat	
Chopped strand (2 in.)[a,b]	.52-.72
Surfacing ($/1000 sq ft)[c]	10-19
Continuous chopped strand (¼-2 in.)	.40

[a]Price includes binder or finish.
[b]Price varies with binder.
[c]0.010-0.020 in. thick.

THERMOSETTING PLASTICS

Material	Molding Compounds	Laminating, Casting Resins
Alkyd	.34-.53	—
Epoxy	—	.45-.80
Melamine	.42-.45	.40-.41
Phenolic	.20-.40	.17-.34
Polyester	.42	.32-.50
Silicone	2.75-5.40	1.55-1.74[a]
Urea	.19-.33	—

[a]60% solids content.

All prices are approximate and given solely for general guidance of those responsible for materials selection.

THERMOPLASTICS

Material	Molding Compounds	Sheet (.030-.250 in.)	Rod ⅛-¼ in.	Rod ⅜-1¼ in.	Tube ⅛-¼ in.	Tube ⅜-1¼ in.
Acrylic	.51-.59	.49-2.15	.90-1.15	.80-.90	1-1.15	.90-1
Cellulosic						
Acetate	.36-.65	.92-1.16	.75-1	.65-.75	.85-1	.75-.85
Butyrate	.50-.72	1-1.28	.95-1.20	.85-.95	1.05-1.20	.85-1.05
Nitrate	—	1.60-2.73	1.45-1.75		2.25-5.00	
Propionate	.51-.63	—	—		—	
Fluorocarbon						
PTFCE	**7-8**	15-23	**18-22**	**14-20**	**20-22.50**	**16-20**
PTFE	4.50-7.45	14.30-11	13		13	
Nylon	1.35-2.30	—	3		3	
Polyethylene	.37-.56	.85-1	.75-1	.65-.75	.85-1	.75-.85
Polystyrene	.27-.44	.57-.61	.65-.90	.55-.65	.75-.90	.65-.75
Vinyl	.27-.43	.62-.92	.75-1	.65-.75	.85-1	.75-.85

NONFERROUS METALS

Mill base prices for large quantities; given in $/lb except where indicated

ALUMINUM

Pig (99-99.9%)	.25-.27
Ingot (99-99.9%)	.27-.29
Foil (5-0.5 mil)	.55-.77
Alloy Ingot (13, 43, A132, 214)	.29-.32
Sheet (1100, 3003; 3-.03 in.)[a]	.40-.45
Plate (1100, 3003, 5050, 3004, 5052)[a]	.40-.43

[a]Mill finish.

BRASS

Form	Cart., 70%	Low, 80%	Red, 85%
Sheet, Strip	.48	.50	.51
Seamless Tubing	.50	.53	.54
Rod (not f.c.)	.47	.50	.51
Wire	.48	.51	.52

COPPER

Ingot (elec)	.32
Sheet, Strip (hot rolled)	.54
Seamless Tubing	.54
Rod, Drawn	.51
Rod, Free Cutting	.60
Wire	
Round	.37
Square, Rectangular	.41
Magnet	.45

LEAD

Common Grade	.16

MAGNESIUM

Pig (98.8%)	.36
Ingot (98.8%)	.37
AZ91B Ingot (die casting)	.37
AZ91C Ingot (sand casting)	.41[a]

[a]Delivered price.

NICKEL

Form	"F"	"A"	Monel
Ingot	.75[a]	—	—
Rod	—	1.07	.89
Sheet, C.R.	—	1.26	1.06
Strip, C.R.	—	1.24	1.08
Seamless Tube	—	1.57	1.29

[a]Delivered price.

TIN

Primary[a]	.98

[a]Delivered price.

(continued on p 274)

NOTHING *can equal Stainless Steel*

in its unique combination of properties

No other design material can match Stainless Steel in its combination of desirable properties: corrosion resistance, strength, hardness, beauty, cleanability and easy fabrication. For a reliable source of supply, United States Steel offers you the widest range of types, finishes and sizes.

UNITED STATES STEEL CORPORATION, PITTSBURGH
AMERICAN STEEL & WIRE DIVISION, CLEVELAND
COLUMBIA-GENEVA STEEL DIVISION, SAN FRANCISCO
NATIONAL TUBE DIVISION, PITTSBURGH
TENNESSEE COAL & IRON DIVISION, FAIRFIELD, ALA.
UNITED STATES STEEL SUPPLY DIVISION, WAREHOUSE DISTRIBUTORS
UNITED STATES STEEL EXPORT COMPANY, NEW YORK

USS STAINLESS STEEL

SHEETS · STRIP · PLATES · BARS · BILLETS
PIPE · TUBES · WIRE · SPECIAL SECTIONS

USS

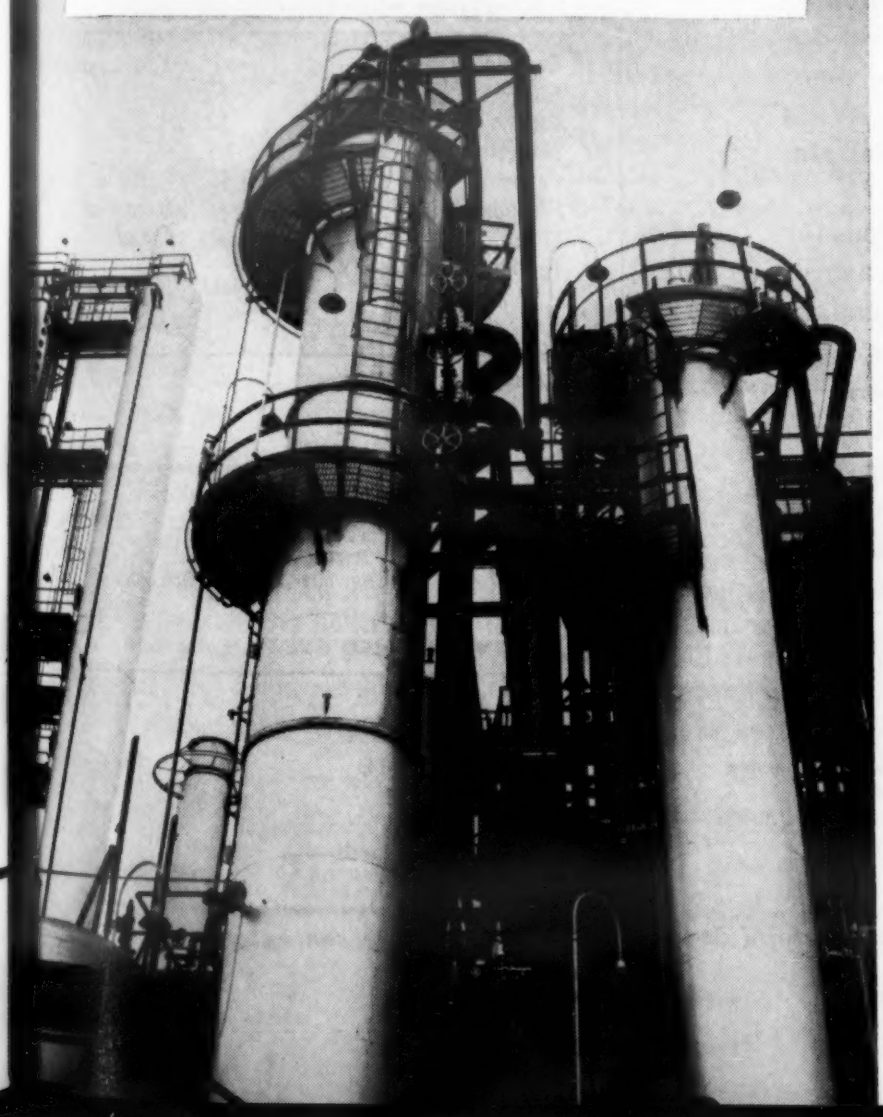
UNITED STATES STEEL

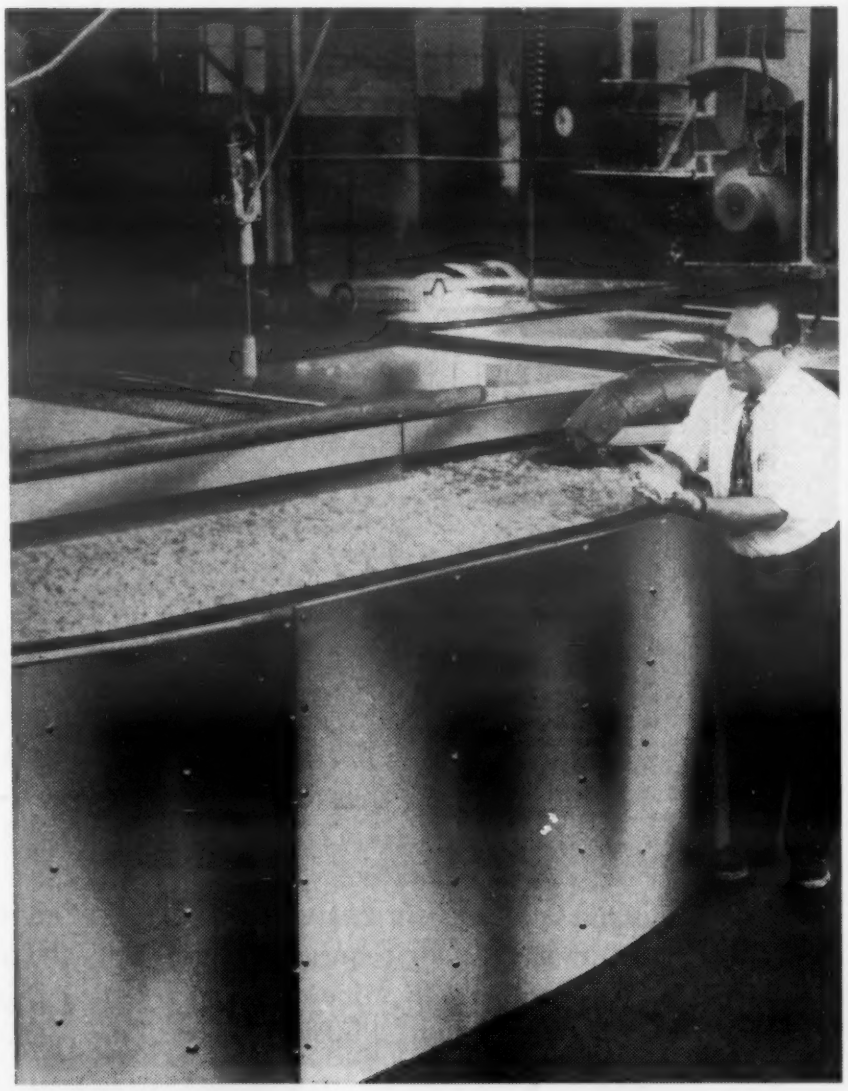
For Sanitation

Food juices are incredibly corrosive, so some restaurants have a lot of trouble in their cold storage rooms because the racks corrode and harbor bacteria. Eastern Steel Rack Company makes racks from Stainless Steel. They are easy to keep clean; and, for all practical purposes, they *never* wear out.

For Corrosion Resistance

This petrochemical extract fractionator was originally made from carbon steel . . . but corrosion ate through the plates and put it out of service in *just two months.* They lined the tower with type 316 Stainless Steel. When examined, the tower had been in service 21 months, and the Stainless was still in good condition.





For Cleanliness

Hawthorne Paper Company, Kalamazoo, Mich., goes to extraordinary lengths to guard against color contamination. Old wooden tanks were thrown out and replaced with Stainless Steel. According to the men at Hawthorne, the Stainless has absolutely no contaminating effect, and it's easy to fabricate.

PRICES AND SUPPLY

TITANIUM

Sponge (99.3+%)	2.50-2.75
Bars, Rod	7.10-7.35
Plate	9.25-11.25
Sheet, Strip	11.40-12.10
Wire	8.50-9.00

ZINC

Primary[a]	.13-.14[c]
Die Casting Alloys[b]	.18-.19[c]
Sheet	.24
Ribbon	.22

[a]Prime Western—Special High Grade. [b]Alloys 2, 3, 5. [c]Delivered price.

METAL POWDERS

Aluminum [a,b]	.36
Brass[a]	.37-.47
Copper (elec or red.)[a]	.46
Columbium	120
Molybdenum (98%)	3.80-4.10
Tantalum	49
Tungsten (C-red. 98.8%; H_2-red. 99+%)	4-5[c]
Zirconium	
Flash Grade	11.50
Electronics Grade	15

[a]Price for —100 mesh. [b]Freight allowed. [c]Delivered price.

OTHER NONFERROUS METALS

Cadmium (bars)	1.70
Gold	$35/troy oz
Indium (99.97+%)	$2.25/troy oz
Manganese (99.9%)	.33[a]
Palladium	$23-24/troy oz
Platinum	$98-101/troy oz
Silver	91¢/troy oz
Tantalum (sheet, rod)	55-60
Vanadium	3.45
Zirconium (sheet, strip, bar)	27-35

[a]Delivered price.

IRONS AND STEELS

Mill base prices for large quantities

SEMIFINISHED STEEL ($/net ton)

Ingots, Alloy	74
Billets, Blooms, Slabs	
Carbon, Re-rolling	74
Carbon, Forging	92
Alloy, Forging	107
Seamless Tube Rounds	112
Wire Rods	$5.85/cwt

(continued on p 276)

New Nylasint® 64 nylon wear parts ... tough, durable, impact-resistant

Nylasint 64 is the newest in the family of Nylasint finely divided nylon powders, bringing new advantages to wear parts formed by the technique of cold pressing and sintering.

Nylasint powders, which can be compounded with various fillers such as molybdenum disulphide or graphite, form parts with these superior properties:

- *High wear and abrasion resistance*
- *Low surface friction*
- *High modulus—resist deformation under load*
- *Low hygroscopic and thermal expansion*
- *High heat distortion temperature*

. . . plus these advantages in processing:

- *Uniform shrinkage, accurate profiles*
- *Require no degating, have no flash lines*
- *Minimized possibility of stress spots or internal strain*
- *Economical mass production*

For detailed information on your applications, write to National Polymer Products, Inc., Reading, Pa.

POLYPENCO

Licensed Fabricators and Design Engineers:
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NATIONAL POLYMER PRODUCTS, INC.
A Subsidiary of The Polymer Corporation
Reading, Pennsylvania

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PRICES AND SUPPLY

FINISHED STEEL ($/cwt)

Form	Carbon	High Str Low Alloy	Alloy
Plate	4.85	7.25	6.85
Sheet, H.R.	4.67	6.90	—
Sheet, C.R.	5.75	8.52	—
Strip, H.R.	4.67	6.95	7.75
Strip, C.R.	6.85	10	14.55
Bar, H.R.	5.07	7.42	6.12
Bar, C.F.	6.85	—	8.32

STAINLESS STEELS ($/lb)

Material	Forging Billets	H. R. Bars	Plate[b]	Sheet, Strip
Austenitic				
301, 302, 302B, 303, 304, 305	.36-.40	.41-.46	.45-.49	.50-.56
321[a]	.45	.53	.58	.63
347[a]	.54	.62	.67	.76
Martensitic				
410[a]	.27	.33	.34	.39
416	.28	.33	.35	.47
403	.31	.36	.39	.47
420, 440	.33	.40	.44	.60
Ferritic				
405, 430, 430F[a]	.28-.29	.33-.34	.35-.36	.39-.50
442	.32	.38	.40	.54
431	.36	.42	.44	.54
446	.38	.45	.46	.67
High Mn				
202[a]	.35	.41	.43	.47
Extra-Low C				
304L	.47	.53	.56	.61
316L	.64	.74	.78	.82
Precip Hard.				
17-7PH	.55	.65	.72	.77-.82

[a]Ingot prices approx 60% of forging billet price.

METAL POWDERS ($/lb)[a]

Sponge Iron	.09-.10
Electrolytic Iron	
Annealed (99.5%)	.37
Unannealed (99+%)	.34
Stainless Steel	
304	1.05
316	1.40

[a]Price for —100 mesh.

IRON ($/gross ton)

Pig	62.50-63.50

(continued on p 278)

PRICES AND SUPPLY

TIN PLATE ($/base box)

Hot Dip (1.25-1.50 lb)	9.70-9.95
Electrolytic (0.25-0.75 lb)	8.40-9.15
Black Plate	7.50-7.60

FINISHES AND COATINGS

ORGANIC COATINGS

Material	Avg Thk per Coat, mil	Mils Required[a]	Cost, ¢/sq ft/dry mil[b]
VARNISHES, ENAMELS			
Short Oil Phenolic			
Varnish	1.0	1.0	1.50
Enamel	1.2	1.0	1.75
100% Phenolic	1.0	1.5	1.75
Straight Oil-Modified Alkyd	1.5	1.5	1.50
Alkyd-Amine (90-10)	1.5	1.5	1.75
Alkyd-Phenolic (50-50)	1.5	1.5	1.75
Alkyd-Vinyl (50-50)	1.0	2.0	2.0
Alkyd-Styrene (70-30)	1.2	1.5	1.75
Epoxy	1.8	1.8	2.00
Silicone	.5-1.0	.5-1.0	6.0
Furane	2.0	2.0	1.0
Neoprene	5.0	5.0	1.50
DISPERSION COATINGS			
Phenolic	1.0	1.5	1.75
Vinyl	1.0	2.0	2.50
Fluorocarbon	1.0	1.0	15.0
LACQUERS			
Nitrocellulose	1.0	2.0	2.50
Vinyl	1.0	2.0	2.50
Acrylic	1.0	2.0	2.75

[a]Thickness over phosphate coating required for exterior durability on steel. For purely decorative coating, 1 mil will usually suffice.
[b]Materials cost only. Realistic price comparison can be made only on basis of dry applied coating, not on basis of cost per gallon.

(continued from p 271)

similar ventures will probably result in even wider use of zinc.

The supply-demand situation is presently balanced and Mr. Kimberley foresees "no demand which the zinc industry will not be able to handle."

(more Prices & Supply on p 280)

PRICES AND SUPPLY

What's Happening in Prices and Supply

Tungsten — Two General Electric Co. technicians are reported to have found what may be a rich deposit of strategic tungsten in Eastern New York State. According to the report, the deposit extends for at least 150 miles, and at two test points the belt of ore is 30 ft deep. Should the deposit be commercially feasible, it could make the United States independent of foreign sources for tungsten. The best known deposits are in China.

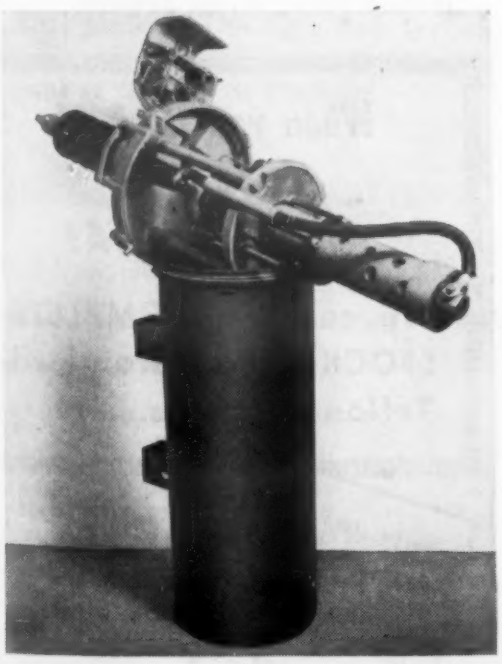
Steel — Beginning with April shipments, the Cleveland-Cliffs Iron Co. price of Lake Superior iron ore will be increased by 60¢ per ton, or about 5%. All other producers of Lake Superior ore are expected to follow suit and since 70% of all iron ore consumed by the domestic steel industry comes from this region, steelmaking costs will be increased.

Sharon Steel Corp. has completed a new $14 million slabbing and blooming mill, increasing its ingot rolling by 1,200,000 tons a year. Sharon's total ingot capacity is expected to exceed 2 million tons by the end of 1957.

Silicon — Du Pont expects to produce annually about 50,000 lb of semiconductor grade silicon once its new plant is completed early in 1958. The material, a vital part of electronic and electrical devices, sells for $320 per lb. At present, Du Pont is the nation's only producer of this "hyper-pure" silicon.

Aluminum—The American Die Casting Institute estimates that the die casting industry will produce 450 million pounds of aluminum die castings in 1957. Moreover, it estimates that by 1960 this figure will grow to 750 million lb. This would be ⅛ of all aluminum, primary and secondary, produced domestically and equiv-

and you put Synthane laminated plastics to work



Automatic Circuit Recloser Parts made from Synthane sheet and tube provide insulation for high voltages.

Think of the many conveniences available simply by plugging into an electrical outlet.

On both sides of the outlet Synthane laminated plastics are at work in power generation and distribution, home appliances and other electrical equipment.

You find Synthane laminated plastics in circuit breakers, buss bar coverings, transformers. Synthane laminated plastics are important insulators in toasters, ranges, food mixers. Synthane is at work in thermostats, voltage regulators, power tools.

Synthane is valued in electrical applications chiefly for its high dielectric strength, low moisture absorption and low dissipation factor plus its additional properties of dimensional stability, machinability and mechanical strength. Synthane is available in over 30 standard grades in sheet, rods, tubes or you can avail yourself of our complete fabricating services.

For more information about the many properties of Synthane and how you can benefit by using Synthane materials and fabricating services, write for our product catalog. Synthane Corporation, 3 River Road, Oaks, Pennsylvania.

DIELECTRIC STRENGTH | IMPACT STRENGTH | HEAT RESISTANCE | LIGHT WEIGHT

SYNTHANE ... industry's unseen essential

SYNTHANE CORPORATION, 3 RIVER ROAD, OAKS, PA.

For more information, turn to Reader Service Card, Circle No. 392

PRICES AND SUPPLY

alent to 15% of the 1960 market for primary aluminum.

Polyethylene — Texas Eastman Co., Div. of Eastman Kodak Co., has increased its polyethylene annual capacity to 55 million pounds. In less than one year the company has increased its capacity by 15 million pounds.

Both Celanese Corp. of America and Hercules Powder Co. are supplying commercial quantities of high density (low pressure) polyethylene. Celanese, under license from Phillips Petroleum Co., will produce 40 million pounds per year. Hercules, using a Ziegler-type process, will produce 30 million pounds per year. Hercules' price ranges from 47 to 53¢ per lb.

Polyesters—Durez Plastics Div. of Hooker Electrochemical Co. will make commercially available a new line of polyester molding compounds (see page 175). Price of the new material ranges from 42 to 77¢ per lb, depending upon quantity.

Polystyrene foam—Price reductions ranging from 10 to 15% on standard board forms of expanded polystyrene have been announced by Dow Chemical Co. The reductions apply to 3, 8 and 9-ft lengths and 12 and 16-in. widths.

Paints—Du Pont plans to build its third plant for the manufacture of titanium dioxide. The new plant will have a capacity of 125 tons a day when it gets under way in early 1959. The unusual growth in use of titanium dioxide is due to its great hiding power; ten times as much white lead and five times as much lithopone pigment are required to attain the opacity provided by titania.

Nylon—About 64 million pounds of nylon tire yarn were used in 1956—about 25% more than was consumed in 1955. Only 8 million pounds of nylon tire yarn were consumed in 1952.

Methyl methacrylate—Hercules Powder Co. and Imperial Chemi-

How Armco 17-4 PH Stainless cuts costs, resists galling and corrosion in valve parts

Ruggedness and resistance to corrosion are prime requisites for relief valves that serve boilers and pressure lines in refineries and chemical plants.

Farris Engineering Corp., the manufacturer of this safety valve, uses special Armco 17-4 PH Stainless Steel for the disc and stem retainer . . . the core of the unit. Here's why:

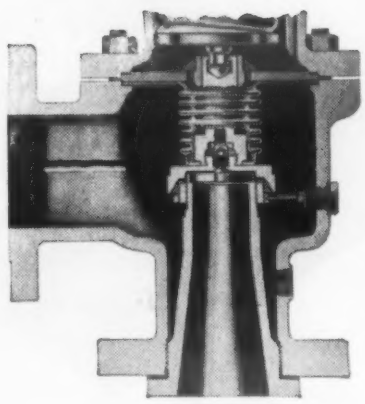
1. Costs are lower because there is no re-machining or grinding after hardening. No distortion occurs during low temperature heat treatment.

2. Parts made of Armco 17-4 PH have high hardness and resistance to galling.

3. Good resistance to impact is provided by this special steel.

4. Since Armco 17-4 PH has a lower coefficient of expansion than the non-hardenable stainless grade used in adjoining parts, a cause of "hanging" is eliminated.

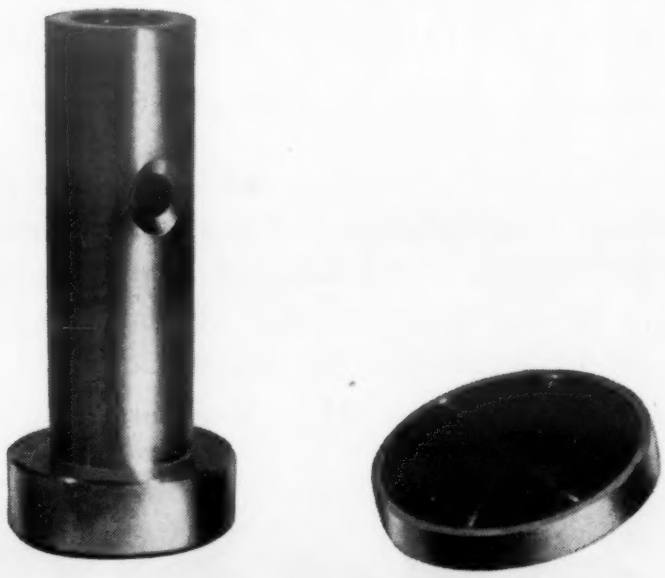
Stem retainer and disc of Armco 17-4 PH Stainless form the tough "heart" of this relief valve, serving on a pressure line in a chemical processing plant. Both parts shown were finish-machined before hardening because this special steel doesn't distort during heat treatment.



ELIMINATE 4 SHOP OPERATIONS

Finish-machine, then heat treat at low temperature —and a part made of Armco 17-4 PH is ready for assembly. You can eliminate re-machining or grinding, stress relieving, pickling, and straightening operations.

Armco 17-4 PH is available in billets, bars and wire. A companion grade, Armco 17-7 PH Stainless, is produced in sheets, strip, plates, billets, bars and wire. Write us at the address below for full information about these special new precipitation-hardening stainless steels.



ARMCO STEEL CORPORATION

957 CURTIS STREET, MIDDLETOWN, OHIO • SHEFFIELD STEEL DIVISION • ARMCO DRAINAGE & METAL PRODUCTS, INC. • THE ARMCO INTERNATIONAL CORPORATION

For more information, turn to Reader Service Card, Circle No. 601

cal Industries, Ltd., have formed a jointly owned company, Hawthorn Chemical Corp., which will produce 35 million pounds of methyl methacrylate annually. ICI will probably continue to produce the material on its own. At present, the major U.S. suppliers are Du Pont and Rohm & Haas.

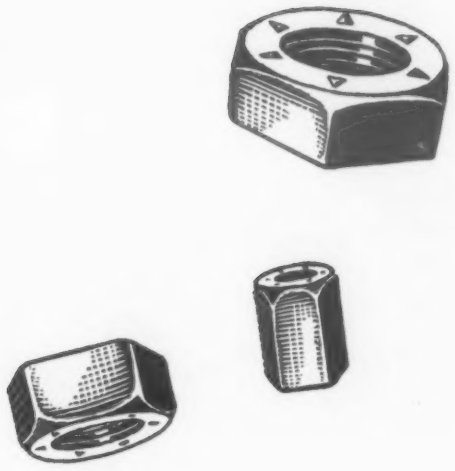
Tellurium—American Smelting and Refining Co. has announced an increase of 15¢ per lb for powdered tellurium in 100-lb lots, the first price increase for tellurium in 3½ years. The new price is $1.65 per lb.

Tantalum, columbium—Fansteel Metallurgical Corp. will build a $6,500,000 tantalum - columbium plant on a 113-acre site near Muscogee, Okla. The new facility is expected to increase Fansteel's tantalum capacity by 50% and its columbium cpacity by 150%.

Packaging materials—In pointing out the important position the packaging industry occupies in terms of materials use, John Warren, technical adviser of American Management Assn.'s packaging division, offered the following statistics: the packaging industry uses 99% of the nation's cellophane production; 80% of its metal foil (about 7% of the aluminum industry's entire output); 70% of all glass other than flat glass; and 55% of the paper and paperboard output.

Price Schedule for Radiation Service

The first private rate schedule for commercial atomic radiation is available from Radiation Applications, Inc. Industrial concerns may purchase gamma radiation from the 1350 curie cobalt-60 source for a base charge of $8 per hr; for continuous 24-hr use the price is $64. Loading charge is $2.50 per operation and the base rate for supervision of experiments is $7.50 per hr.

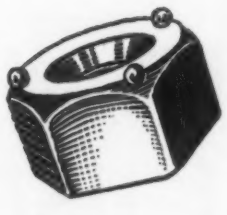


For over 50 years, leading manufacturers in all the major industries have used Gripco lock nuts to simplify production, lower manufacturing and maintenance costs and to improve the durability of all kinds of assembled products. To maintain this enviable reputation for outstanding product quality, the Grip Nut Company of South Whitley, Indiana, uses quality-controlled Youngstown Scrapless Nut Wire and Bars as basic raw material.

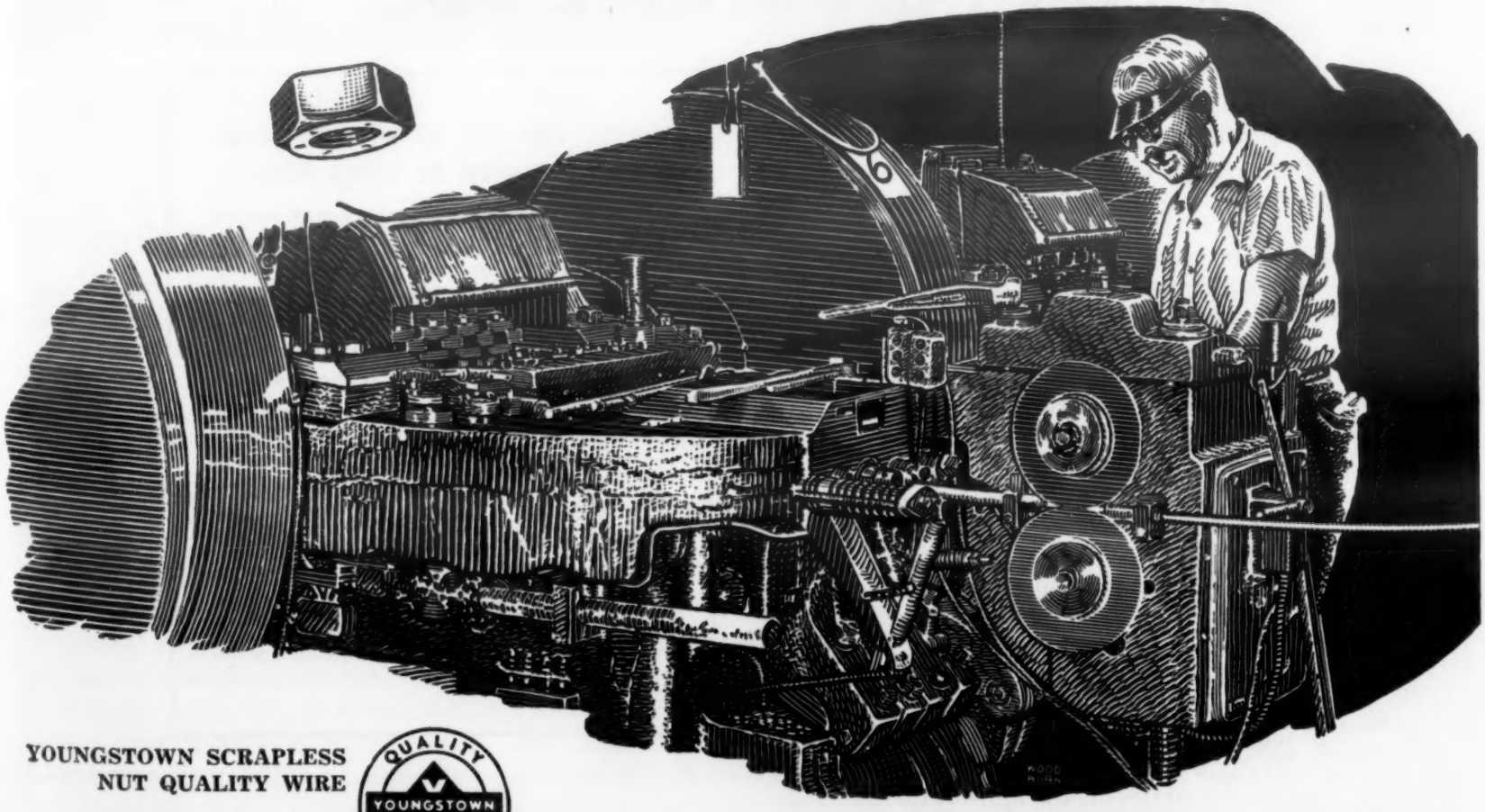
Because it comes to your plant free from all piping, injurious seams, laps, die marks, internal tearing and cupping, and non-metallic inclusions —Youngstown Scrapless Nut Quality Wire will provide increased production with fewer rejects which adds up to a healthy over-all profit boost. Also, its smooth coating extends die life thus minimizing costly die replacements.

YOUNGSTOWN SCRAPLESS NUT WIRE

Helps Maintain Quality of GRIP *Lock Nuts*



Youngstown Scrapless Nut Quality Wire is provided in special resulphurized steels as well as in standard AISI grades. Cold Heading Bolt Wire, of the same high Youngstown quality, is also available in all standard carbon and alloy analyses. Why not phone or write to our nearest District Sales Office for additional information or metallurgical assistance?



YOUNGSTOWN SCRAPLESS NUT QUALITY WIRE

QUALITY YOUNGSTOWN SERVICE

THE YOUNGSTOWN SHEET AND TUBE COMPANY

Manufacturers of Carbon, Alloy and Yoloy Steel

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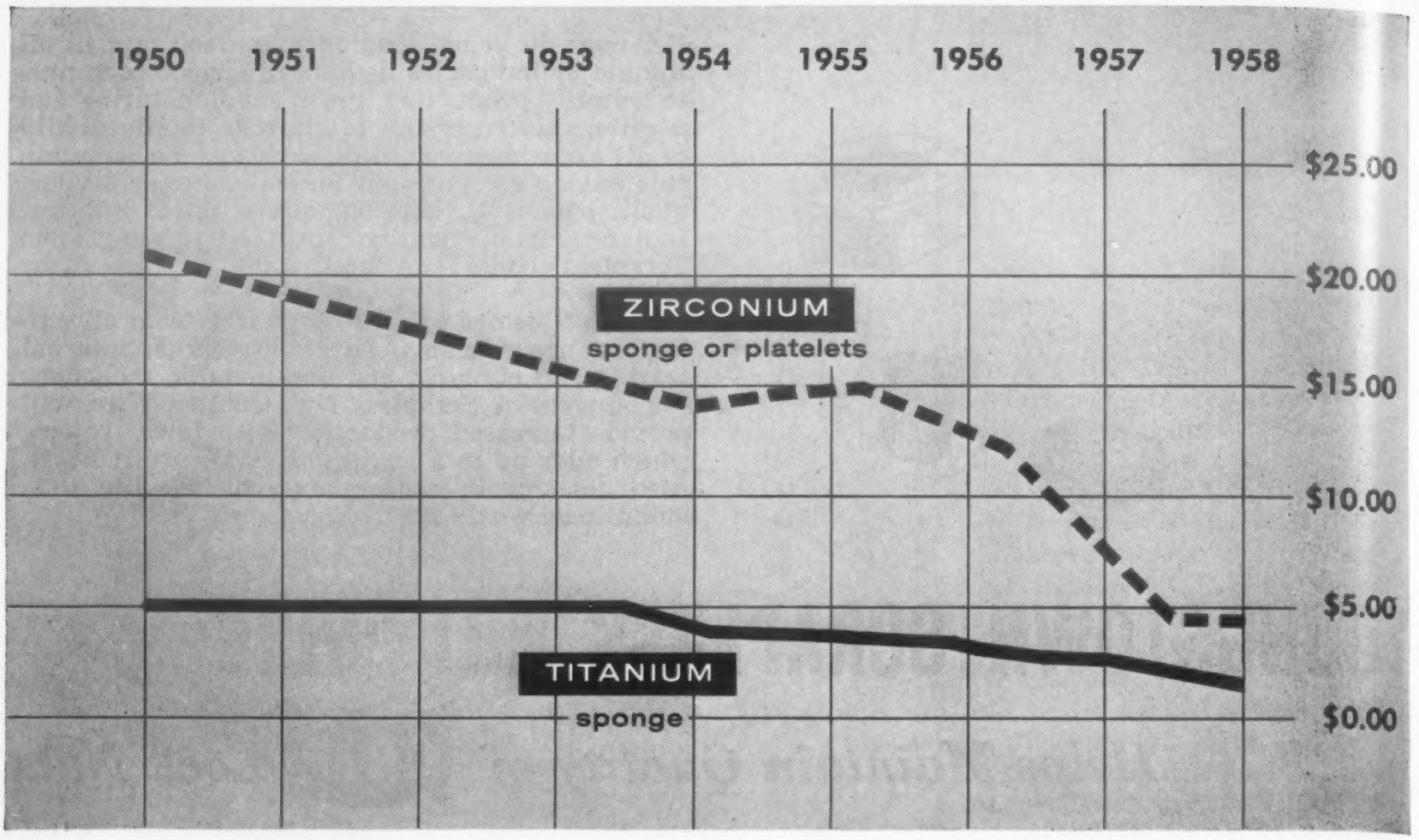


Available soon at lower prices

ZIRCONIUM AND TITANIUM FOR INDUSTRIAL USE

Now is the time to do some new thinking about titanium and zirconium. These metals with their many advantages will soon be *much more plentiful* at *much lower cost.* Reason: U.S.I. will be coming onstream shortly with a 10-million pound per year titanium plant AND a zirconium plant which will supply one million pounds of that metal to industry.

Zirconium from the new plant will sell for considerably less than current prices. Here's why: U.S.I. will use the most economical production technique ever developed for reducing metallic chlorides – a semi-continuous sodium reduction process. This process has possibilities of reducing titanium prices in the future as well.

So think again about zirconium and titanium for industrial equipment. Remember that they are lighter than other metals – a pound goes farther. Remember that they are more durable than other metals–a fabricated product lasts longer.

Write to Bill Greenleaf, U.S.I. Manager of Metals Department, for more information on these new metals from U.S.I.

Chemical Progress Week — April 8-12

WHAT CAN YOU DO WITH TITANIUM AND ZIRCONIUM AT LOWER PRICES?

In the future titanium sponge prices are expected to drop to about $2.00 a pound, with a corresponding drop in the prices of mill products. At these prices the exceptional strength-to-weight ratio and corrosion resistance of titanium can be put to work in the aircraft, marine, automotive, chemical and allied fields.

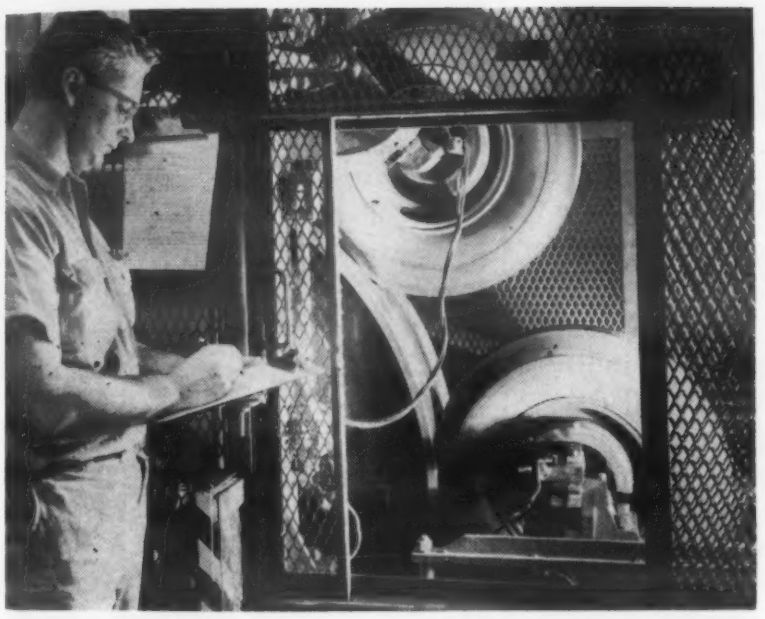
Or consider the eventual price of U.S.I. commercial grade zirconium: an estimated $3.00 a pound for platelets and 2 or 2½ times this price for the average mill product. This price will make zirconium practical for chemical equipment, marine equipment, food equipment and surgical metals among other uses. Zirconium has light weight, high structural strength, excellent corrosion and heat resistance; and reactor-grade zirconium has outstanding nuclear properties.

U.S.I. INDUSTRIAL CHEMICALS CO.

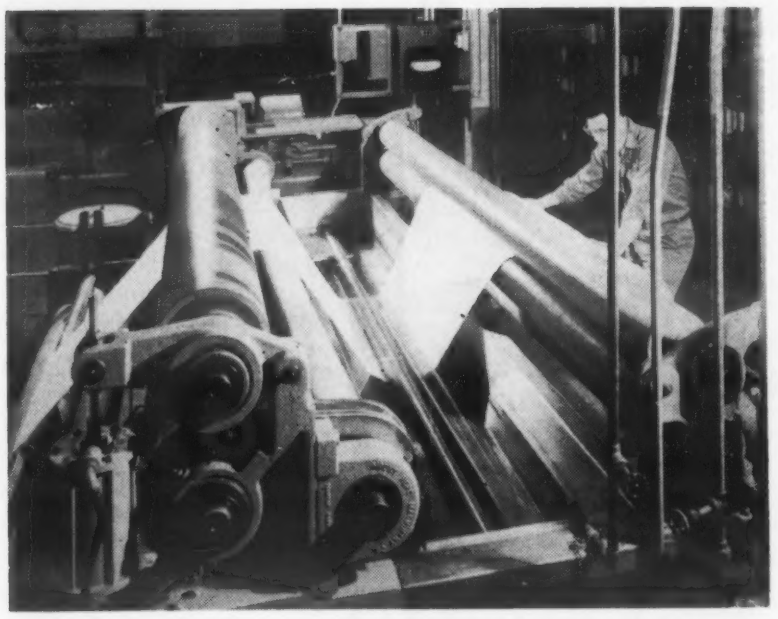
Division of National Distillers Products Corporation
99 Park Avenue, New York 16, N. Y.

For more information, turn to Reader Service Card, Circle No. 552

News OF INDUSTRY



***Tires** are tested at various loads and inflation pressures to determine performance of synthetic tire cord.*



***Nonwoven felt** of synthetic fibers in final production step. Density, hardness and other properties can be varied by controlled changes in processing.*

Industrial Use of Synthetic Fibers Studied in Textile Laboratory

■ Du Pont has taken the lid off a heretofore unpublicized research laboratory engaged in a broad scale study of industrial applications of synthetic fibers. Established in 1954 by Du Pont's Textile Fibers Dept., the laboratory has been instrumental in the development of fibers for such applications as tire cord, plastics reinforcement, nonwoven fabrics and felts, paper, bearings, coated protective coverings, filling materials and mechanical rubber goods.

One of the areas in which the lab has been particularly valuable is automobile tire research. The lab has complete tiremaking facilities, including a dip-stretch unit that can process from 1 to 64 cords at a time. With this laboratory-scaled replica of a large commercial unit, researchers are able to vary conditions widely to determine effect on cord or to develop improved processes for tire manufacture. Two specially devised test wheels duplicate any one condition of tire service, and each of the 45 test tires produced weekly is used to test some new concept of tire construction.

Also available in the laboratory are Instron testers with loading

Plan to Attend the Design Show

1. To hear talks about latest developments in materials and processes.
2. To see exhibits of new products and designs.
3. To meet and talk with people who may be able to answer your materials or other design problems.

The Design Engineering Show and Conference will be held at the New York Coliseum May 20-23. See the May issue of MATERIALS & METHODS for complete registration details, list of exhibitors and program of technical sessions.

News OF INDUSTRY

***Nylon cord** for tires is checked prior to application of adhesive.*

capacities ranging from 10,000 lb of thrust or tension to a few grams — the latter suitable for measuring the tenacity of individual fibers. Another special device determines fatigue resistance of cord by recording the number of twists sustained by a short length of hose reinforced with the cord before it ruptures and allows compressed air to escape from within it.

The Laboratory is under the direction of Richard W. Nebel.

AIME Conference To Be Held This Month

The American Institute of Mining, Metallurgical and Petroleum Engineers, in cooperation with the High Temperature Committee of the Institute of Metals Div., will hold a two day conference on high temperature materials in Cleveland April 16 and 17.

Papers and discussions will cover cobalt, nickel, chromium and molybdenum-base alloys; refractory metals; SAP-type materials; cermets and hard metal compounds; ceramics; graphite and methods of testing; effect of atmosphere on high temperature properties; and effects of vacuum melting and casting on properties.

(more News on p 290)

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A single reliable "supermarket" for all of your precision casting needs? Yes sir! Regardless of size, complexity or material, all of your investment casting requirements can be met by Alloy Precision Casting Co — the nation's only foundry with both FROZEN MERCURY and LOST WAX facilities under one roof.

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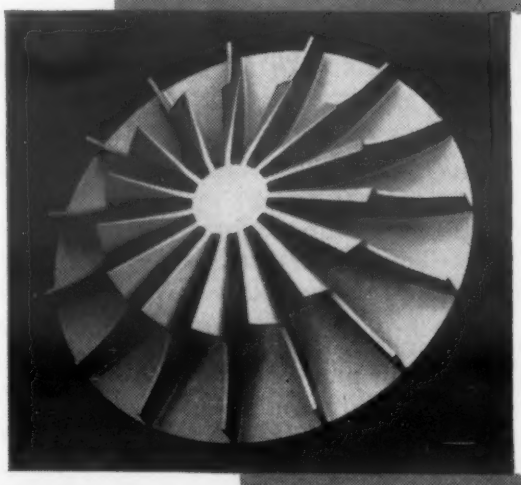
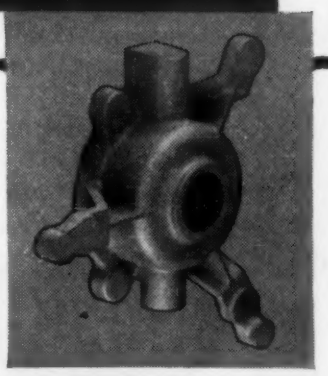
Many of America's outstanding industrial firms have come to regard Alloy Precision as their investment casting "supermarket" because of demonstrated skill, consistent HIGH QUALITY and deliveries made on schedule!

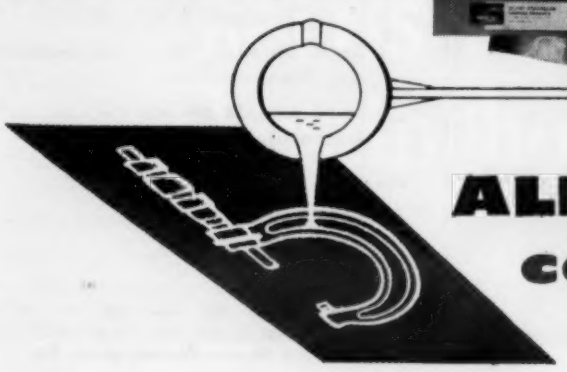
Insure the success of your investment casting designs! Send them to Alloy Precision Casting Co.





FREE GUIDES!

"HOW TO DESIGN, SPECIFY AND BUY INVESTMENT CASTINGS" literature includes description of Alloy Precision's modern plant and techniques. Write today! Send blue prints for quotes, design recommendations and value analysis to:



ALLOY PRECISION castings company

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A-1061

For more information, turn to Reader Service Card, Circle No. 586

News OF INDUSTRY

Electron microscope *modified for analysis of steel specimen areas only a few microns in diameter.*

Electrons, X-Rays Aid Steel Studies

A new metallurgical research technique permits analysis of steel specimen areas 10,000 times smaller than is possible by any other method. The technique makes use of an electron microscope modified to excite x-ray emission from a region as small as a few microns in diameter.

Broad applications

The new method, being studied and modified at U. S. Steel Corp.'s Fundamental Research Laboratory, has wide potential application in metallurgy for 1) studying intergranular corrosion, 2) analyzing segregation of alloying elements among the metallic phases and along metallic grain boundaries, 3) measuring interdiffusion during welding and plating, and 4) determining the composition of fine precipitate particles.

The technique is as follows: steel samples are placed in a specimen chamber in the face of the 4-ft. electron column. An electron beam, accelerated to approximately 30,000 v., is focused by three electrical lenses. The electron beam crossover point, formed

News OF INDUSTRY

by the objective lens, is focused by a repeater lens on the surface of the steel sample. An optical binocular microscope and mechanical stage motion permit the operator to make visual adjustments of the specimen under the beam.

Beam is analysed

The focused beam strikes a selected area of the specimen's surface, causing x-ray emission. The x-ray beam is then analyzed to determine its component wave lengths by reflection from a lithium fluoride crystal. The x-ray intensity at each wave length is amplified through a vacuum tube arrangement to activate a pen on a graph in which the x-axis indicates the wave length, the y-axis the intensity. These details are then analyzed quantitatively. At present the instrument is capable of detecting all elements with atomic number 22 (titanium) or higher.

Metallurgy, Titanium Lectures at NYU

New York University's College of Engineering will offer two special programs of lectures on metallurgy. The first, to be conducted from June 10-14, will consist of 25 lectures on vacuum metallurgy. Specialists from this country and abroad will discuss vacuum pumping systems, thermodynamics, specific processes, design and operation of arc and induction melting systems, and application of vacuum processed materials. Inquiries should be addressed to R. F. Bunshah, Associate Engineering Scientist, New York University College of Engineering, University Heights, N. Y.

The third annual titanium lecture program will be held Sept 9-13. Applications and further information can be obtained from Harold Margolin, New York University.

News OF INDUSTRY

Engineers

Harry L. Bishop, Jr. and Sundaresan Ramachandran have joined Allegheny Ludlum Steel Corp. as research advisers.

Robert K. Allen is now superintendent of product development at Babcock & Wilcox Co.'s Research Center; **Claude L. Huey** is the newly appointed manager of the company's Atlanta District.

Donald Bohn, designer, inventor and engineer, has retired from Aluminum Co. of America after more than 34 years of service.

Henry M. Haase has been elected vice president in charge of engineering and research, Borg-Warner Corp., York, Pa.

L. W. Newton is the newly appointed assistant to the vice president—research, Carbide and Carbon Chemicals Co., Div. of Union Carbide and Carbon Corp.

Ernest W. Neben is director of the Central Engineering Div., Pfaudler Co. **Edward W. Zoller** is now works manager of the company's Rochester Div.

Charles J. Meloun succeeds **H. J. Flaherty** as manager of engineering, General Electric's Outdoor Lighting Dept., Hendersonville, N. C. Mr. Flaherty has been named a consultant.

Wilton E. Parker is now assistant chief engineer, AiResearch Industrial Div., Garrett Corp.

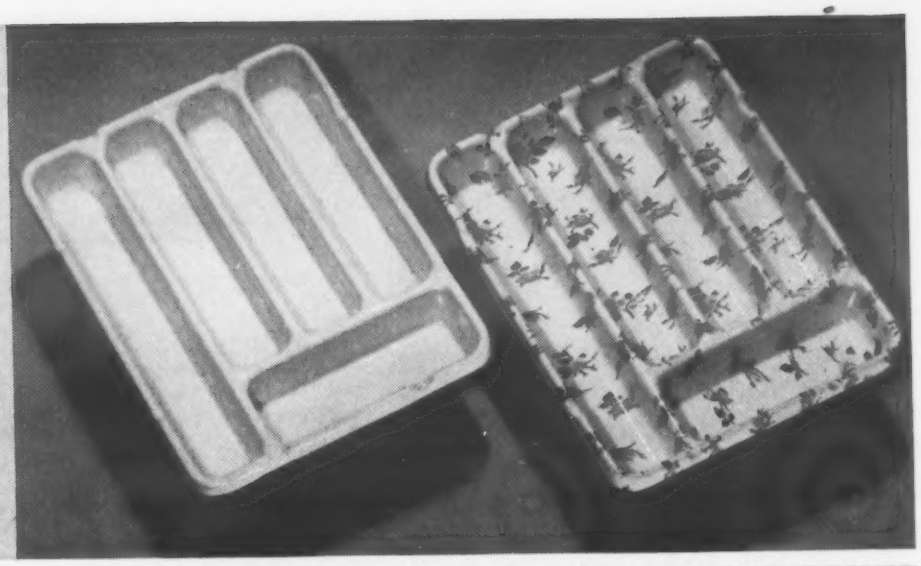
Douglas W. Fuerstenau has received the Robert Lansing Hardy Gold Medal. The medal was presented by the American Institute of Mining, Metallurgical and Petroleum Engineers in recognition of exceptional promise in the field of metallurgy.

Dr. Henry H. Hausner has been elected vice president of Penn-Texas Corp.

Franklin P. Hinman has been appointed to the newly created post of operations manager, cathode ray and power tube departments, of Westinghouse Electric Corp.'s Electronic Tube Div., Elmira, N. Y.

(news of Companies on p 296)

any pattern ▶



◀ any finish

any decoration ▶

now available in Campco sheet

Here's the bright new picture in plastic finishing. Whatever color you want . . . *in any pattern* . . . can now be supplied in CAMPCO sheets. Thanks to a special laminating process, the pattern you need is integrally – and permanently – bonded to the rubber modified styrene base.

In fact, you can have CAMPCO styrene decorated with any pattern you dream up – or photograph – for less cost than decals or other common techniques of applying designs. Several lively ones already widely used are: wood grains, polka dots, checks, laces and marble. Even simulated *textures,* like leather or cloth can be added by surface embossing. And the sheet can be formed into an almost endless range of products . . . quickly . . . and at low cost.

For data on how these new CAMPCO decorating ideas can make *your* product more attractive and more salable, phone or write today.

CAMPCO DIVISION

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See Campco at the National Packaging Show, April 8-11.
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For more information, turn to Reader Service Card, Circle No. 369

News of Industry

Companies

Pencoyd Steel & Forge Corp. has purchased the **Fairmount Steel Corp.** of Phila.

Resistoflex Corp. has doubled production facilities at its plant in Roseland, N. J.

Bendix Aviation Corp. and **Sheffield Corp.** have combined. Sheffield will retain its corporate title as a wholly owned subsidiary.

Brown Fintube Co. has announced that its Fired Heater Div. will be incorporated within a newly formed subsidiary, **Brown Thermal Development Co.**

Borden Co.'s Chemical Div. has established a Forest Products Research Group in Philadelphia for the development of resin and polymer products.

Kelsey-Hayes Co. will erect an 80,000-sq ft building near Springfield, Ohio, for expansion of its Speco Aviation Div.

Robertshaw-Fulton Controls Co.'s Bridgeport Thermostat Div. has opened a new plant at Milford, Conn., which more than doubles the size and output of the old plant. In Philadelphia, the company will consolidate the newly acquired Beta Corp. with its Fielder Instrument Div.

Reactive Metals, Inc., a new firm engaged in melting zirconium and its alloys, is jointly owned by Mallory-Sharon Titanium Corp. and National Distillers Products Corp.

Rust-Oleum Corp. has completed a $500,000 plant addition at Evanston, Ill., that doubles previous output.

Hubbard and Co. has acquired all outstanding stock of **Illinois Gear & Machine Co.**; it is also adding a new plant to its South Works.

Sharon Steel Corp., Brainard Div., is opening a new Product Research Development Laboratory for tool and product development and to increase engineering services.

Daco Machine & Tool Co. has changed its name to **Daco Instrument Co.**

Molded Fiber Glass Companies has

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News OF INDUSTRY

completed a $100,000 research and testing laboratory at Ashtabula, Ohio.

Kelsey-Hayes Co. has constructed a new plant near Utica, N. Y. for the Vacuum Metals Div. of its Utica Drop Forge & Tool Div. Kelsey-Hayes will also erect an 80,000-sq-ft building near Springfield, Ohio, for expansion of its Speco Aviation Div.

NRC Vaculite Corp. is the new name of National Research Corp.'s **Foiltone Products, Inc.**

L. A. Young Spring & Wire Corp. has purchased the complete assets of **Flexo Mfg. Co., Inc.,** manufacturers of aluminum honeycombs.

J. I. Case Co. announces consolidation of **American Tractor Corp.** into Case.

Summers Gyroscope Co. is building a new plant, adjacent to the main building, that will more than double its present facilities.

Allmetal Screw Products Co. announces its second Annual Allmetal Stainless Steel Awards competition. Cash awards will total $1500; deadline for entries is June 1.

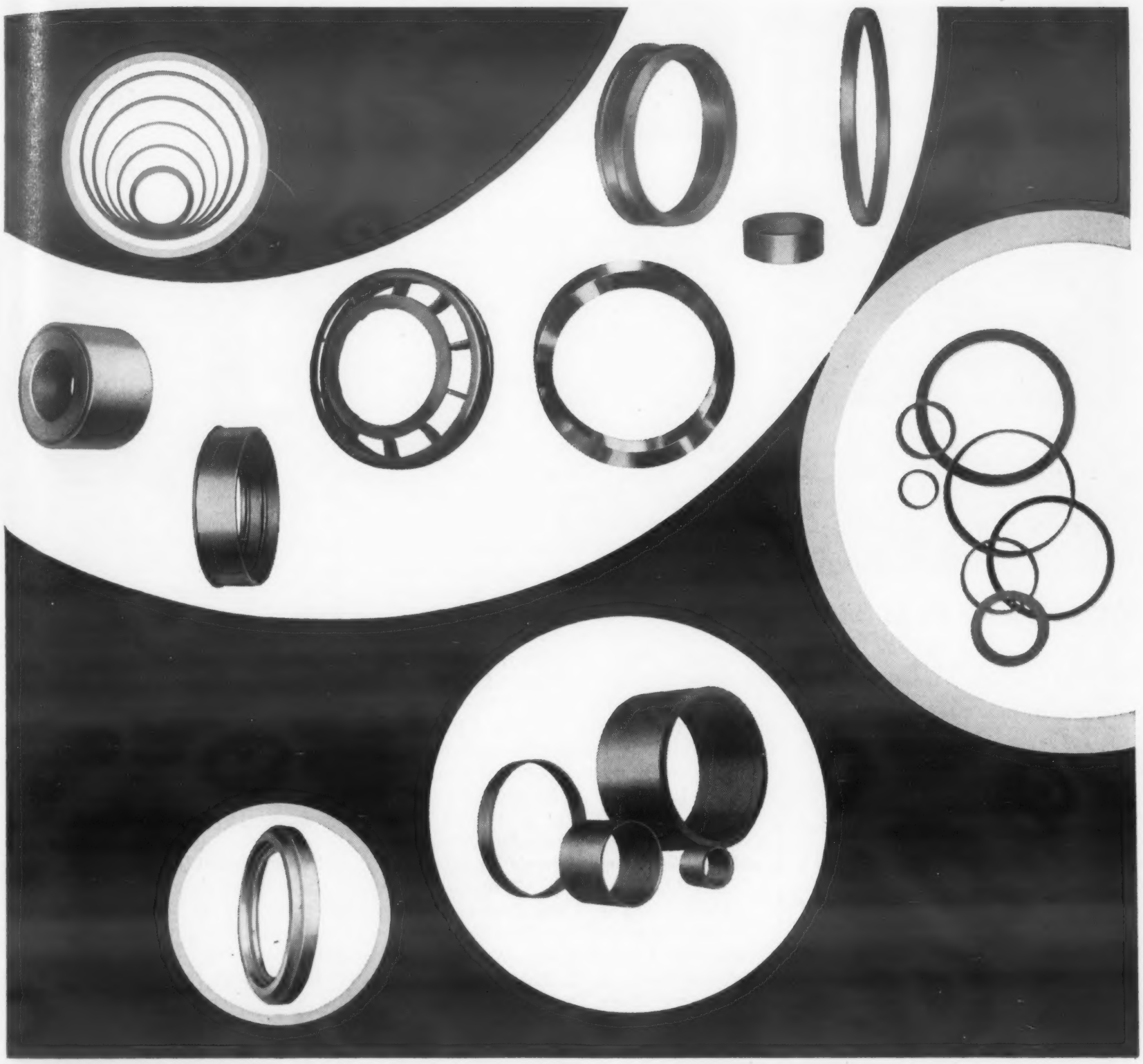
Jerguson Gage & Valve Co. has moved into its new plant at Burlington, Mass.

Societies

Federation of Paint and Varnish Production Clubs has named Joseph W. Tomecko, of Canadian Industries, Ltd., president-elect.

Aluminum Assn. elected the following officers at its annual meeting: president, S. D. DenUyl, Bohn Aluminum & Brass Corp., vice presidents: Russel B. Caples, Anaconda Aluminum Co.; W. E. Dunlap, Aluminum Extrusions, Inc.; Frank R. Nichols, Nichols Wire & Aluminum Co. Board members are: honorary chairman, Arthur V. Davis, Aluminum Co. of America; chairman of the board, Everett G. Fahlman, Permold Co. Directors-at-large are: George A. Ginsburg, United Smelting & Aluminum Co., Inc.; David P. Reynolds, Alcoa.

(more news of Societies on p 300)



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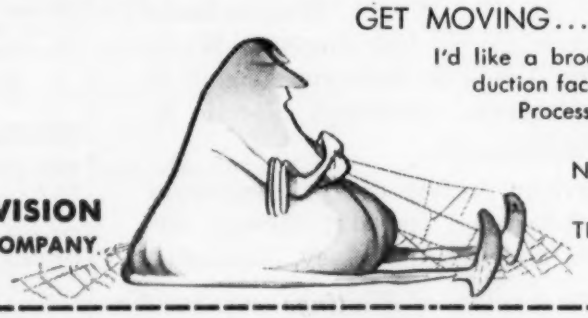

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News OF INDUSTRY

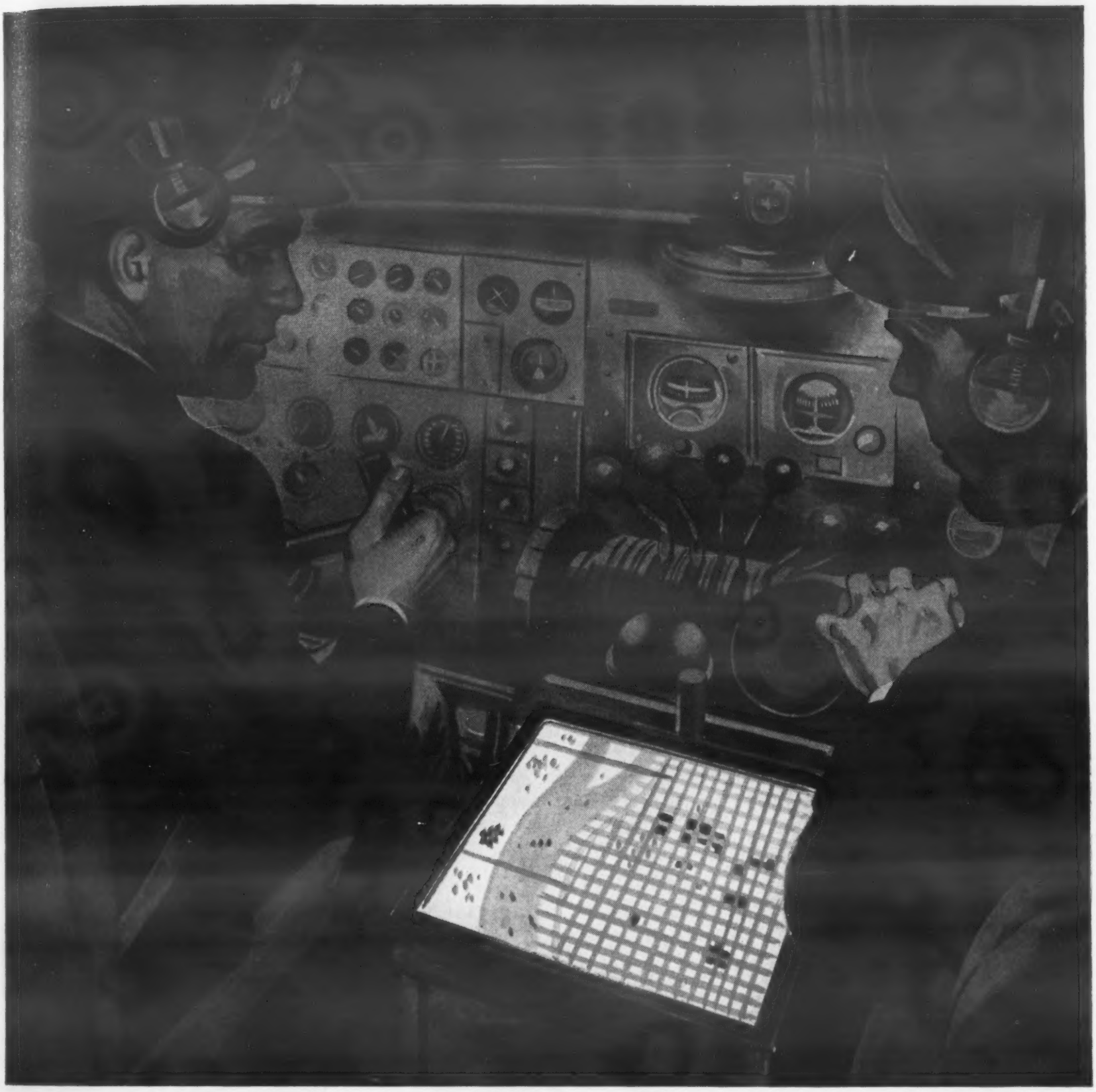
Institute of the Aeronautical Sciences, Council has elected the following 1957 Area Counselors: Joseph J. Jerger, consulting engineer; Earle Stewart, Vertol Aircraft Corp.; Smith J. DeFrance, Ames Aeronautical Laboratory, NACA; George R. Mellinger, North American Aviation, Inc.; John D. Akerman, Institute of Technology, Univ. of Minnesota; Maurice J. Zucrow, Purdue University.

American Institute of Electrical Engineers has bestowed the grade of Fellow on 16 electrical engineers for notable contributions in their fields and to the profession. The new Fellows are: Victor H. Braunig, City Public Service Board, San Antonio, Texas; Volney J. Cissna, Tennessee Valley Authority; Anatole R. Gruehr, Polytechnic Institute; Thomas J. Higgins, Univ. of Wisconsin; Russell M. Kerchner Kansas State College; Clarence H. Linder, General Electric Co.; Lawrence J. Lunas, Westinghouse Electric Corp.; Earl F. Mekelburg, Square D Company; John A. Potts, Wisconsin Electric Power Co.; Leon T. Rosenberg Allis-Chalmers Mfg. Co.; Fred J. Van Zeeland, Milwaukee School of Engineering; S. B. Morris, Los Angeles Water and Power Dept.; L. R. Patterson, Electric Operations Public Service Co.; A. H. Phillips, Gilbert Associates, Inc.; H. I. Romnes, American Telephone & Telegraph Co.; Victor Siegfried, Ansonia Wire & Cable Co.

AIEE has also announced its 1957-58 slate of officers: president, Walter J. Barrett, N. J. Bell Telephone Co.; treasurer, L. F. Hickernell, Anaconda Wire & Cable Co. The five vice presidents are: Benjamin R. Teare, Jr., Carnegie Institute of Technology; Robert W. Oetinger, Duke Power Co.; Albert G. Johnson, Omaha Public Power District; Orien A. Gustafson, General Electric Co. San Francisco; Geordon F. Tracy, University of Toronto. Directors are: E. W. Morris, Westinghouse Electric Corp., Los Angeles; W. R. Clark, Leeds & Northrup Co.; J. C. Strasbourger, Cleveland Electric Illuminating Co.

American Society of Tool Engineers has chartered its first foreign offshore chapter in Sydney, Australia.

(news of Meetings on p 302)



Next—pilots will watch their own landings on TV!

Up from pitch-dark airfields come light signals invisible to the human eye . . . A new electronic "cat eye" in the cockpit amplifies these signals to produce daylight pictures of the ground on the pilot's television screen.

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News OF INDUSTRY

Meetings

LEAD INDUSTRIES ASSN. annual meeting. Chicago. Apr 24-25.

AMERICAN ZINC INSTITUTE, INC., annual meeting. Chicago. April 25-26.

METAL POWDER ASSN. annual meeting and Metal Powder Show. Chicago. Apr 30-May 1.

ENGINEERED CASTINGS SHOW, American Foundrymen's Society. Cincinnati. May 6-10.

AMERICAN FOUNDRYMEN'S SOCIETY, annual convention. Cincinnati. May 6-10.

COPPER & BRASS RESEARCH ASSN. annual meeting. Hot Springs, Va. May 12-15.

ELECTROCHEMICAL SOCIETY, INC., spring meeting. Washington, D. C. May 12-16.

AMERICAN SOCIETY OF MECHANICAL ENGINEERS, design engineering conference. New York. May 20-22.

DESIGN ENGINEERING SHOW. New York Coliseum, New York. May 20-23.

AMERICAN IRON AND STEEL INSTITUTE, 65th general meeting of members. New York. May 22-23.

AMERICAN INSTITUTE OF MINING, METALLURGICAL AND PETROLEUM ENGINEERS, INSTITUTE OF METALS DIV., annual conference. Boston. May 17-18.

SOCIETY OF AUTOMOTIVE ENGINEERS, summer meeting. Atlantic City. June 2-7.

AMERICAN SOCIETY OF MECHANICAL ENGINEERS, semiannual meeting. San Francisco. June 9-13.

MAGNESIUM ASSN., annual meeting. Hot Springs, Va. June 10-11.

MALLEABLE FOUNDERS' SOCIETY, annual meeting. Colorado Springs. June 13-14.

AMERICAN SOCIETY FOR TESTING MATERIALS, annual meeting. Atlantic City. June 16-21.

AMERICAN ELECTROPLATERS' SOCIETY, annual convention. Montreal. June 17-20.

AMERICAN SOCIETY FOR ENGINEERING EDUCATION, annual meeting, Cornell Univ., Ithaca, N. Y. June 17-21.

ALLOY CASTING INSTITUTE, annual meeting. Hot Springs, Va. June 23-25.

AMERICAN INSTITUTE OF ELECTRICAL ENGINEERS, summer general meeting. Montreal. June 24-28.

BOOKS & REPORTS

Books

Relaxation Properties of Steels and Super-Strength Alloys at Elevated Temperatures. *Prepared by James W. Freeman and Howard R. Voorhees. ASTM Special Technical Publication No. 187, American Society for Testing Materials, Philadelphia. 1956. Paper, 8½ by 11 in., 102 pp. Price $4.00*

Summarizes a study of relaxation strengths for low alloyed molybdenum, chromium and vanadium bearing steels, carbon steel wires, cast iron, nickel-base alloys and iron-base alloys. Residual stresses for relaxation to 100, 500, 1000 and 10,000 hr are the main measure of relaxation strength. Elevated temperatures used in the evaluation range from 750 to 1100 F, with data at 1200 to 1500 F for super-strength alloys. In each case, the relaxation strength is a function of the initial stress as well as chemical composition and heat treatment. A graph compares relaxation strengths of the various alloys.

The Final Forming and Shaping of Wrought Nonferrous Metals. *Institute of Metals, London, England. 1956. Cloth, 8¾ by 11 in., 128 pp. Price $3.50*

The illustrated papers given in this book discuss: 1) machining properties of nonferrous metals, 2) deep drawing and spinning of sheet metal, with particular reference to nonferrous materials, 3) rubber pressing of aluminum and magnesium alloys, 4) research into some metal forming and shaping operations, 5) cold roll forming and manipulation of light gage sections, 6) stretch forming of nonferrous metals, 7) bending and allied forming operations, and 8) hot forming of magnesium alloys.

Nickel Handbook and Commercial Outlook for 1957. *Herman B. Director Associates, 1511 K St., NW, Wash. 5, D.C. 1956. Paper, 8½ by 11 in., 70 pp. Price $10.*

Designed as a handbook for purchasing agents and management, as well as sales and marketing executives, this book looks into the supply and demand status of nickel in 1957

Lightweight! But magnesium can really take punishment

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BOOKS & REPORTS

and gives valuable information concerning its production and consumption. It contains an index of both primary and secondary nickel suppliers and gives prices and government activities in nickel. It also lists nickel plating supply houses and nickel jobbers. In addition, a description and reproduction of government priorities and export regulations are given.

Mr. Director compiles MATERIALS & METHODS' monthly forecast on price and supply trends in engineering materials and conducts his own market research firm in Washington.

Engineering Uses of Rubber. *Edited by A. T. McPherson and Alexander Klemin. Reinhold Publishing Corp., New York 22, N. Y. 1956. Cloth, 6¼ by 9¼ in., 490 pp. Price $12.50.*

Designed for everyday use by engineers both in and out of the rubber industry, this book, written by 18 well known rubber technologists, reveals why and how rubber is used. It gives information on the manufacture of rubber products; the properties, behavior and industrial applications of rubber; and information on how to specify and purchase standard and special rubber products.

Uses of natural and synthetic rubber in such products as tires, electrical insulation, tank linings, conveyor belts, automobile suspension springs and aircraft fuel cells are discussed from the standpoint of composition, and mechanical, thermal and chemical properties. A brief explanation of the mechanical behavior of rubber is given in terms of molecular structure.

Reports

High temperature alloy THE DEVELOPMENT OF A FORGEABLE HIGH STRENGTH, HIGH TEMPERATURE, CHROMIUM-RICH, CHROMIUM-IRON ALLOY, PART 2. *D. P. Moon, H. A. Blank and A. M. Hall, Battelle Memorial Institute. Oct 1954. 26 pp. Available from Office of Technical Services, Dept. of Commerce, Wash. 25, D.C. 75¢ (PB 121111)*

Describes production of experimental chromium-rich, chromium iron alloys by induction melting. The alloys were cast into molds and fabricated by various hot working methods. Forged bars showed good thermal shock properties up to 2000 F.

(more Reports on p 308)

BOOKS & REPORTS

Damping properties THE EFFECT OF STATIC MEAN STRESS ON THE DAMPING PROPERTIES OF MATERIALS. *N. L. Person and B. J. Lazan, Univ. of Minnesota. July 1956. 34 pp. Available from Office of Technical Services, Dept. of Commerce, Wash. 25, D.C. $1 (PB 121522)*

Damping properties of materials were investigated through the use of newly developed vibration decay equipment which determined the effect of static mean stress on the damping associated with a given alternating stress. A type 403 stainless steel showed a 90% decrease in damping energy when superimposed static mean stress was increased from 0 to 40,000 psi.

Titanium carbide IRON BONDED TITANIUM CARBIDE. *R. E. Wilson, New York State College of Ceramics. Dec 1953. 39 pp. Available from Office of Technical Services, Dept. of Commerce, Wash. 25, D.C. $1 (PB 121323)*

Physical properties of iron bonded titanium carbide were found to be inferior to those of nickel bonded titanium carbide for use in aircraft power plants. However, effective techniques were developed for pressing iron bonded titanium carbide into various shapes.

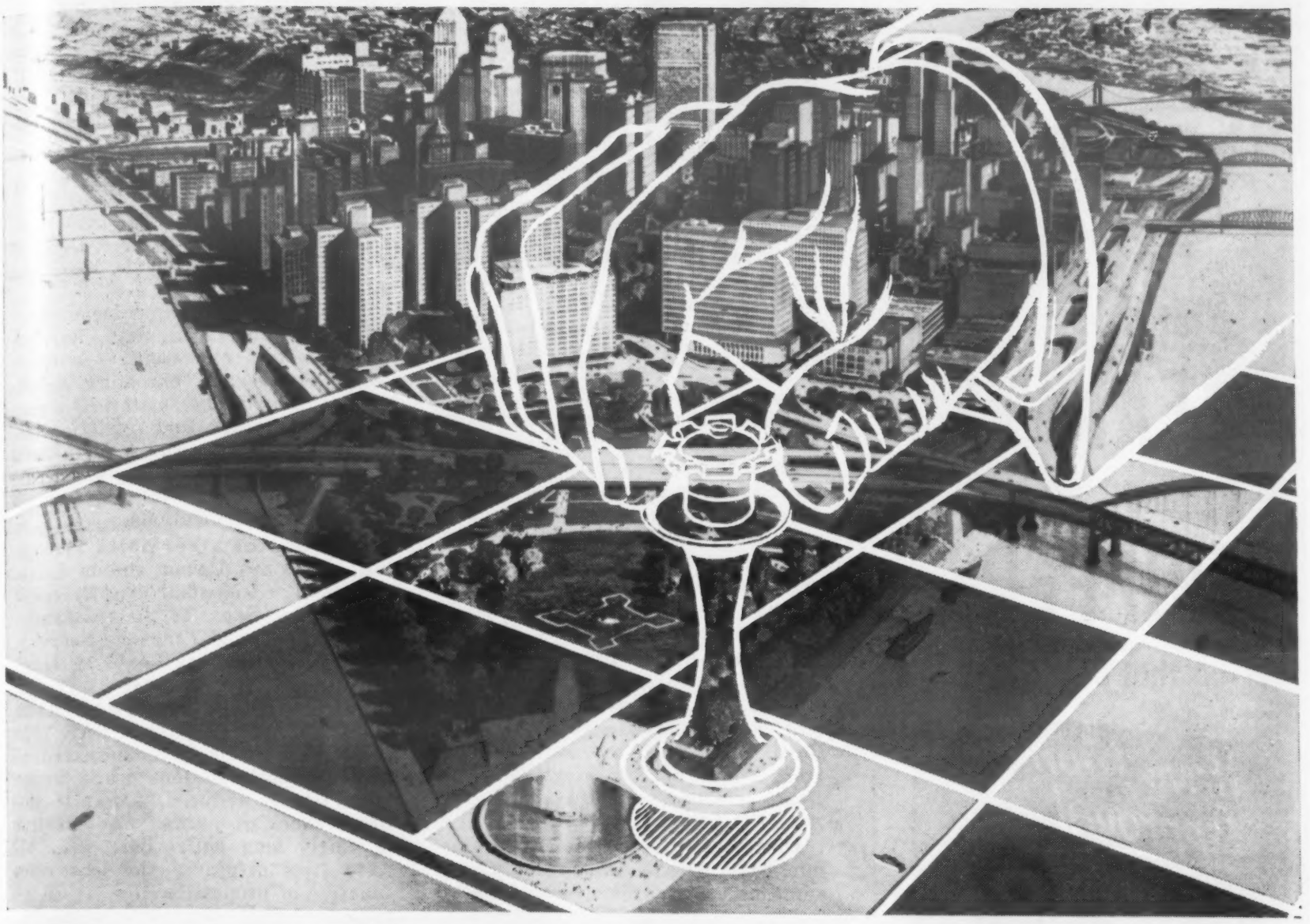
Fluorocarbon elastomers SYNTHETIC RUBBERS FROM CARBON-FLUORINE COMPOUNDS. *Frank A. Bovey, Minnesota Mining and Mfg. Co. Apr 1956. 67 pp., illus. Available from Office of Technical Services. Dept. of Commerce. Wash. 25, D.C. $1.75 (PB 121351)*

Evaluation of fluorine-containing elastomers with wide temperature ranges and resistance to solvents, hydraulic fluids, lubricants and other liquids. Includes studies of homopolymers and copolymers of fluorinated dienes and copolymers of 1,1,2-trifluorobutadiene with 1,1-dihydroperfluorobutyl acrylate (FBA).

Nickel consumption A BASIS FOR FORECASTING NICKEL DEMANDS IN THE UNITED STATES. *Available from Henry D. Lytton, 1326 27th St., NW, Washington 7, D.C. $7.50. (Library of Congress Cat. No. 56-39509)*

A survey of 45 years of nickel consumption and derivation of a demand formula, with nickel forecasts from 1956 to 1965. Gives a brief supply outlook and indicates trends of competing ferroalloys and nonferrous metals. Also compares the marketing of nickel and aluminum.

(more Reports on p 310)



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BOOKS & REPORTS

Correlating creep data CORRELATIONS OF HIGH TEMPERATURE CREEP DATA. *O. D. Sherby and J. E. Dorn, Univ. of California, June 1955. 37 pp. Available from Office of Technical Services, Dept. of Commerce, Wash. 25, D.C. $1 (PB 121287)*

Experiments on aluminum and nickel reveal that creep at high temperatures is controlled by a single thermal activation process. Simple parameters to correlate creep strain, secondary creep and stress rupture were successfully applied to very high temperature data on iron, copper, molybdenum, beryllium, commercial steels, cast irons and complex high temperature alloys.

Aluminum-base powder alloys POWDER FABRICATION OF ALUMINUM ALLOYS. *J. B. Hess and R. S. Mateer, Kaiser Aluminum & Chemical Corp. Sept 1955. 29 pp. Available from Office of Technical Services, Dept. of Commerce, Wash. 25, D.C. 75¢ (PB 121138)*

Discusses preparation of aluminum-base powder alloys containing additions of various intermetallic and refractory compounds not usually alloyable with aluminum. These compounds improved Young's modulus but tensile properties were mediocre because the additions were dispersed in a matrix of unalloyed aluminum.

Cemented borides CEMENTED BORIDES. *American Electro Metal Corp. July '55. 140 pp, illus. Available from Office of Technical Services, Dept. of Commerce, Wash. 25, D. C. Price $3.50 (PB 121346)*

Summarizes experimentation during 1954 and 1955 with Barolite IV, a cermet consisting of a chromium boride and chromium-molybdenum alloy. The material shows good heat, shock and oxidation resistance at temperatures above 2000 F. However, it has low impact resistance which hinders its use in high temperature applications.

Properties of steel bolts PROPERTIES OF BOLTS UNDER SHOCK LOADING. *E. W. Clements, Naval Research Laboratory. Sept. '56. 40 pp. Available from Office of Technical Services, Dept. of Commerce, Wash. 25, D. C. Price $1.25 (PB 121372)*

Bolts prepared from SAE 4140, SAE 1020 hot rolled, and SAE 1020 cold rolled steels were subjected to various shock motions while under load. Use of reduced shanks to improve shock properties was effective in fairly long bolts. Bolts of SAE 4140 steel displayed the best combination of properties.

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THE LAST WORD

by ***H. R. Clauser,*** *Editor*

Last Word on the Right Word

The Last Word is now on TV. I must hasten to say that it is not *me (I)* and this column that *are (is)* the program. It is a program *that (which)* deals with the proper and improper use of the English language and is conducted by the well known Dr. Bergen Evans of Northwestern University. Every Sunday afternoon he and a small panel of well known personalities get into some lively discussions and thereby demonstrate that dealing with English usage can be entertaining as well as informative.

I recommend the program to all engineers, because it very effectively puts grammar in its proper place. Grammar is a tool or a means to an end, not an end in itself. Most of those who are forever criticizing the engineer for his poor writing are really criticizing his failure to follow the textbook rules on such matters as split infinitives, prepositions at ends of sentences, and the use of the words set in italics in the above paragraph. Although the rules should not be ignored, it is important to realize that good writing is not simply a matter of closely following all the rules. Above all, clear writing is based on clear thinking. Careful adherence to all the grammatical rules in the book will never transform inaccurate, sloppy thinking into clear, simple, easily understandable writing.

Church Has a Place for Metallurgists

One of the constantly recurring problems for local sections of technical societies is where to hold their monthly meetings. Most groups like to have dinner meetings, but it is difficult these days to find a place that serves a good meal at a reasonable price, and is also satisfactory for the technical session.

The Columbus Chapter of the American Society for Metals has found a unique solution to this problem; it meets in the recreation hall of a church and has been doing so for the past five years. The hall is spacious and comfortable as I found when I spoke there last month. And the ladies auxiliary of the church prepares and serves a delicious home-cooked dinner for two dollars.

What more could one want? Oh yes, cocktails. Well, the few who want or need a drink (such as the speaker) congregate at a nearby bar and satisfy their thirst before going on to the meeting.

Chestless Plastics Drawers

The first MATERIALS & METHODS Awards Competition is over, the judging is completed, and the winners will be announced in next month's issue. The response was way above our expectations and the quality of many of the entries was excellent.

Although the competition was concerned with selection and use of materials, a number of the products were particularly interesting in themselves. One of the most interesting is a set of dice mounted on a top. When the top is spun the dice perform somewhat like a gyroscope. The inventor hopes his device will replace the old manual method of shaking the dice and thus make for a more honest game.

Another of the products should prove a boon to all gas station attendants. It is an automobile battery cap designed to show the level of the electrolyte without the need for removing the cap.

Perhaps the most intriguing of the entries was the one on chestless plastics drawers. No, they are not, as you might think, underwear without tops. The chestless plastics drawer is actually a new concept of furniture design which makes possible the construction of chests of drawers without any enclosing cabinet work.